

DAFTAR PUSTAKA

- Anonim.(2016). Data-data lepas tentang PT International Nickle Tbk (Inco).
- Arif, I., (2018). Nikel Indonesia. PT Gramedia, Jakarta, p. 246.
- Astuti, W., Zulfiadi Z., Shofi A.,Isnugroho K., Nurjaman F., dan Prasetyo E. (2012). "Pembuatan Nickel Pig Iron (NPI) dari Bijih Nikel Laterit Indonesia Menggunakan Mini Blast Furnace." Prosiding InSINas. hal. 4-6.
- Aquino, Karmina A., Arcilla, Carlo A., Schardt, Christian; Tupaz, Carmela A. J. (2022). Mineralogical and Geochemical Characterization of the Sta. Cruz Nickel Laterite Deposit, Zambales, Philippines.
- Bahfie, F. et al., (2021). Tinjauan Teknologi Proses Ekstraksi Bijih Nikel Laterit. *Jurnal Teknologi Mineral dan Batubara*, Volume 17, pp. 136-149.
- Brand, N. W., Butt, C. R. and Elias, M., (1998). Nickel laterites: Classification and Features. *AGSO Journal of Australian Geology and Geophysics*, Volume 17, pp. 81-88.
- Butt, C., (2007). “Nickel laterites characteristics, classification, and processing option”. CRCLEME. *Cooperative Research Centre for Landscape Enviroments and Mineral Exploration*.
- Cao, Z.C., Sun, T.C., Yang, H.F., Wang, J.J., and Wu, X.D. (2010). Recovery of iron and nickel from nickel laterite ore by direct reduction roasting and magnetic separation. *Journal of University of Science and Technology Beijing* , 32(6), pp. 708-712 .
- Choiriyah. (2010). Information Gop Pengungkapan Lingkungan Hidup di Indonesia. Skripsi S1 Fakultas Ekonomi Universitas.
- Dalvi, Bacon, and Osborne. (2004). “The past and the future of nickel laterite”. PDAC 2004: International convention. Trade show & investor exchange, 4(3), pp.26- 27.
- D, Ashok, Gordon Bacon, dan Robert C Osborne. (2004). The Past and the Future of Nickel Laterites. PDAC 2004 International Convention. 7 – 10 Maret 2004 Canada.
- Elliott, R., Rodrigues, F., Pickles, C. A. dan Peacey, J. (2015) “A two-stage thermal upgrading process for nickeliferous limonitic laterite ores,” *Canadian Metallurgical Quarterly*, 54(4), hal. 395-405.
- Farrokhpay, S., Filippov, L., & Fornasiero, D. (2019). Pre-concentration of nickel in laterite ores using physical separation methods. *Minerals Engineering*, 141(July), 105892.

- Firdiyono, F., Ginting, I., dan Mitsutomi, K. (1983). "Pengamatan Mineralogi Laterit Nikel Pomalaa". *Metalurgi*, 3, 3-9.
- Gleeson, S., Butt, C. & El, M., (2003). Nickel Laterites : A Review. Society of Economic Geologists (SEG), July, pp. 12-18.
- Golightly, J.P. (1981). "Nickeliferous laterite deposits", *Economic Geology*(75).pp.710- 735.
- Hamada M., Ganscow S., Klimm D., Seorghio G., Reichman. J. H, and Bickermann. (2022). Wustite (Fe_{1-x}O) Thermodynamic and crystal growth. *Journal Zeitschrift für Naturforschung B*.
- Heslop, R. dan D.L. Robinson. (1960). *Inorganic Chemistry*. Elsevier Publishing Company.
- Huang, J. Hu, H. Y, F. Yang, W. Sun, (2010). Study on the technology and mechanism of magnetic roasting and separation of a refractory red iron ore, *Min. Metall. Eng.* 30. 38–41.
- Ishii, Kotaro dan Shibata. (1975). Method For Producing High-Grade FerroNickel Directly From Nickeliferous Oxide Ores. US Patent 3996045.
- Jiang, M., Sun, T., Liu, Z., Kou, J., Liu, N. dan Zhang, S. (2013) "Mechanism of sodium sulfate in promoting selective reduction of nickel laterite ore during reduction roasting process," *International Journal of Mineral Processing*, 123, hal. 32–38.
- Klacanska. M. (2017). Kalsinasi Nikel MUD. Fakultas Bahan Ilmu Dan Teknologi Di Trnava. Slovakia University Of Technology In Bratislava.
- Kuck, P.H, (2013). Nickel, U.S. Geological Survey, Mineral Commodity Summaries," <http://minerals.usgs.gov>., 2013.
- Kyle, J., (2010), Nickel laterite processing technologies—where to next, Paper presented at the ALTA 2010 Nickel/Cobalt/Copper Conference, 24-27 May, Perth, Australia.
- Kyle, J., (2010). *Nickel Laterite Processing Technologies- Where to Next?*. Perth, ALTA 2010 Nickel/Cobalt/Copper Conference.
- Lee, H. Y., Kim, S. G. & Oh, J. K., (2005). Electrochemical leaching of nickel from low-grade laterites. *Hydrometallurgy*, Volume 77, pp. 263-268.
- Li, G., Tangming, S., Mingjun, R., Tao, J. dan Yuanbo, Z. (2012) "Beneficiation of nickeliferous laterite by reduction roasting in the presence of sodium sulfate," *Minerals Engineering*, 32, hal. 19–26.

- Lv, X., Bai, C., He, S. dan Huang, Q. (2010) “Mineral change of Philippine and Indonesia nickel lateritic ore during sintering and mineralogy of their sinter,” *ISIJ International*, 50(3), hal. 380–385.
- Ma, X., Cui, Z. dan Zhao, B. (2016) “Efficient utilization of nickel laterite to produce master alloy,” *JOM*, 68(12), hal. 3006–3014.
- McDonald, R.G. and Whittington, B.I., (2008)a, Atmospheric acid leaching of nickel laterites review: Part I. Sulphuric acid technologies. *Hydrometallurgy*, 91(1–4): p. 35-55.
- Mcrae, M., E., (2019). Nickel statistics and information, U.S. Geological Survey, MineralCommoditySummaries:USA, <http://www.usgs.gov/centers/nmic/nickelstatistics-and-information>. Diakses pada tanggal 19 juli 2023.
- Munasir. (2012). Uji XRD dan XRF pada Bahan Mineral (Batuan dan Pasir) Sebagai Sumber Material Cerdas (CaCO_3 dan SiO_2). *Jurnal Penelitian Fisika dan Aplikasinya (JPFA)* v2n1, 20-29.
- Moskalyk, R.R., Alfantazi, A.M. (2002). Nickel laterite processing and electrowinning practice. *Miner. Eng.*, Vol. 20 (15), pp. 593–595.
- Nurjaman, F., Astuti, W., Bahfie, F., & Suharno, B. (2021). Study of selective reduction in lateritic nickel ore: Saprolite versus limonite. *Materials Today: Proceedings*, 44, 1488–1494. Norgate, T. & Jahanshahi, S., (2011). Assessing the energy and greenhouse gas footprints of nickel laterite processing. *Mineral Engineering*.
- Oxley, A. & Barcza, N., (2013). Hydro-pyro integration in the processing of nickel laterites. *International Journal of Minerals Engineering*, pp. 2-13.
- Pickles C.A., Forster J., and Elliot R. (2014). “Thermodynamic analysis of the carbothermic reduction roasting of nickeliferous limonitic laterite ore,” *Minerals Engineering*., vol.65, pp. 33-40, 2014.
- Pournaderi, S., Keskinikliç, E., Geveci, A. and Topkaya, Y. A. (2014) “Reducibility of nickeliferous limonitic laterite ore from Central Anatolia,” *Canadian Metallurgical Quarterly*, 53(1), pp. 26–37.
- Prasetyo, A., dan Puguh. (2011). Peningkatan Kadar Nikel dan Besi dari Bijih Nikel Laterit Kadar Rendah Jenis Saprolit untuk Bahan Baku NPI. *Jurnal Metalurgi*. Vol. 26. No. 3. Pp: 123-130.
- Prasetyo, P.; & Ronald, N. (2014). Masih Terbukanya Peluang Penelitian Proses Caron Untuk Mengolah Nikel Laterit Kadar Rendah di Indonesia. *Majalah Metalurgi*, 26, 35-44.
- Raivel, dan Firman. (2020). Karakteristik Endapan Nikel Laterit di Bawah Molasa, Daerah Tinanggea, Sulawesi Tenggara. *Jurnal GeoMining*. Program Sudi Teknik Pertambangan, Fakultas Teknik. Kendari.

- Rao, M., Li, G., Zhang, X., Luo, J., Peng, Z., and Jiang, T.,(2016). “Reductive Roasting of Nickel Laterite Ore with Sodium Sulphate for Fe-Ni Production”, Part I: Reduction/Sulfidation Characteristics. *Separation Science and Technology*, (51).pp. 1408-1420.
- Rusmini, (2010). Analisis besi dalam mineral melalui proses kopresipitasi menggunakan nikel dibutil ditiokarba ma. Semarang: UNNES.
- Rodrigues, F. M., (2013), *Investigation Into The Thermal Upgrading Of Nickeliferous Laterite Ores. A thesis submitted to the Robertbuchar Department of Mining In Corminity with the requirements for The degree of Master of applied Sciece*, Queens University, Kingston, Toronto, Canada.
- Ropp, R. C. (2013) Group 14 (C, Si, Ge, Sn, and Pb) Alkaline Earth Compunds. *Encyclopedia of the Alkaline Earth Compounds*, 351 – 480.
- Santoso, B. dan Subagio, (2018). Pemodelan Nikel Laterit Berdasarkan Data Resistivitas Di Daerah Kabaena Selatan Kabupaten Bombana, Provinsi Sulawesi Tenggara The Laterite Nickel Modelling Based On Resistivity Data, In South Kabaena, Bombana District, Southeast Sulawesi Province. *Jurnal Geologi dan Sumberdaya Mineral*, Departemen Geokimia, Universitas Padjajaran, jalan Diponegoro, Bandung.
- Sembiring. M dan Sinaga, T. (2003). Arang Aktif (Pengenalan Dan Proses Pembuatannya). Medan: Universitas Sumatra Utara.
- Sembiring, S., & Simanjuntak, W. (2015). Silika Sekam Padi Potensinya Sebagai Bahan Baku Keramik Industri (Vol. 148). Plantaxia.
- Setiawan, I., (2016). Pengolahan Nikel Laterit Secara Pirometalurgi: Kini Dan Penelitian Kedepan. *Seminar Nasional Sains dan Teknologi*. Pp 1-7
- Sufriadin, (2013), *Mineralogi, Geokimia dan Sifat Leaching pada Endapan Laterit Nikel Sorowako, Sulawesi Selatan Indonesia*, Universitas Gadjahmada.
- Tarumingkeng Stephanie. (2016). *Termodinamika Dalam Memahami Proses Pengolahan Mineral Prodi Fisika FMIPA Institut Teknologi Bandung*.
- Warner, A. E. M., Díaz, C. M., Dalvi, A. D., Mackey, P. J., Tarasov, A. V., & Jones, R. T. (2007). JOM world nonferrous smelter survey Part IV: Nickel: Sulfide. *Jom*, 59(4), 58–72.
- Wills, B. A., and Napiermunn, T., (2006). *Mineral Processing Technology: An Introduction to the Practical Aspects of Ore Treatment and Mineral Recovery*, 7th ed. Elsevier. Burlington.
- Y. Qu, L. Xing, L. Shao, Y. Luo, Z. Zou, (2019). Microstructural characterization and gas-solid reduction kinetics of iron ore fines at high temperature, *Powder Technol.* 355. 26–36.

- Y. Lu, Z. Wei, Y. Wang, J. Zhang, G. Li, Y. Zhang, (2019). Research on the characteristics and kinetics of direct reduction of limonite ore fines under CO atmosphere in a rotary drum reactor, *Powder Technol.* 352. 240–250. <https://doi.org/10.1016/j.powtec.2019.04.069>.
- Zhu, D. Q., Cui, Y., Vining, K., Hapugoda, S., Douglas, J., Pan, J. dan Zheng, G. L. (2012) “Upgrading low nickel content laterite ores using selective reduction followed by magnetic separation,” *International Journal of Mineral Processing*, 106–109, hal. 1–7.

LAMPIRAN

LAMPIRAN 1
HASIL ANALISIS *X-RAY DIFFRACTION* (XRD)

1. Sampel Awal

Match! Phase Analysis Report

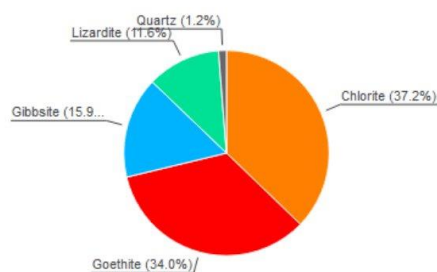
Sample: Shinta-SampelAwal

Sample Data

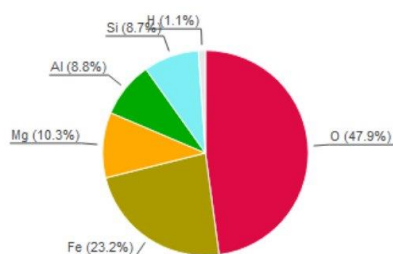
File name Shinta-SampelAwal.txt
 File path E:/BISMILLAH TA SHINTA/SKRIPSI/Shinta-SampelAwal
 Data collected Sep 29, 2023 11:57:32
 Data range 5.000° - 70.000°
 Original data range 5.000° - 70.000°
 Number of points 3251
 Step size 0.020
 Rietveld refinement converged No
 Alpha2 subtracted No
 Background subtr. No
 Data smoothed Yes
 Radiation X-rays
 Wavelength 1.541874 Å

Analysis Results

Phase composition (Weight %)



Elemental composition (Weight %)



IndexAmountName (%)

A 37.2 Chlorite
 B 34.0 Goethite
 C 15.9 Gibbsite
 D 11.6 Lizardite
 E 1.2 Quartz
 1.3 Unidentified peak area

Formula sum

Al_{0.865} Fe_{0.255} H₄ Mg_{2.292} O₉ Si_{1.588}
 Fe H O₂
 Al O₃
 H₄ Mg₃ O₉ Si₂
 O₂ Si

Element Amount (weight %)

O 47.9% (*)
 Fe 23.2%
 Mg 10.3%
 Al 8.8%
 Si 8.7%
 H 1.1% (*)
 *LE (sum) 49.0%

Amounts calculated by RIR (Reference Intensity Ratio) method

Details of identified phases

A: Chlorite (37.2 %)*

Formula sum Al_{0.865} Fe_{0.255} H₄ Mg_{2.292} O₉ Si_{1.588}
 Entry number 96-901-0164
 Figure-of-Merit (FoM) 0.576327*
 Total number of peaks 600
 Peaks in range 312
 Peaks matched 98
 Intensity scale factor 0.21*
 Space group C 1 2/m 1
 Crystal system monoclinic
 Unit cell a= 5.3363 Å b= 9.2400 Å c= 14.3700 Å β= 96.930 °
 I/c 0.69
 Calc. density 2.700 g/cm³
 Reference Zanazzi P. F., Montagnoli M., Nazzareni S., Comodi P., "Structural effects of pressure on monoclinic chlorite: a single-crystal study", American Mineralogist **92**, 655-661 (2007)

B: Goethite (34.0 %)*

Formula sum	Fe H O ₂
Entry number	96-900-2160
Figure-of-Merit (FoM)	0.749632*
Total number of peaks	364
Peaks in range	74
Peaks matched	45
Intensity scale factor	0.65*
Space group	P n m a
Crystal system	orthorhombic
Unit cell	a= 9.9189 Å b= 3.0148 Å c= 4.5835 Å
I/Ic	2.38
Calc. density	4.306 g/cm ³
Reference	Gualtieri A., Venturelli P., "In situ study of the goethite-hematite phase transformation by real timesynchrotron powder diffractionSample at T = 156 C", American Mineralogist 84 , 895-904 (1999)

C: Gibbsite (15.9 %)

Formula sum	Al O ₃
Entry number	96-901-5977
Figure-of-Merit (FoM)	0.000000
Total number of peaks	996
Peaks in range	348
Peaks matched	119
Intensity scale factor	0.23
Space group	P 1 2 ₁ /n 1
Crystal system	monoclinic
Unit cell	a= 8.6410 Å b= 5.0700 Å c= 9.7200 Å β= 85.430 °
I/Ic	1.79
Calc. density	2.347 g/cm ³
Reference	Megaw H., "The crystal structure of Hydrargillite Al (O H) ₃ _cod_database_code 1011081", Zeitschrift fur Kristallographie 87 , 185-204 (1934)

D: Lizardite (11.6 %)*

Formula sum	H ₄ Mg ₃ O ₉ Si ₂
Entry number	96-900-0849
Figure-of-Merit (FoM)	0.467227*
Total number of peaks	224
Peaks in range	56
Peaks matched	18
Intensity scale factor	0.13*
Space group	P 3 1 m
Crystal system	trigonal (hexagonal axes)
Unit cell	a= 5.3320 Å c= 7.2330 Å
I/Ic	1.35
Calc. density	2.584 g/cm ³
Reference	Mellini M., "The crystal structure of lizardite 1T: hydrogen bonds and polytypism", American Mineralogist 67 , 587-598 (1982)

E: Quartz (1.2 %)

Formula sum	O ₂ Si
Entry number	96-900-0776
Figure-of-Merit (FoM)	0.000000
Total number of peaks	140
Peaks in range	36
Peaks matched	11
Intensity scale factor	0.03
Space group	P 3 ₂ 2 1 S
Crystal system	trigonal (hexagonal axes)
Unit cell	a= 4.9160 Å c= 5.4054 Å
I/Ic	2.95
Calc. density	2.646 g/cm ³
Reference	Levien L., Prewitt C. T., Weidner D. J., "Structure and elastic properties of quartz at pressureP = 1 atm", American Mineralogist 65 , 920-930 (1980)

(*)2theta values have been shifted internally for the calculation of the amounts, the intensity scaling factors as well as the figure-of-merit (FoM), due to the active search-match option 'Automatic zero point adaption'.

Candidates

Name	Formula	Entry No.	FoM
Neon	Ne	96-901-1723	0.6112
	Nb Zr	96-153-7846	0.5676
Li _{0.77} (Ni _{0.7} Fe _{0.15} Co _{0.15}) _{1.03} O ₂	Co _{0.1545} Fe _{0.1545} Li _{0.77} Ni _{0.721} O ₂	96-152-6305	0.5476
Li Co _{0.333} Ni _{0.333} Mn _{0.333} O ₂	Co _{0.333} Li Mn _{0.333} Ni _{0.333} O ₂	96-400-2444	0.5456
(Li _{0.99} Ni _{0.01}) ((Ni _{0.70} Co _{0.15} Al _{0.15}) O ₂)	Al _{0.15} Co _{0.15} Li _{0.99} Ni _{0.71} O ₂	96-153-3586	0.5448
Lithium Cobalt Oxide	Co Li _{1.43} O ₂	96-155-0400	0.5388
(Li _{0.82} Ni _{0.026}) Ni _{0.994} O ₂	Li _{0.82} Ni _{1.02} O ₂	96-152-6281	0.5373
Li (Cr _{0.167} Li _{0.277} Mn _{0.556}) O ₂	Cr _{0.167} Li _{1.277} Mn _{0.556} O ₂	96-153-2835	0.5251
Li (Cr _{0.25} Li _{0.25} Mn _{0.5}) O ₂	Cr _{0.25} Li _{1.25} Mn _{0.5} O ₂	96-153-2836	0.5250
(Li _{0.88} Mg _{0.02}) (Ni _{0.92} Mg _{0.08}) O ₂	Li _{0.88} Mg _{0.1} Ni _{0.92} O ₂	96-152-6285	0.5075
(Li _{0.98} Ni _{0.02}) (Li _{0.05} Ni _{0.75} Co _{0.1} Mn _{0.1}) O ₂	Co _{0.1} Li _{1.03} Mn _{0.1} Ni _{0.77} O ₂	96-152-0790	0.5026
	Li _{0.65} Ni _{1.08} O ₂	96-153-5513	0.5013

Spinel	Al ₂ .401 Mg _{0.398} O ₄	96-900-5769	0.4197
Spinel	Al ₂ Mg O ₄	96-900-5768	0.4173
Spinel	Al _{1.88} Fe _{0.225} Mg _{0.887} Mn _{0.005} Ni ₂ O ₄ Zn _{0.001}	96-900-5346	0.3825
Spinel (Li, Ti)	Li _{1.03} O ₄ Ti ₂	96-100-8792	0.0000
Spinel (Li, Ti)	Li _{0.89} O ₄ Ti ₂	96-100-8793	0.0000
Spinel (Li, Ti)	Li _{0.75} O ₄ Ti ₂	96-100-8794	0.0000
Iron diiron(III) oxide (Magnetite)	Fe ₃ O ₄	96-101-1033	0.0000
Aluminium hydroxide (Gibbsite)	Al H ₃ O ₃	96-101-1082	0.0000
Iron diiron(III) oxide (Magnetite)	Fe ₃ O ₄	96-101-1085	0.0000
Silicon oxide β -alpha (Quartz low)	O ₂ Si	96-101-1098	0.0000
Trimagnesium dihydroxide phyllo-tetrasilicate (Talc 2M)	H ₂ Mg ₃ O ₁₂ Si ₄	96-101-1153	0.0000
Silicon oxide (Quartz low)	O ₂ Si	96-101-1160	0.0000
Silicon oxide β -alpha (Quartz low)	O ₂ Si	96-101-1173	0.0000
Silicon oxide - β -alpha (Quartz low)	O ₂ Si	96-101-1177	0.0000
Silicon oxide - β (Quartz high)	O ₂ Si	96-101-1201	0.0000
Silicon oxide (Quartz high)	O ₂ Si	96-110-0020	0.0000
Montmorillonite	Al ₂ Ca O ₁₂ Si ₄	96-110-1055	0.0000
Aluminium hydroxide (Gibbsite)	Al H ₃ O ₃	96-120-0017	0.0000
Lithium Manganese Oxide (0.78/1.88/4) (Unnamed_Spinel)	Li _{0.78} Mn _{1.88} O ₄	96-151-4008	0.0000
Lithium Manganese Oxide (1/2/4) (Unnamed_Spinel)	Li Mn ₂ O ₄	96-151-4042	0.0000
Lithium Manganese Oxide (1/2/4) (Unnamed_Spinel)	Li Mn ₂ O ₄	96-151-4043	0.0000
Lithium Manganese Oxide (1/2/4) (Unnamed_Spinel)	Li Mn ₂ O ₄	96-151-4051	0.0000
Magnetite	Fe ₃ O ₄	96-153-9748	0.0000
Zn ₂ TiO ₄ ordered spinel	O ₄ Ti Zn ₂	96-154-4335	0.0000
LiFe ₅ O ₈ ordered spinel	Fe ₅ Li O ₈	96-154-4336	0.0000
LiZnNbO ₄ ordered spinel	Li Nb O ₄ Zn	96-154-4337	0.0000
Al(OH) ₃ gibbsite (gibbsite)	Al H ₃ O ₃	96-154-4376	0.0000
Zn ₂ TiO ₄ cubic spinel	O ₄ Ti Zn ₂	96-154-4563	0.0000
Zn _{1.92} Ti _{0.84} Ta _{0.16} O ₄ cubic spinel	O ₄ Ta _{0.16} Ti _{0.84} Zn _{1.92}	96-154-4565	0.0000
Zn _{1.925} Ti _{0.85} Ta _{0.15} O ₄ cubic spinel	O ₄ Ta _{0.15} Ti _{0.85} Zn _{1.925}	96-154-4566	0.0000
Zn _{1.93} Ti _{0.86} Ta _{0.14} O ₄ cubic spinel	O ₄ Ta _{0.14} Ti _{0.86} Zn _{1.93}	96-154-4567	0.0000
Zn _{1.95} Ti _{0.9} Ta _{0.1} O ₄ cubic spinel	O ₄ Ta _{0.1} Ti _{0.9} Zn _{1.95}	96-154-4568	0.0000
Zn _{1.7} Ti _{0.4} Ta _{0.6} O ₄ tetragonal spinel	O ₄ Ta _{0.6} Ti _{0.4} Zn _{1.7}	96-154-4569	0.0000
Zn _{1.925} Ti _{0.85} Ta _{0.15} O ₄ tetragonal spinel	O ₄ Ta _{0.15} Ti _{0.85} Zn _{1.925}	96-154-4570	0.0000
Zn _{1.925} Ti _{0.85} Ta _{0.15} O ₄ cubic spinel	O ₄ Ta _{0.15} Ti _{0.85} Zn _{1.925}	96-154-4576	0.0000
(Co _{0.4} Al _{0.4})Al ₂ O ₄ defect spinel	Al _{2.4} Co _{0.4} O ₄	96-154-5122	0.0000
Zn ₂ SiO ₄ modified spinel (Zn ₂ SiO ₄ wadsleyite phase)	O ₄ Si Zn ₂	96-154-9040	0.0000
Zn ₂ GeO ₄ cubic spinel	Ge O ₄ Zn ₂	96-154-9041	0.0000
Zn ₂ GeO ₄ tetragonal spinel	Ge O ₄ Zn ₂	96-154-9042	0.0000
spinel (Ni _{0.15} Al _{0.85})(Ni _{0.425} Al _{0.475} Cr _{0.1}) ₂ O ₄	Al _{1.8} Cr _{0.2} Ni O ₄	96-155-9487	0.0000

and 880 others...

Search-Match

Settings

Reference database used	COD-Inorg 2023.06.06
Automatic zeropoint adaptation	Yes
Downgrade entries with low scaling factors	Yes
Minimum figure-of-merit (FoM)	0.50
2theta window for peak corr.	0.30 deg.
Minimum rel. int. for peak corr.	0
Parameter/influence 2theta	0.50
Parameter/influence intensities	0.50
Parameter multiple/single phase(s)	0.50

Criteria for entries added by user

Reference:

Entry number:	96-101-1153;96-300-0049;96-900-8041;96-900-8298;96-900-8732;96-901-4436;96-901-7404;96-110-1055;96-900-2780;96-901-0957;96-901-0958;96-901-0959;96-901-0960;96-101-1033;96-101-1085;96-153-9748;96-722-8111;96-900-0927;96-900-0928;96-900-0929;96-900-0930;96-900-0931;96-900-0932;96-900-0933;96-900-0934;96-900-0935;96-900-2317;96-900-2318;96-900-2319;96-900-2320;96-900-2321;96-900-2322;96-900-2323;96-900-2324;96-900-2325;96-900-2326;96-900-2327;96-900-2328;96-900-2329;96-900-2330;96-900-2331;96-900-2332;96-900-2333;96-900-2674;96-900-2675;96-900-4088;96-900-4156;96-900-4157;96-900-5813;96-900-5814;96-900-5815;96-900-5816;96-900-5817;96-900-5837;96-900-5838;96-900-5839;96-900-5840;96-900-5841;96-900-5842;96-900-5843;96-900-6185;96-900-6190;96-900-6195;96-900-6200;96-900-6243;96-900-6248;96-900-6253;96-900-6266;96-900-6921;96-900-6922;96-900-6923;96-900-7645;96-900-7707;96-900-7708;96-900-9769;96-900-9770;96-901-0940;96-901-0941;96-901-0942;96-901-3530;96-901-3531;96-901-3532;96-901-3533;96-901-3534;96-901-3535;96-901-3536;96-901-6802;96-901-6803;96-901-6804;96-901-6805;96-901-6806;96-901-6807;96-901-6808;96-901-6809;96-901-6810;96-901-6811;96-901-6812;96-901-6813;96-901-6814;96-901-6815;96-901-6816;96-901-6817;96-901-6818;96-901-7087;96-901-7088;96-900-0849;96-900-1092;96-900-1093;96-900-1639;96-900-1640;96-900-1779;96-900-1883;96-900-4509;96-900-4510;96-900-4511;96-900-4512;96-900-4513;96-900-4514;96-900-4994;96-900-4995;96-900-7425;96-901-4665;96-901-5164;96-901-5487;96-901-5581;96-901-6051;96-901-6148;96-901-7502;96-101-1098;96-101-1160;96-101-1173;96-101-1177;96-101-1201;96-110-0020;96-500-0036;96-900-0776;96-900-0777;96-900-0778;96-900-0779;96-900-0780;96-900-0781;96-900-5018;96-900-5019;96-900-5020;96-900-5021;96-900-5022;96-900-5023;96-900-5024;96-900-5025;96-900-5026;96-900-5027;96-900-5028;96-900-5029;96-900-5030;96-900-5031;96-900-5032;96-900-5033;96-900-5034;96-900-7379;96-900-8093;96-900-8094;96-900-9667;96-901-0145;96-901-0146;96-901-0147;96-901-1494;96-901-1495;96-901-1496;96-901-1497;96-901-2601;96-901-2602;96-901-2603;96-901-2604;96-901-2605;96-901-2606;96-901-3322;96-901-5023;96-101-1082;96-120-0017;96-154-4376;96-900-3875;96-900-8238;96-901-1748;96-901-5516;96-901-5977;96-100-8792;96-100-8793;96-100-8794;96-151-4008;96-151-4042;96-151-4043;96-151-4051;96-154-
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6052;96-901-6077;96-901-6091;96-901-6097;96-901-6176;96-901-6239;96-901-6268;96-901-6317;96-901-6329;96-901-6337;96-901-6344;96-901-6363;96-901-6364;96-901-6365;96-901-6371;96-901-6417;96-901-6435;96-901-6475;96-901-6505;96-901-6565;96-901-6578;96-901-6603;96-901-6677;96-901-6699;96-901-6720;96-901-6915;96-901-6916;96-901-6917;96-901-6918;96-901-6919;96-901-7026;96-901-7027;96-901-7028;96-901-7030;96-901-7031;96-901-7032;96-901-7033;96-901-7034;96-901-7035;96-901-7036;96-901-7037;96-901-7038;96-901-7053;96-901-7054;96-901-7055;96-901-7056;96-901-7057;96-201-4618;96-201-4619;96-201-4931;96-220-5377;96-220-7380;96-220-7381;96-900-0159;96-900-4189;96-901-0164;96-901-0165;96-901-0166;96-901-0167;96-901-0168;96-901-0169;96-901-0170

Peak List

No.	2theta [°]	d [Å]	I/I0 (peak height)	Counts (peak area)	FWHM	Matched
1	6.45	13.7037	111.48	7.90	0.5333	A
2	10.82	8.1802	56.39	7.03	0.9391	
3	12.45	7.1119	375.61	24.24	0.4858	A,D
4	14.02	6.3182	36.64	1.77	0.3645	C
5	15.45	5.7364	28.60	1.48	0.3885	
6	16.79	5.2805	18.83	1.13	0.4526	
7	18.72	4.7413	408.78	28.96	0.5334	A
8	21.28	4.1757	1000.00	112.47	0.8467	B
9	25.05	3.5551	418.05	23.47	0.4226	A
10	26.64	3.3467	200.90	11.29	0.4230	A,B,C,E
11	31.48	2.8422	79.86	4.35	0.4098	A,C,D
12	33.33	2.6886	311.44	34.83	0.8418	A,B,C,D
13	34.96	2.5664	125.36	21.68	1.3021	A,B,C
14	35.72	2.5136	380.28	33.47	0.6626	B,C,D
15	36.86	2.4389	891.16	89.27	0.7542	A,B,C,E
16	40.35	2.2355	155.06	22.83	1.1082	A,B,C,E
17	41.35	2.1837	148.84	13.41	0.6782	A,B,C,D
18	43.38	2.0860	0.37	0.10	2.0400	A,B,C
19	44.58	2.0326	27.56	3.07	0.8400	A,C
20	45.22	2.0053	42.89	10.64	1.8680	A,B,C
21	47.40	1.9180	33.77	7.99	1.7820	B,C
22	48.52	1.8763	5.83	1.17	1.5076	A,B,C
23	51.00	1.7908	48.48	8.21	1.2757	A,B,C,D,E
24	53.70	1.7069	354.41	62.11	1.3193	A,B,C
25	57.48	1.6033	106.33	9.00	0.6375	A,B,C,E
26	59.24	1.5598	148.97	23.39	1.1821	A,B,C
27	61.76	1.5021	108.12	11.94	0.8315	A,B,C,D
28	63.00	1.4754	105.11	8.32	0.5959	B,C
29	64.18	1.4511	7.58	2.43	2.4131	A,B,C,D,E
30	66.19	1.4120	0.27	0.10	2.7659	A,B,C,D,E
31	66.86	1.3994	42.63	9.64	1.7022	A,C
32	68.80	1.3646	35.38	8.00	1.7022	A,B,C

Integrated Profile Areas

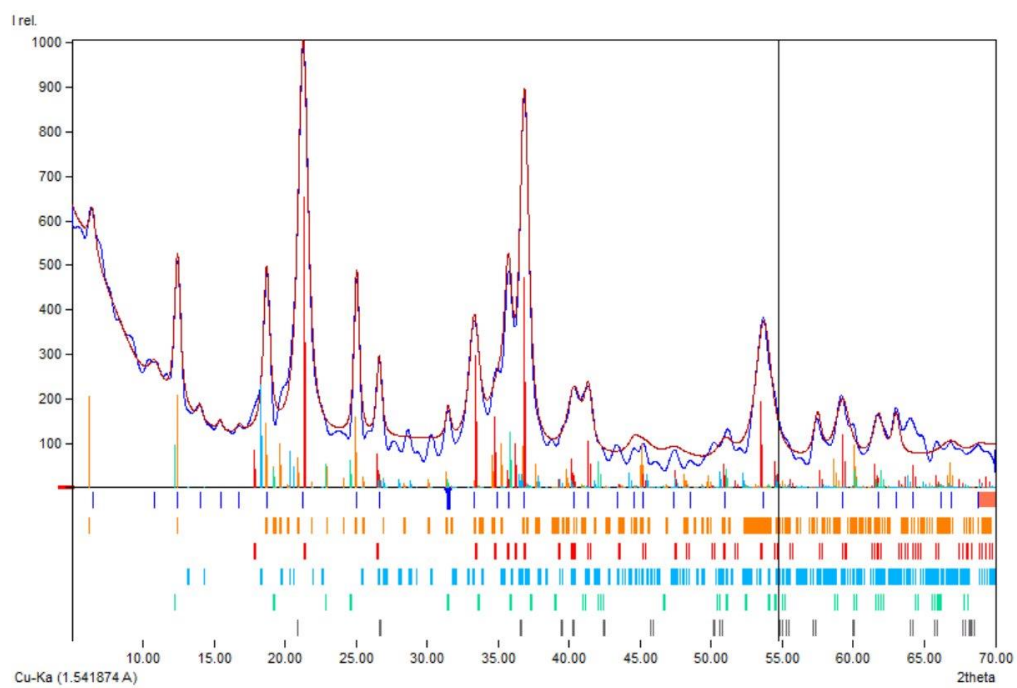
Based on calculated profile

Profile area	Counts	Amount
Overall diffraction profile	73538	100.00%
Background radiation	45253	61.54%
Diffraction peaks	28286	38.46%
Peak area belonging to selected phases	27346	37.19%
Peak area of phase A (Chlorite)	8252	11.22%
Peak area of phase B (Goethite)	13889	18.89%
Peak area of phase C (Gibbsite)	2865	3.90%
Peak area of phase D (Lizardite)	2137	2.91%
Peak area of phase E (Quartz)	203	0.28%
Unidentified peak area	940	1.28%

Peak Residuals

Peak data	Counts	Amount
Overall peak intensity	606	100.00%
Peak intensity belonging to selected phases	504	83.20%
Unidentified peak intensity	102	16.80%

Diffraction Pattern Graphics



Match! Copyright © 2003-2023 CRYSTAL IMPACT, Bonn, Germany

2. Sampel Setelah Pemangggangan Tereduksi dengan Peningkatan Ni Tertinggi pada Suhu Pemangggangan 1000°C dan Fraksi 100 Mesh

Match! Phase Analysis Report

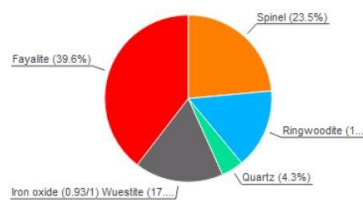
Sample: Shinta-1000C (5-70)

Sample Data

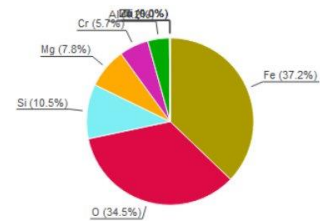
File name	Shinta-1000C.ORG
File path	E:/BISMILLAH TA SHINTA/SKRIPSI/Shinta-1000C
Data collected	Sep 29, 2023 11:57:32
Data range	5.000° - 70.000°
Original data range	5.000° - 70.000°
Number of points	3251
Step size	0.020
Rietveld refinement converged	No
Alpha2 subtracted	No
Background subtr.	No
Data smoothed	Yes
Radiation	X-rays
Wavelength	1.540600 Å

Analysis Results

Phase composition (Weight %)



Elemental composition (Weight %)



Index	Amount (%)	Name	Formula sum
A	23.5	Spinel	Al _{1.129} Cr _{0.799} Fe _{0.307} Mg _{0.736} Mn _{0.004} Ni _{0.005} O ₄ Si _{0.002} Ti _{0.005} Zn _{0.003}
B	15.4	Ringwoodite	Mg ₂ O ₄ Si
C	4.3	Quartz	O ₂ Si
D	17.2	Iron oxide (0.93/1)	WuestiteFe _{0.932} O
E	39.6	Fayalite	Fe ₂ O ₄ Si
	6.8	Unidentified peak area	

Amounts calculated by RIR (Reference Intensity Ratio) method

Element	Amount (weight %)
Fe	37.2%
O	34.5% (*)
Si	10.5%
Mg	7.8%
Cr	5.7%
Al	4.2%
Ni	0.0%
Ti	0.0%
Mn	0.0%
Zn	0.0%
*LE (sum)	34.5%

Details of identified phases

A: Spinel (23.5 %)
 Formula sum: Al_{1.129}Cr_{0.799}Fe_{0.307}Mg_{0.736}Mn_{0.004}Ni_{0.005}O₄Si_{0.002}Ti_{0.005}Zn_{0.003}
 Entry number: 96-900-5621
 Figure-of-Merit (FoM): 0.666389
 Total number of peaks: 34
 Peaks in range: 34
 Peaks matched: 6
 Intensity scale factor: 0.55
 Space group: F d -3 m
 Crystal system: cubic
 Unit cell: a = 8.2129 Å
 I/c: 2.93
 Calc. density: 4.126 g/cm³
 Reference: Carraro A., "Crystal chemistry of Cr-spinels from a suite of spinel peridotite mantle xenoliths from the Predazzo Area (Dolomites, Northern Italy) Sample: CRSP4", European Journal of Mineralogy **15**, 681-688 (2003)

B: Ringwoodite (15.4 %)
 Formula sum: Mg₂O₄Si
 Entry number: 96-900-0270
 Figure-of-Merit (FoM): 0.000000
 Total number of peaks: 34
 Peaks in range: 4
 Peaks matched: 4
 Intensity scale factor: 0.26
 Space group: F d -3 m
 Crystal system: cubic
 Unit cell: a = 8.1200 Å
 I/c: 2.13
 Calc. density: 3.491 g/cm³
 Reference: Baur W. H., "Computer-simulated crystal structures of observed and hypothetical Mg₂SiO₄ polymorphs of low and high density normal", American Mineralogist **57**, 709-731 (1972)

C: Quartz (4.3 %)
 Formula sum: O₂Si
 Entry number: 96-901-2605
 Figure-of-Merit (FoM): 0.000000
 Total number of peaks: 60
 Peaks in range: 60
 Peaks matched: 5

Intensity scale factor 0.09
 Space group P 31 2 1
 Crystal system trigonal (hexagonal axes)
 Unit cell a= 4.5940 Å c= 5.2000 Å
 I/Ic 2.68
 Calc. density 3.149 g/cm³
 Reference Hazen R. M., Finger L. W., Hemley R. J., Mao H. K., "High-pressure crystal chemistry and amorphization of alpha-quartzSample: P = 9.5 GPa", Solid State Communications **72**, 507-511 (1989)

D: Iron oxide (0.93/1)
Wuestite (17.2 %)

Formula sum Fe_{0.932} O
 Entry number 96-101-1167
 Figure-of-Merit (FoM) 0.000000
 Total number of peaks 10
 Peaks in range 10
 Peaks matched 2
 Intensity scale factor 0.76
 Space group F m -3 m
 Crystal system cubic
 Unit cell a= 4.2909 Å
 I/Ic 5.54
 Meas. density 5.660 g/cm³
 Calc. density 5.721 g/cm³
 Reference Jette E R., Foote F., "An x-ray study of the wuestite (Fe O) solid solutions", Journal of Chemical Physics **1**, 29-36 (1933)

E: Fayalite (39.6 %)*

Formula sum Fe₂ O₄ Si
 Entry number 96-901-1589
 Figure-of-Merit (FoM) 0.000000
 Total number of peaks 378
 Peaks in range 378
 Peaks matched 30
 Intensity scale factor 0.54
 Space group P b n m
 Crystal system orthorhombic
 Unit cell a= 4.8220 Å b= 10.4880 Å c= 6.0940 Å
 I/Ic 1.70
 Calc. density 4.392 g/cm³
 Reference Kudoh Y., Takeda H., "Single crystal X-ray diffraction study on the bond compressibility of fayalite, Fe₂-SiO₄- and rutile, TiO₂- under high pressureSample: P = 0.001 kbar", Physica B+C **140**, 333-336 (1986)

(*2theta values have been shifted internally for the calculation of the amounts, the intensity scaling factors as well as the figure-of-merit (FoM), due to the active search-match option 'Automatic zero point adaption'.

Candidates

Name	Formula	Entry No.	FoM
	Fe ₂ Si	96-901-4529	0.7055
	Fe Sb	96-900-8895	0.7030
Dolomite	C Ca _{0.5} Mg _{0.5} O ₃	96-900-3521	0.6855
Sr ₃ Sn ₂ O ₇	O ₇ Sn ₂ Sr ₃	96-152-1095	0.6829
Dolomite	C Ca _{0.5} Mg _{0.5} O ₃	96-900-3520	0.6819
Dolomite	C Ca _{0.5} Mg _{0.5} O ₃	96-900-3522	0.6800
Zr ₅₀ Sc ₁₂ O ₁₁₈	O ₁₁₈ Sc ₁₂ Zr ₅₀	96-153-6706	0.6763
SrSiO ₃ (SrSiO ₃ cubic perovskite at 37.8 GPa)	O ₃ Si Sr	96-155-7931	0.6735
Dolomite	C ₂ Ca _{1.14} Mg _{0.86} O ₆	96-900-4934	0.6730
Dolomite	C ₂ Ca Mg O ₆	96-900-0084	0.6711
	Ni Sn	96-900-8906	0.6669
Dolomite	C ₂ Ca Mg O ₆	96-900-1007	0.6665
Dolomite	C ₂ Ca Mg O ₆	96-900-1011	0.6665
Ba ₂ Nb (Nb _{2.5} V _{1.5}) O ₉	Ba ₂ Nb _{3.5} O ₉ V _{1.5}	96-153-1604	0.6661
Ag _{3.5} S I	Ag _{3.5} I S	96-150-9831	0.6647
Dolomite	C ₂ Ca Fe _{0.33} Mg _{0.67} O ₆	96-900-4935	0.6641
Dolomite	C ₂ Ca _{1.13} Mg _{0.87} O ₆	96-900-4932	0.6631
Ankerite	C ₂ Ca _{1.007} Fe _{0.542} Mg _{0.451} O ₆	96-900-1247	0.6616
Dolomite	C ₂ Ca Mg O ₆	96-900-0106	0.6600
Dolomite	C Ca _{0.5} Mg _{0.5} O ₃	96-900-0888	0.6589
Dolomite	C Ca _{0.5} Mg _{0.5} O ₃	96-900-3524	0.6568
Magnesium Calcium Carbonate (.1/1.9/1) (Dolomite)	C ₂ Ca Mg O ₆	96-151-7797	0.6555
Calcium magnesium cobalt dicarbonate	C ₂ Ca Co _{0.17} Mg _{0.83} O ₆	96-224-0440	0.6551
Calcium Magnesium Carbonate (Dolomite)	C ₂ Ca Mg O ₆	96-210-5964	0.6539
Dolomite	C ₂ Ca _{1.07} Mg _{0.93} O ₆	96-900-4933	0.6536
Dolomite	C ₂ Ca Mg O ₆	96-900-1006	0.6528
Dolomite	C ₂ Ca Mg O ₆	96-900-1010	0.6528
	U	96-153-9737	0.6527
lead hafnate titanate	Hf _{0.8} O ₃ Pb Ti _{0.2}	96-210-2004	0.6521
Dolomite	C ₂ Ca _{1.08} Mg _{0.92} O ₆	96-900-4929	0.6519
Dolomite	C ₂ Ca Fe _{0.05} Mg _{0.94} Mn _{0.01} O ₆	96-901-7357	0.6517
Dolomite	C ₂ Ca _{1.07} Mg _{0.93} O ₆	96-900-4931	0.6512
Calcium magnesium carbonate (Dolomite)	C ₂ Ca Mg O ₆	96-120-0015	0.6510
Calcium magnesium carbonate (Dolomite)	C ₂ Ca Mg O ₆	96-500-0117	0.6510
Dolomite	C ₂ Ca Fe _{0.05} Mg _{0.94} Mn _{0.01} O ₆	96-900-9593	0.6510
Dolomite	C ₂ Ca Mg O ₆	96-900-1044	0.6499
Dolomite	C Ca _{0.5} Mg _{0.5} O ₃	96-900-3526	0.6497
Dolomite	C ₂ Ca _{0.997} Fe _{0.234} Mg _{0.769} O ₆	96-900-1246	0.6469
	Ba Co _{0.4} Fe _{0.4} O _{2.426} Zr _{0.2}	96-156-7215	0.6434
Silver selenide - S-alpha	Ag ₂ Se	96-101-1339	0.6430
Cu ₁₅ (B ₂ O ₅) ₂ (B O ₃) ₆ O ₂	B ₁₀ Cu ₁₅ O ₃₀	96-210-5419	0.6423
Ba (Sn O ₃)	Ba O ₃ Sn	96-153-8371	0.6415
	Au Rb	96-151-0281	0.6397
barium tantalum oxynitride	Ba N _{0.76} O _{2.24} Ta	96-451-9034	0.6393
	Fe ₂ O ₇ P ₂	96-400-0292	0.6384
(Ga Pu)	Ga Pu	96-152-3831	0.6375
barium tantalum oxynitride	Ba N _{0.58} O _{2.42} Ta	96-451-9033	0.6372
	Li Pb	96-152-2615	0.6357
Ankerite	C ₂ Ca _{0.997} Fe _{0.676} Mg _{0.273} Mn _{0.054} O ₆	96-900-1413	0.6350
Silver niobium sulfide (0.6/1/2)	Ag _{0.6} Nb S ₂	96-150-9008	0.6348
Lead Barium Zirconium Titanium Oxide	Ba _{0.3} O ₃ Pb _{0.7} Ti _{0.35} Zr _{0.65}	96-210-2952	0.6342
	Ba Li _{0.2} N _{0.19} O _{2.81} Ta _{0.8}	96-451-2486	0.6339

and 1064 others...

Search-Match

Settings
 Reference database used COD-Inorg 2023.06.06
 Automatic zeropoint adaptation Yes

5	31.66	2.8238	536.21	19.98	0.2370	E
6	34.10	2.6272	173.12	10.47	0.3847	E
7	35.04	2.5588	390.79	26.37	0.4294	E
8	35.98	2.4941	1000.00	102.31	0.6509	E
9	36.44	2.4636	689.28	38.41	0.3545	A,B,D
10	37.38	2.4038	141.31	9.77	0.4400	E
11	39.14	2.2997	127.13	15.78	0.7898	C,E
12	41.27	2.1859	67.45	4.39	0.4138	C,E
13	43.80	2.0652	783.48	33.88	0.2751	A,E
14	44.60	2.0299	323.08	32.25	0.6350	B
15	49.55	1.8380	74.28	5.08	0.4354	E
16	51.02	1.7886	208.29	8.37	0.2558	
17	52.00	1.7573	72.07	6.97	0.6150	E
18	54.76	1.6750	98.96	22.05	1.4174	A,E
19	58.28	1.5820	156.17	21.56	0.8783	A,C,E
20	58.80	1.5693	157.65	10.18	0.4109	B
21	61.02	1.5173	115.73	13.79	0.7579	D,E
22	64.23	1.4490	208.48	43.29	1.3211	A,E
23	64.54	1.4428	133.52	3.82	0.1822	C,E

Integrated Profile Areas

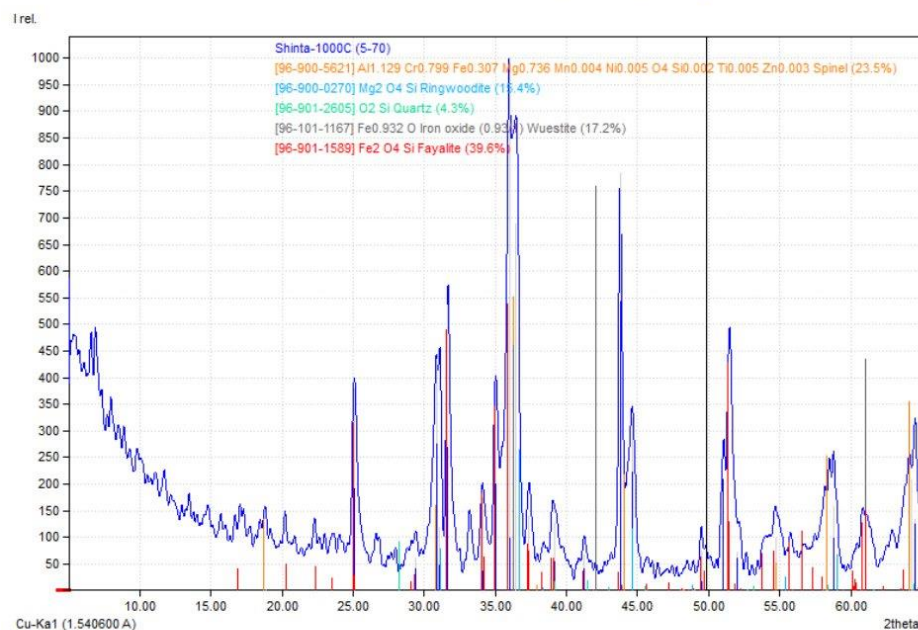
Based on calculated profile

Profile area	Counts	Amount
Overall diffraction profile	62715	100.00%
Background radiation	35808	57.10%
Diffraction peaks	26907	42.90%
Peak area belonging to selected phases	22644	36.11%
Peak area of phase A (Spinel)	5833	9.30%
Peak area of phase B (Ringwoodite)	2362	3.77%
Peak area of phase C (Quartz)	406	0.65%
Peak area of phase D (Iron oxide (0.93/1) Wuestite)	2173	3.47%
Peak area of phase E (Fayalite)	11869	18.93%
Unidentified peak area	4263	6.80%

Peak Residuals

Peak data	Counts	Amount
Overall peak intensity	517	100.00%
Peak intensity belonging to selected phases	368	71.16%
Unidentified peak intensity	149	28.84%

Diffraction Pattern Graphics



LAMPIRAN 2
HASIL ANALISIS *X-RAY FLUORESCENCE* (XRF)

HASIL ANALISIS XRF

Sample id	Kadar Unsur/ Senyawaan yang dianalisa sesuai dengan komoditi (%)													
Element Dimension	Ni	Co	Fe	Cr	Na ₂ O	MgO	Al ₂ O ₃	SiO ₂	K ₂ O	CaO	TiO ₂	Cr ₂ O ₃	MnO	Fe ₂ O ₃
Detection Limit	0,005	0,001	0,01	0,005	0,01	0,01	0,01	0,01	0,001	0,003	0,01	0,005	0,01	0,01
Method	WDXRF	WDXRF	WDXRF	WDXRF	WDXRF	WDXRF	WDXRF	WDXRF	WDXRF	WDXRF	WDXRF	WDXRF	WDXRF	WDXRF
Unit	%	%	%	%	%	%	%	%	%	%	%	%	%	%
DS 001 ORI	1,52	0,03	37,47	2,03	0,01	2,63	10,69	12,16	0,00	0,06	0,23	2,97	0,45	53,59
DS 002 ORI	1,60	0,05	39,82	2,17	0,03	3,27	12,67	14,72	0,29	0,06	0,24	3,17	0,63	56,95
DS 003 ORI	1,51	0,04	40,17	2,13	0,02	2,99	12,92	13,79	0,29	0,09	0,24	3,11	0,59	57,45
DS 004 ORI	1,41	0,05	38,97	1,94	0,02	2,92	12,75	13,45	0,27	0,08	0,24	2,84	0,63	55,72
DS 005 ORI	1,63	0,05	41,19	2,24	0,01	3,63	13,48	15,42	0,29	0,07	0,25	3,27	0,71	58,90
DS 006 ORI	1,52	0,04	41,20	2,11	0,03	3,04	12,81	13,85	0,28	0,08	0,25	3,09	0,60	58,91
DS 007 ORI	1,51	0,05	40,97	2,11	0,03	3,13	13,55	14,24	0,28	0,07	0,26	3,08	0,61	58,59
DS 008 ORI	1,74	0,06	42,87	2,40	0,02	3,83	14,42	16,48	0,26	0,06	0,27	3,51	0,75	61,31
DS 009 ORI	1,71	0,05	43,58	2,36	0,05	3,50	14,43	15,59	0,22	0,07	0,27	3,45	0,63	62,31
DS 010 ORI	1,64	0,04	46,08	2,39	0,06	3,65	14,56	15,69	0,19	0,08	0,29	3,50	0,62	65,89
DS 011 ORI	1,63	0,09	44,95	2,49	0,08	4,91	16,56	16,34	0,24	0,06	0,29	3,64	1,30	64,28
DS 012 ORI	1,73	0,04	47,98	2,53	0,05	4,01	15,39	16,50	0,26	0,07	0,29	3,70	0,67	68,62
DS 013 ORI	1,66	0,04	47,01	2,46	0,12	3,78	14,99	15,87	0,27	0,08	0,30	3,60	0,60	67,22

LAMPIRAN 3
PERHITUNGAN *RECOVERY*

A. Nikel

Suhu (°C)	Ukuran fraksi (Mesh)	Kadar awal Ni (%)	Berat sampel awal + reduktor (gr)	Berat setelah roasting (gr)	Kadar akhir Ni (%)	Recovery Ni (%)
800	100	1,52	20	16,1	1,60	84,58
	150	1,52	20	16,0	1,51	79,41
	200	1,52	20	16,1	1,41	74,47
900	100	1,52	20	15,4	1,63	82,58
	150	1,52	20	15,2	1,52	76,25
	200	1,52	20	15,5	1,51	76,89
1000	100	1,52	20	14,6	1,74	83,36
	150	1,52	20	14,5	1,71	81,76
	200	1,52	20	14,4	1,64	77,60
1100	100	1,52	20	13,5	1,63	72,35
	150	1,52	20	13,6	1,73	77,23
	200	1,52	20	13,3	1,66	72,36

Recovery Ni dihitung menggunakan rumus sebagai berikut:

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

1. Recovery Ni pada suhu 800°C menggunakan fraksi 100 mesh

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{16,1 \text{ (gr)} \times 1,60 \text{ (\%)}}{20 \text{ (gr)} \times 1,52 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 84,58\%$$

2. Recovery Ni pada suhu 800°C menggunakan fraksi 150 mesh

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{16 \text{ (gr)} \times 1,51 \text{ (\%)}}{20 \text{ (gr)} \times 1,52 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 79,41\%$$

3. Recovery Ni pada suhu 800°C menggunakan fraksi 200 mesh

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{16,1 \text{ (gr)} \times 1,41 \text{ (\%)}}{20 \text{ (gr)} \times 1,52 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 74,47\%$$

4. *Recovery Ni pada suhu 900°C menggunakan fraksi 100 mesh*

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{15,4 \text{ (gr)} \times 1,63 \text{ (\%)}}{20 \text{ (gr)} \times 1,52 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 82,58\%$$

5. *Recovery Ni pada suhu 900°C menggunakan fraksi 150 mesh*

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{15,2 \text{ (gr)} \times 1,52 \text{ (\%)}}{20 \text{ (gr)} \times 1,52 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 76,25\%$$

6. *Recovery Ni pada suhu 900°C menggunakan fraksi 200 mesh*

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{15,5 \text{ (gr)} \times 1,51 \text{ (\%)}}{20 \text{ (gr)} \times 1,52 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 76,89\%$$

7. *Recovery Ni pada suhu 1000°C menggunakan fraksi 100 mesh*

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{14,6 \text{ (gr)} \times 1,74 \text{ (\%)}}{20 \text{ (gr)} \times 1,52 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 83,36\%$$

8. *Recovery Ni pada suhu 1000°C menggunakan fraksi 150 mesh*

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{14,5 \text{ (gr)} \times 1,71 \text{ (\%)}}{20 \text{ (gr)} \times 1,52 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 81,76\%$$

9. *Recovery Ni pada suhu 1000°C menggunakan fraksi 200 mesh*

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{14,4 \text{ (gr)} \times 1,64 \text{ (\%)}}{20 \text{ (gr)} \times 1,52 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 77,60\%$$

10. *Recovery Ni pada suhu 1100°C menggunakan fraksi 100 mesh*

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{13,5 \text{ (gr)} \times 1,63 \text{ (\%)}}{20 \text{ (gr)} \times 1,52 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 72,35\%$$

11. Recovery Ni pada suhu 1100°C menggunakan fraksi 150 mesh

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{13,6 \text{ (gr)} \times 1,63 \text{ (\%)}}{20 \text{ (gr)} \times 1,52 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 77,23\%$$

12. Recovery Ni pada suhu 1100°C menggunakan fraksi 150 mesh

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Ni}}{\text{Berat sampel awal} \times \text{kadar awal Ni}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{13,3 \text{ (gr)} \times 1,66 \text{ (\%)}}{20 \text{ (gr)} \times 1,52 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 72,36\%$$

B. Iron

Suhu (°C)	Ukuran fraksi (Mesh)	Kadar awal Fe (%)	Berat awal sampel + reduktor (gr)	Berat sampel akhir (gr)	Kadar akhir Fe (%)	Recovery Fe (%)
800	100	37,47	20	16,1	39,82	85,40
	150	37,47	20	16,0	40,17	85,70
	200	37,47	20	16,1	38,97	83,49
900	100	37,47	20	15,4	41,19	84,65
	150	37,47	20	15,2	41,20	83,84
	200	37,47	20	15,5	40,97	84,63
1000	100	37,47	20	14,6	42,87	83,31
	150	37,47	20	14,5	43,58	84,53
	200	37,47	20	14,4	46,08	88,45
1100	100	37,47	20	13,5	44,95	80,94
	150	37,47	20	13,6	47,98	86,89
	200	37,47	20	13,3	47,01	83,12

Recovery Fe dihitung menggunakan rumus sebagai berikut:

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

1. Recovery Fe pada suhu 800°C menggunakan fraksi 100 mesh

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{16,1 \text{ (gr)} \times 39,82 \text{ (\%)}}{20 \text{ (gr)} \times 37,47 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 85,40\%$$

2. Recovery Fe pada suhu 800°C menggunakan fraksi 150 mesh

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{16 \text{ (gr)} \times 40,17 \text{ (\%)}}{20 \text{ (gr)} \times 37,47 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 85,70\%$$

3. Recovery Fe pada suhu 800°C menggunakan fraksi 200 mesh

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{16,1 \text{ (gr)} \times 38,97 \text{ (\%)}}{20 \text{ (gr)} \times 37,47 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 83,49\%$$

4. Recovery Fe pada suhu 900°C menggunakan fraksi 100 mesh

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{15,4 \text{ (gr)} \times 41,19 \text{ (\%)}}{20 \text{ (gr)} \times 37,47 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 84,65\%$$

5. Recovery Fe pada suhu 900°C menggunakan fraksi 150 mesh

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{15,2 \text{ (gr)} \times 41,20 \text{ (\%)}}{20 \text{ (gr)} \times 37,47 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 83,84\%$$

6. Recovery Fe pada suhu 900°C menggunakan fraksi 200 mesh

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{15,5 \text{ (gr)} \times 40,97 \text{ (\%)}}{20 \text{ (gr)} \times 37,47 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 83,63\%$$

7. Recovery Fe pada suhu 1000°C menggunakan fraksi 100 mesh

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanggangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{14,6 \text{ (gr)} \times 42,87 \text{ (\%)}}{20 \text{ (gr)} \times 37,47 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 83,31\%$$

8. *Recovery Fe pada suhu 1000°C menggunakan fraksi 150 mesh*

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanngangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{14,5 \text{ (gr)} \times 43,58 \text{ (\%)}}{20 \text{ (gr)} \times 37,47 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 84,53\%$$

9. *Recovery Fe pada suhu 1000°C menggunakan fraksi 200 mesh*

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanngangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{14,4 \text{ (gr)} \times 46,08 \text{ (\%)}}{20 \text{ (gr)} \times 37,47 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 88,45\%$$

10. *Recovery Fe pada suhu 1100°C menggunakan fraksi 100 mesh*

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanngangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{13,5 \text{ (gr)} \times 44,95 \text{ (\%)}}{20 \text{ (gr)} \times 37,47 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 80,94\%$$

11. *Recovery Fe pada suhu 1100°C menggunakan fraksi 150 mesh*

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanngangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{13,6 \text{ (gr)} \times 47,98 \text{ (\%)}}{20 \text{ (gr)} \times 37,47 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 86,89\%$$

12. *Recovery Fe pada suhu 1100°C menggunakan fraksi 200 mesh*

$$\text{Recovery (\%)} = \frac{\text{Berat sampel setelah pemanngangan} \times \text{kadar akhir Fe}}{\text{Berat sampel awal} \times \text{kadar awal Fe}} \times 100\%$$

$$\text{Recovery (\%)} = \frac{13,3 \text{ (gr)} \times 47,01 \text{ (\%)}}{20 \text{ (gr)} \times 37,47 \text{ (\%)}} \times 100\%$$

$$\text{Recovery (\%)} = 83,12\%$$