

DAFTAR PUSTAKA

- Alfirdaus, Ade Putra. dkk. (2019) *Evaluasi Teknis Penggunaan Kolom Komposit Baja Beton Pada Bangunan Bertingkat Banyak*, 8 (2): 286. Tersedia di: <https://ejournal.unsrat.ac.id/index.php/jss/article/view/22799/22496>
- Giatmajaya, Wayan. dkk. (2021) *Perencanaan Struktur Komposit Baja-Beton Dengan Metode LRFD (Load And Resistance Factor Design) Ruang Kelas Lantai III SMK PARIWISATA LABUAN BAJO-FLORES NTT*, 3 (2): 53. Tersedia di: https://www.researchgate.net/publication/344697962_Perencanaan_Struktur_Komposit_Baja-Beton_Dengan_Metode_Lrfd_Load_And_Resistance_Factor_Design_Ruang_Kelas_Lantai_Iii_Smk_Pariwisata_Labuan_Bajo_-_Flores_-_Ntt
- Dai, L., Wang, L., Zhang, J. and Zhang, X. (2015) ‘A global model for corrosion-induced cracking in prestressed concrete structures’, *Engineering Failure Analysis*, 62, pp. 263–275. Available at: <https://doi.org/10.1016/j.engfailanal.2016.01.013>.
- Djamaluddin, R. and Irmawaty, R. (2017) ‘Relationship Model of the Moment Capacity of GFRP Sheet Strengthened RC Beams to the Duration of Sea Water Exposure’, in *Procedia Engineering*. Elsevier Ltd, pp. 1195–1202. Available at: <https://doi.org/10.1016/j.proeng.2017.04.280>.
- Idris, M., Parung, H. and Djamaluddin, R. (2019) ‘Flexural Behavior of Shear-Cracked Reinforced Concrete Beam Strengthened with GFRP Sheet’, *International Journal of Civil Engineering and Technology (IJCIET)*, 10(10), pp. 64–72. Available at: <http://www.iaeme.com/IJCIET/index.asp64http://www.iaeme.com/ijciet/issues.asp?JType=IJCIET&VType=10&IType=10http://www.iaeme.com/IJCIET/index.asp65http://www.iaeme.com/IJCIET/issues.asp?JType=IJCIET&VType=10&IType=10>.
- Luckai, J. (2011) *Evaluating the Effects of Spalling on the Capacity of Reinforced Concrete Bridge Girders*. University of Waterloo. Available at: https://uwspace.uwaterloo.ca/bitstream/handle/10012/6229/Luckai_Jeffrey.pdf;sequence=1 (Accessed: 23 February 2023).
- Moccia, F., Fernández Ruiz, M. and Muttoni, A. (2021) ‘Spalling of concrete cover induced by reinforcement’, *Engineering Structures*, 237. Available at: <https://doi.org/10.1016/j.engstruct.2021.112188>.
- Qiao, D., Nakamura, H., Kim Tran, K., Yamamoto, Y., Miura, T. and Professor, A. (2015) *Experimental and analytical evaluation of concrete cover spalling behavior due to local corrosion*, *Journal of Structural Engineering*.
- Tata, A., Raffel, A.F., Ihsan, M. and Djamaluddin, R. (2018) *Fatigue Flexural Behavior of RC Beams Strengthened using GFRP-Sheet After Seawater Immersion*.

Wang, L., Zhang, X., Zhang, J., Ma, Y., Xiang, Y. and Liu, Y. (2014) ‘Effect of insufficient grouting and strand corrosion on flexural behavior of PC beams’, *Construction and Building Materials*, 53, pp. 213–224. Available at: <https://doi.org/10.1016/j.conbuildmat.2013.11.069>.

Zandi, K. (2015) ‘Corrosion-induced cover spalling and anchorage capacity’, *Structure and Infrastructure Engineering*, 11(12), pp. 1547–1564. Available at: <https://doi.org/10.1080/15732479.2014.979836>.

. Shen et al., (2021) Korosi baja pada beton akan cepat terjadi di lingkungan yang keras, seperti daerah pesisir, tropis, atau gurun di mana kadar garam yang tinggi dan suhu ekstrim mempercepat laju pembusukannya.

Proses inisiasi korosi pada beton bertulang akibat infiltrasi klorida dimulai Ketika klorida masuk ke dalam beton dan merusak lapisan pasif tulangan (Kolio et al., 2015).

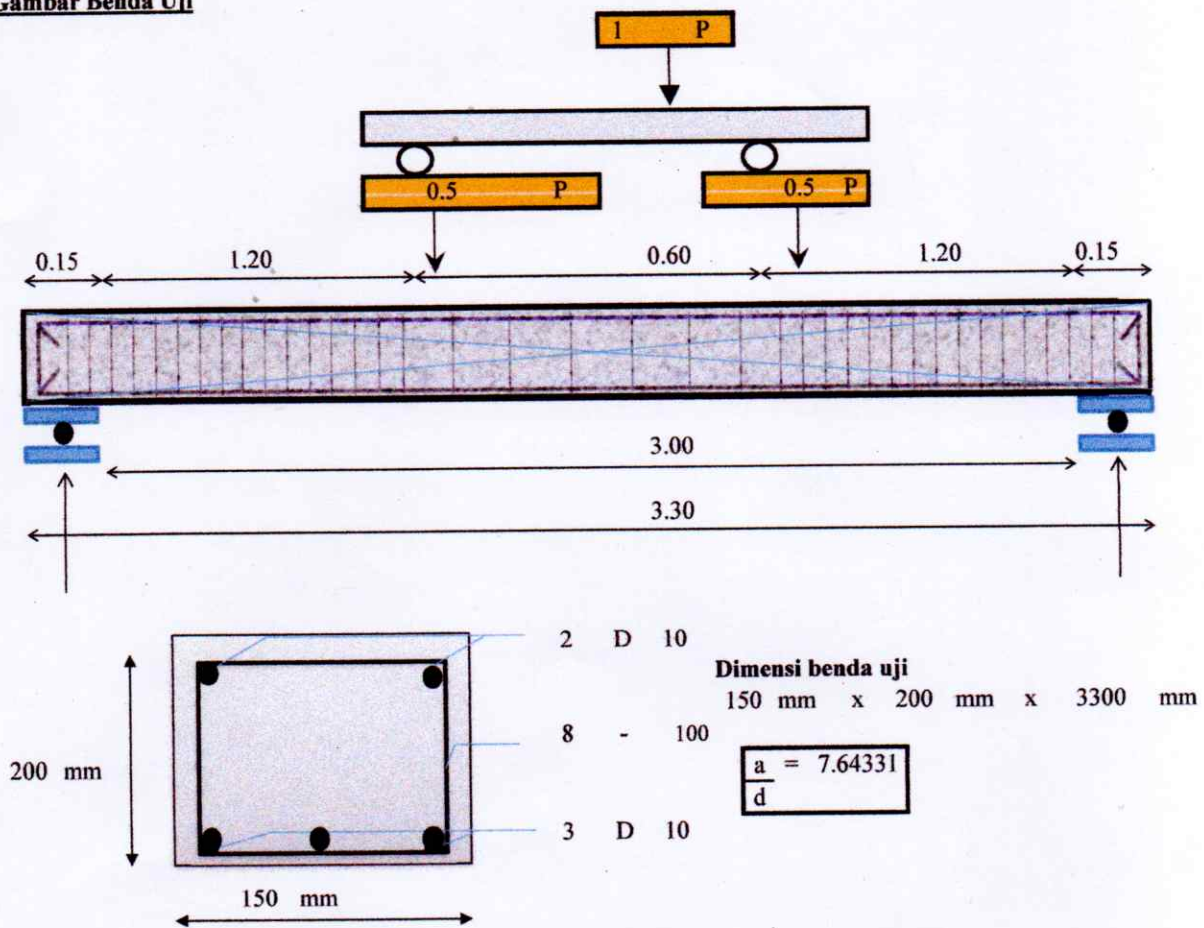
Spalling pada penutup beton merupakan fenomena kompleks yang mempengaruhi tidak hanya keadaan batas ultimit dari komponen struktur beton, tetapi juga respon layanan dan daya tahannya (Moccia, 2021).

R. Irmawaty, Fakhruddin, and J. J. Ekaputri, Experimental and analytical study for shear *strengthening* of reinforced-concrete *beams* using a prefabricated geopolymer–mortar panel, *Case Stud. Constr. Mater.*, vol. 17, no. July (2022) p. e01568, doi: 10.1016/j.cscm.2022.e01568.
serta kerusakan konstruksi yang akan lebih banyak menimbulkan biaya

LAMPIRAN

ANALISA PENDAHULUAN

Gambar Benda Uji



Menurut SK SNI - 03 - 2847 - 2002 (hal 63) , perencanaan tinggi balok minimum (h) dengan mutu baja 400 Mpa, adalah:

- balok dengan dua tumpuan sederhana

$$h = \frac{L}{16}$$

$$= \frac{3000}{16.0}$$

$$= 188 \text{ mm} \approx 200 \text{ mm}$$

$$b = \frac{d}{1.5} = \frac{157}{1.5} = 104.667 \text{ mm} \approx 150 \text{ mm}$$

Data Penampang

Dimensi balok (B x H) = 150 mm x 200 mm
 Tulangan tarik 3 D 10
 Tulangan tekan 2 D 10

Data Material

Kuat tekan beton $f_c = 23.4$ MPa
 Kuat leleh baja $f_y = 280$ MPa

Data Analisis

Kuat tekan beton $f_c = 23.4$ MPa
 Kuat leleh tulangan tarik $f_y = 280$ MPa
 Kuat leleh tulangan tekan $f_y = 280$ MPa
 Kuat leleh tulangan transversal $f_y = 280$ MPa
 Modulus elastisitas beton $E_c = 22711.2637$ MPa
 Modulus elastisitas baja $E_s = 200000$ MPa
 Modulus keruntuhan $f_r = 0.7 f_c^{0.5} = 3.38$ MPa
 Berat jenis beton $g_c = 2400$ kg/m³
 Lebar penampang $b = 150$ mm
 Tinggi penampang $h = 200$ mm
 Tinggi efektif penampang $d = 157.00$ mm
 Jarak tulangan tekan ke serat tekan terluar $d' = 43.00$ mm
 Beban berat sendiri balok $q = 0.07$ t/m¹ = 0.72 kN/m¹
 Berat benda uji $W = 0.24$ t = 237.60 kg
 Luas tulangan tarik $A_s = 3 \text{ D } 10 = 235.62 \text{ mm}^2$
 Luas tulangan tekan $A_s' = 2 \text{ D } 10 = 157.08 \text{ mm}^2$
 Luas tulangan sengkang $A_{sv} = 2 \text{ D } 8 = 100.53 \text{ mm}^2$
 Angka ekuivalensi beton terhadap baja $n = \frac{E_s}{E_c} = 8.81$; $nf = \frac{E_f}{E_c} = 3.553$

Perhitungan nilai d_s , d , d' dan d_d

$$d_s = 30 + 8 + \frac{10}{2}$$

$$d = 200 - 43$$

$$d' = 30 + 8 + \frac{10}{2}$$

$$d_d = 200 - 30 - 8 - \frac{10}{2}$$

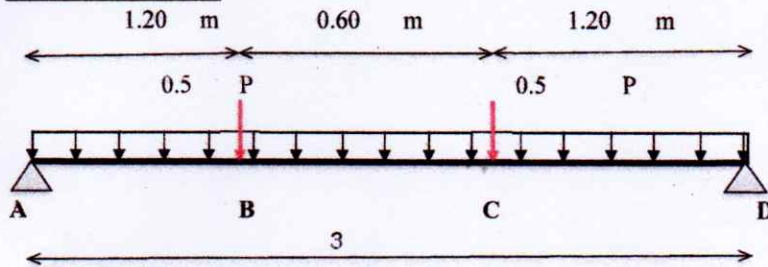
$$d_s = 43.0 \text{ mm}$$

$$d = 157 \text{ mm}$$

$$d' = 43 \text{ mm}$$

$$d_d = 157 \text{ mm}$$

Statika Gaya Dalam



$$\begin{aligned} q &= 0.15 \cdot 0.2 \cdot 2.4 \\ &= 0.072 \text{ t/m} \\ &= 0.72 \text{ kN/m} \end{aligned}$$

*gambar dalam satuan meter

$$V_A = V_D = 0.5 P + \frac{1}{2} \cdot 0.72 \cdot 3$$

$$= 0.5 P + 1.08 \text{ kN}$$

$$\begin{aligned} M_{\text{maks di tengah bentang}} &= -\frac{1}{2} \cdot 0.72 \cdot 1.5^2 + (0.5 P + 1.08) \cdot 1.5 \\ &\quad - 0.5 P \cdot 0.3 \end{aligned}$$

$$\begin{aligned} M_{\text{maks di tengah bentang}} &= -0.81 + 0.75 P + 1.62 - 0.15 P \\ &= 0.81 + 0.6 P \text{ kN.m} \end{aligned}$$

$M_{\text{maks di tengah bentang}}$	$=$	$0.81 + 0.6 P$	kN.m
-------------------------------------	-----	----------------	---------------

Bila digunakan satuan t.m maka :

$$V_A = V_D = 0.5 P + \frac{1}{2} \cdot 0.072 \cdot 3$$

$$= 0.5 P + 0.108 \text{ ton}$$

$$\begin{aligned} M_{\text{maks pada tengah bentang}} &= -\frac{1}{2} \cdot 0.072 \cdot 1.5^2 + (0.5 P + 0.108) \cdot 1.5 \\ &\quad - 0.5 P \cdot 0.3 \end{aligned}$$

$$\begin{aligned} &= -0.081 + 0.75 P + 0.162 - 0.15 P \\ &= 0.081 + 0.6 P \text{ t.m} \end{aligned}$$

$M_{\text{maks pada tengah bentang}}$	$=$	$0.081 + 0.6 P$	t.m
---------------------------------------	-----	-----------------	--------------

Geser yang terjadi

AB (0.00 ≤ x ≤ 1.20)

$$\begin{aligned}
 M_x &= -0.5 q x^2 + (0.5 P + 0.108) (x - 0.00) \\
 &= -0.5 \cdot 0.072 x^2 + 0.5 P x - 0 P + 0.108 x - 0 \\
 &= -0.036 x^2 + 0.5 P x + 0.108 x - 0 P - 0 \\
 M_{0.00} &= 0 + 0 P \text{ t.m} \\
 M_{1.20} &= 0.07776 + 0.6 P \text{ t.m}
 \end{aligned}$$

$$\begin{aligned}
 V_x &= -0.072 x + 0.5 P + 0.108 \\
 V_{0.00} &= 0.108 + 0.5 P \text{ ton} \\
 V_{1.20} &= 0.0216 + 0.5 P \text{ ton}
 \end{aligned}$$

BC (1.20 ≤ x ≤ 1.80)

$$\begin{aligned}
 M_x &= -0.036 x^2 + 0.5 P x + 0.108 x - 0 P - 0 \\
 &\quad - 0.5 P (x - 1.20) \\
 &= -0.036 x^2 + 0 P x + 0.108 x - -0.6 P - 0 \\
 M_{1.20} &= 0.07776 + 0.6 P \text{ t.m} \\
 M_{1.80} &= 0.07776 + 0.6 P \text{ t.m}
 \end{aligned}$$

$$\begin{aligned}
 \max \quad ; \quad -0.072 x + 0 P + 0.108 &= 0 \\
 x &= 1.5 \text{ m}
 \end{aligned}$$

$$M_{1.50} = 0.081 + 0.6 P \text{ t.m}$$

$$\begin{aligned}
 V_x &= -0.072 x + 0 P + 0.108 \\
 V_{1.20} &= 0.0216 + 0 P \text{ ton} \\
 V_{1.80} &= -0.0216 + 0 P \text{ ton}
 \end{aligned}$$

CD (1.80 ≤ x ≤ 3.00)

$$\begin{aligned}
 M_x &= -0.036 x^2 + 0 P x + 0.108 x - -0.6 P - 0 \\
 &\quad - 0.5 P (x - 1.80) \\
 &= -0.036 x^2 + -0.5 P x + 0.108 x - -1.5 P - 0 \\
 M_{1.80} &= 0.07776 + 0.6 P \text{ t.m} \\
 M_{3.00} &= 0 + 0 P \text{ t.m}
 \end{aligned}$$

$$\begin{aligned}
 V_x &= -0.072 x + -0.5 P + 0.108 \\
 V_{1.80} &= -0.0216 + -0.5 P \text{ ton} \\
 V_{3.00} &= -0.108 + -0.5 P \text{ ton}
 \end{aligned}$$

