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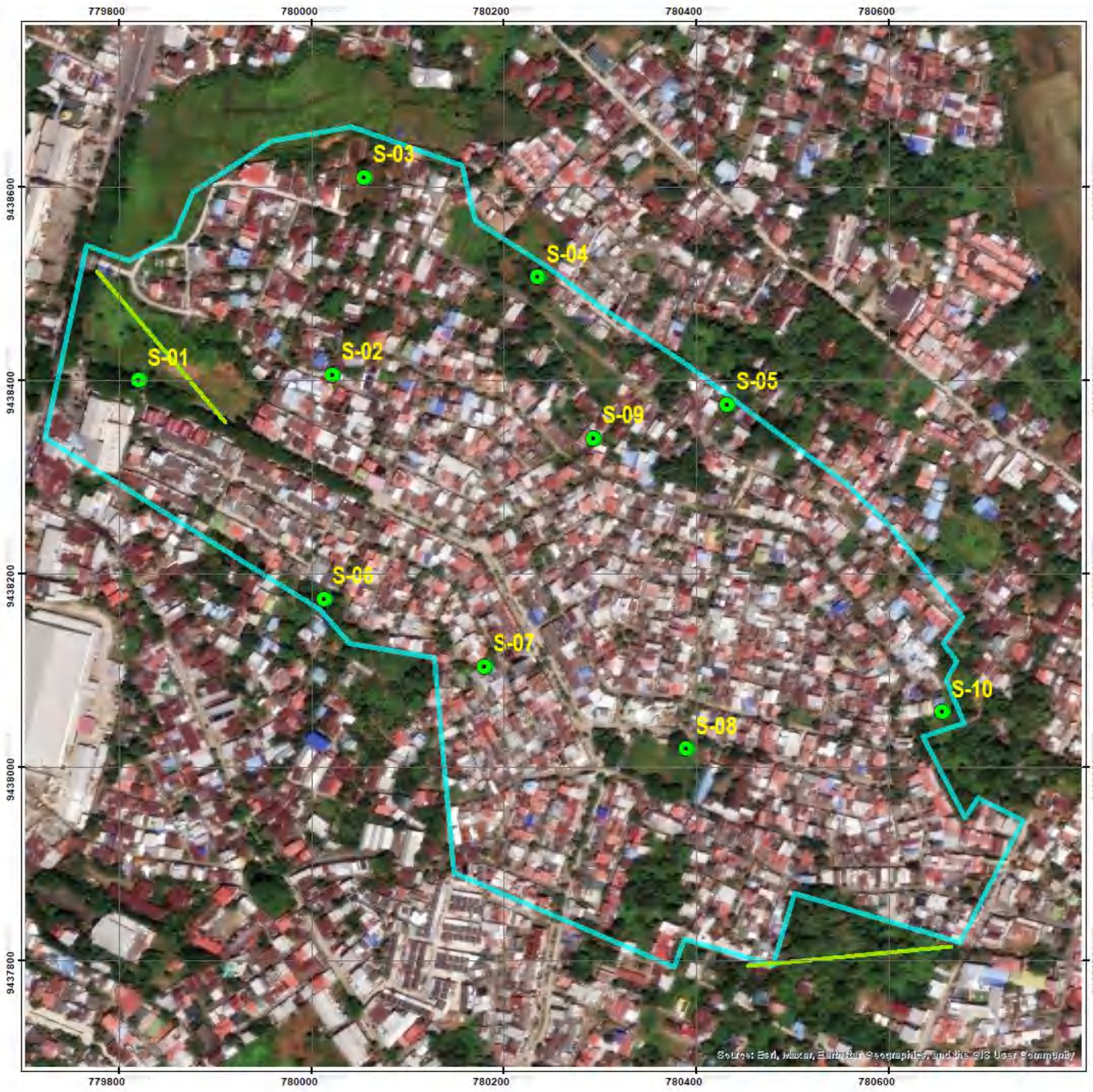
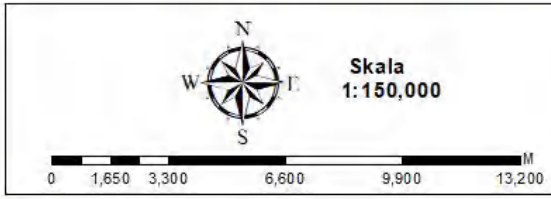
# LAMPIRAN

# LAMPIRAN A
# PETA LOKASI PENELITIAN

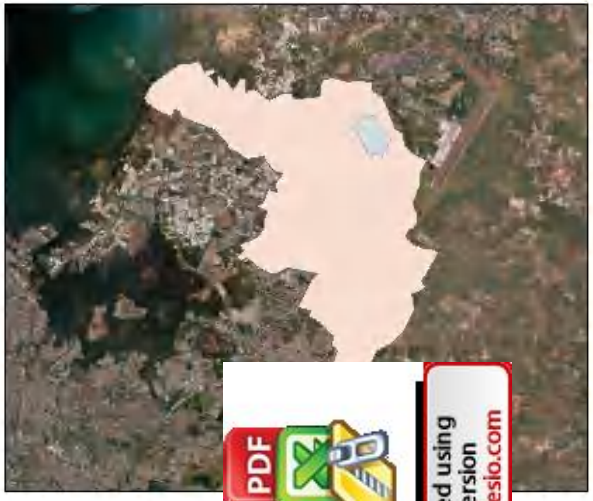
# PETA DAERAH PENELITIAN BUMI PERMATA SUDIANG




## Legend

- Titik Pengukuran Laju Infiltrasi
- Lintasan Geolistrik
- Bumi Permata Sudiang





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# LAMPIRAN B
# PETA GEOLOGI LOKASI PENELITIAN

# PETA GEOLOGI
# LOKASI PENELITIAN

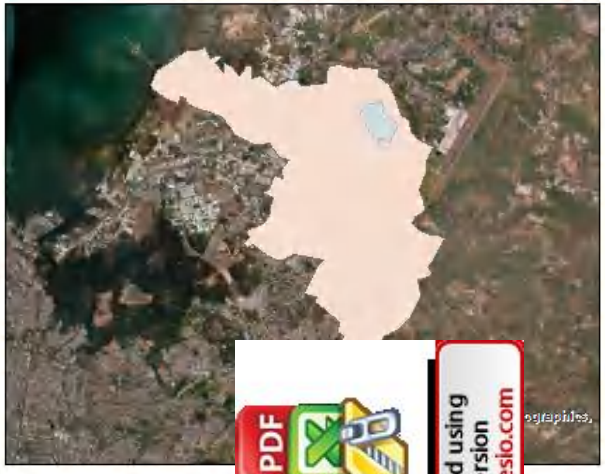

N
W E
S

Skala
1:150,000

0 1,650 3,300 6,600 9,900 13,200 M

## Legend

- Kontur
- Laut
- Bumi Permata Sudiang
- Formasi Tonasa (Temt)
- Formasi Salo Kalupang (Teos)
- Endapan Aluvium (Qac)
- Formasi Camba (Tmc)
- Basal dan Retas Basal (b1)





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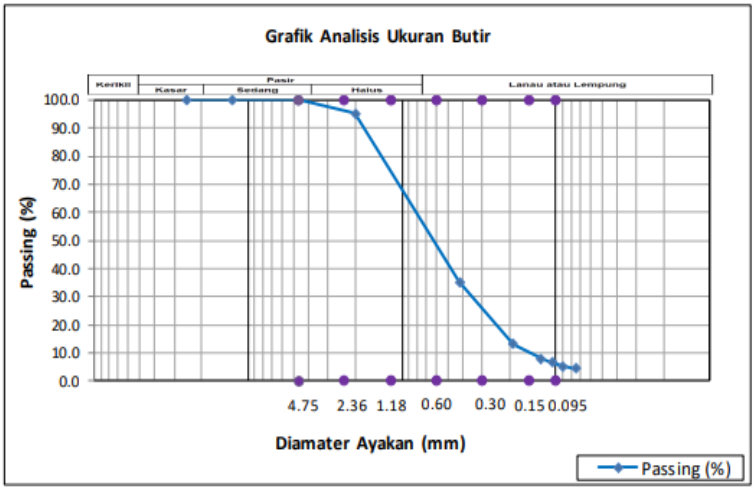
# LAMPIRAN C
# PERHITUNGAN DISTRIBUSI UKURAN

## Titik 1

| Ukuran Ayakan (mm) | Berat Tertahan (gram) | Persen Tertahan (%) | Persen Kumulatif Tertahan (%) | Persen Total Lolos (%) |
|---|---|---|---|---|
| 25.00 | 0.0 | 0.0 | 0.0 | 100.0 |
| 12.50 | 0.0 | 0.0 | 0.0 | 100.0 |
| 4.75 | 0.0 | 0.0 | 0.0 | 100.0 |
| 2.00 | 14.6 | 4.9 | 4.9 | 95.1 |
| 0.43 | 179.5 | 59.8 | 64.7 | 35.3 |
| 0.19 | 66.50 | 22.2 | 86.9 | 13.1 |
| 0.13 | 15.50 | 5.17 | 92.0 | 8.0 |
| 0.11 | 4.30 | 1.43 | 93.5 | 6.5 |
| 0.09 | 3.90 | 1.30 | 94.8 | 5.2 |
| 0.075 | 2.70 | 0.90 | 95.7 | 4.3 |
| Pan | 7.50 | 2.50 | 98.2 | 1.8 |
| Total | 294.50 | **FM** | **4.37** | |




**$D_{10}$ = 0.15**

**$D_{30}$ = 0.36**

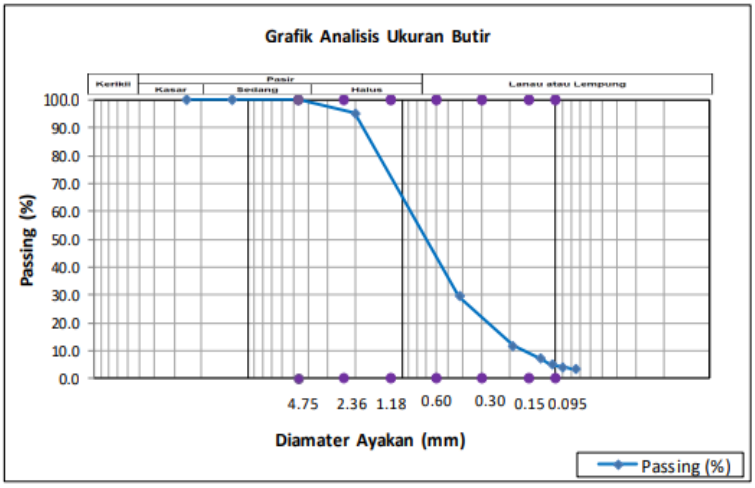
**$D_{60}$ = 0.80**

**$C_U = \frac{D_{60}}{D_{10}} = \frac{1.10}{0.15} = 7.33$**

**$C_c = \frac{(D_{30})^2}{D_{60} \times D_{10}} = \frac{(0.36)^2}{1.1 \times 0.15} = 0.79$**

## Titik 2

| Ukuran Ayakan (mm) | Berat Tertahan (gram) | Persen Tertahan (%) | Persen Kumulatif Tertahan (%) | Persen Total Lolos (%) |
|---|---|---|---|---|
| 25.00 | 0.0 | 0.0 | 0.0 | 100.0 |
| 12.50 | 0.0 | 0.0 | 0.0 | 100.0 |
| 4.75 | 0.0 | 0.0 | 0.0 | 100.0 |
| 2.00 | 14.4 | 4.8 | 4.8 | 95.2 |
| 0.43 | 197.2 | 65.7 | 70.5 | 29.5 |
| 0.19 | 53.20 | 17.7 | 88.3 | 11.7 |
| 0.13 | 14.00 | 4.67 | 92.9 | 7.1 |
| 0.11 | 5.90 | 1.97 | 94.9 | 5.1 |
| 0.09 | 3.10 | 1.03 | 95.9 | 4.1 |
| 0.075 | 1.80 | 0.60 | 96.5 | 3.5 |
| Pan | 1.20 | 0.40 | 96.9 | 3.1 |
| Total | 290.80 | **FM** | **4.47** | |




**$D_{10}$ = 0.18**

**$D_{30}$ = 0.43**

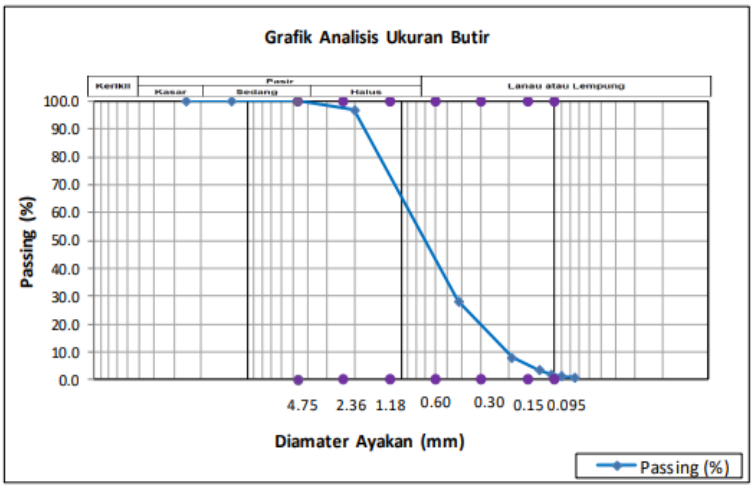
**$D_{60}$ = 0.90**

$$C_U = \frac{D_{60}}{D_{10}} = \frac{0.90}{0.18} = 5$$

$$C_c = \frac{(D_{30})^2}{D_{60} \times D_{10}} = \frac{(0.43)^2}{0.90 \times 0.18} = 1.14$$

## Titik 3

| Ukuran Ayakan (mm) | Berat Tertahan (gram) | Persen Tertahan (%) | Persen Kumulatif Tertahan (%) | Persen Total Lolos (%) |
|---|---|---|---|---|
| 25.00 | 0.0 | 0.0 | 0.0 | 100.0 |
| 12.50 | 0.0 | 0.0 | 0.0 | 100.0 |
| 4.75 | 0.0 | 0.0 | 0.0 | 100.0 |
| 2.00 | 9.6 | 3.2 | 3.2 | 96.8 |
| 0.43 | 206.0 | 68.7 | 71.9 | 28.1 |
| 0.19 | 60.50 | 20.2 | 92.0 | 8.0 |
| 0.13 | 13.50 | 4.50 | 96.5 | 3.5 |
| 0.11 | 4.20 | 1.40 | 97.9 | 2.1 |
| 0.09 | 2.70 | 0.90 | 98.8 | 1.2 |
| 0.075 | 0.70 | 0.23 | 99.1 | 0.9 |
| Pan | 0.60 | 0.20 | 99.3 | 0.7 |
| Total | 297.80 | **FM** | **4.60** | |




**$D_{10}$ = 0.20**

**$D_{30}$ = 0.45**

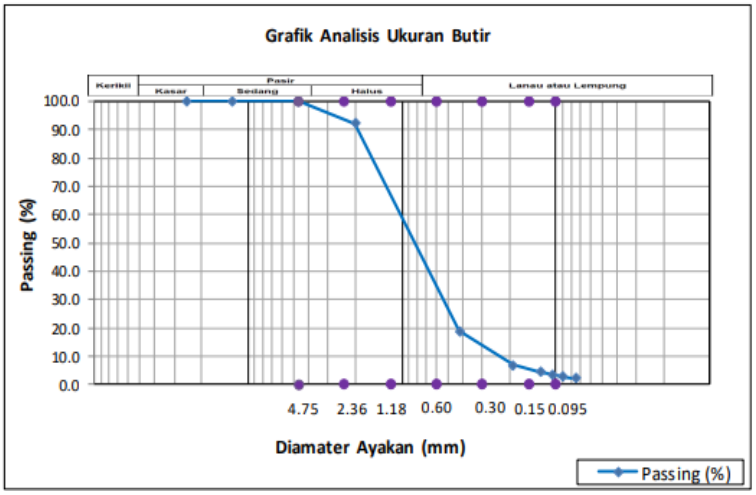
**$D_{60}$ = 0.89**

$$C_U = \frac{D_{60}}{D_{10}} = \frac{0.89}{0.20} = 4.45$$

$$C_c = \frac{(D_{30})^2}{D_{60} \times D_{10}} = \frac{(0.45)^2}{0.89 \times 0.20} = 1.14$$

## Titik 4

| Ukuran Ayakan (mm) | Berat Tertahan (gram) | Persen Tertahan (%) | Persen Kumulatif Tertahan (%) | Persen Total Lolos (%) |
|---|---|---|---|---|
| 25.00 | 0.0 | 0.0 | 0.0 | 100.0 |
| 12.50 | 0.0 | 0.0 | 0.0 | 100.0 |
| 4.75 | 0.0 | 0.0 | 0.0 | 100.0 |
| 2.00 | 23.7 | 7.9 | 7.9 | 92.1 |
| 0.43 | 220.0 | 73.3 | 81.2 | 18.8 |
| 0.19 | 35.50 | 11.8 | 93.1 | 6.9 |
| 0.13 | 7.70 | 2.57 | 95.6 | 4.4 |
| 0.11 | 2.50 | 0.83 | 96.5 | 3.5 |
| 0.09 | 2.20 | 0.73 | 97.2 | 2.8 |
| 0.075 | 1.30 | 0.43 | 97.6 | 2.4 |
| Pan | 4.50 | 1.50 | 99.1 | 0.9 |
| Total | 297.40 | **FM** | **4.72** | |




**$D_{10}$ = 0.24**

**$D_{30}$ = 0.55**

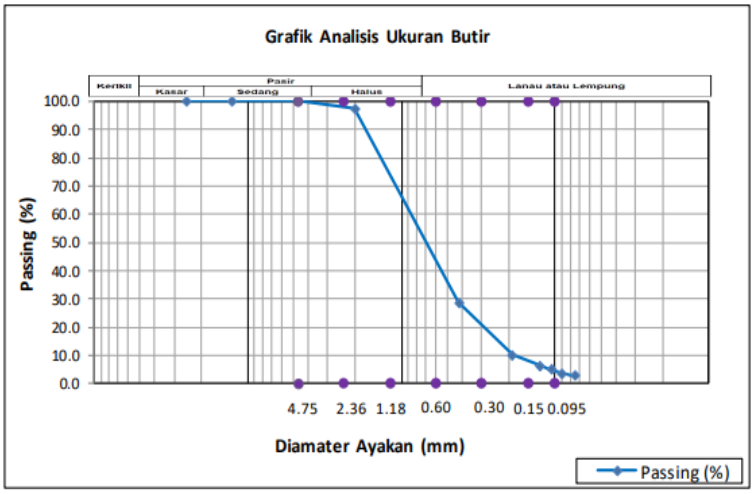
**$D_{60}$ = 1**

$$C_U = \frac{D_{60}}{D_{10}} = \frac{1}{0.24} = 4.17$$

$$C_c = \frac{(D_{30})^2}{D_{60} \times D_{10}} = \frac{(0.55)^2}{1 \times 0.24} = 1.26$$

## Titik 5

| Ukuran Ayakan (mm) | Berat Tertahan (gram) | Persen Tertahan (%) | Persen Kumulatif Tertahan (%) | Persen Total Lolos (%) |
|---|---|---|---|---|
| 25.00 | 0.0 | 0.0 | 0.0 | 100.0 |
| 12.50 | 0.0 | 0.0 | 0.0 | 100.0 |
| 4.75 | 0.0 | 0.0 | 0.0 | 100.0 |
| 2.00 | 8.1 | 2.7 | 2.7 | 97.3 |
| 0.43 | 206.1 | 68.7 | 71.4 | 28.6 |
| 0.19 | 55.60 | 18.5 | 89.9 | 10.1 |
| 0.13 | 11.20 | 3.73 | 93.7 | 6.3 |
| 0.11 | 3.90 | 1.30 | 95.0 | 5.0 |
| 0.09 | 4.00 | 1.33 | 96.3 | 3.7 |
| 0.075 | 3.00 | 1.00 | 97.3 | 2.7 |
| Pan | 5.80 | 1.93 | 99.2 | 0.8 |
| Total | 297.70 | **FM** | **4.49** | |




**$D_{10}$ = 0.19**

**$D_{30}$ = 0.45**

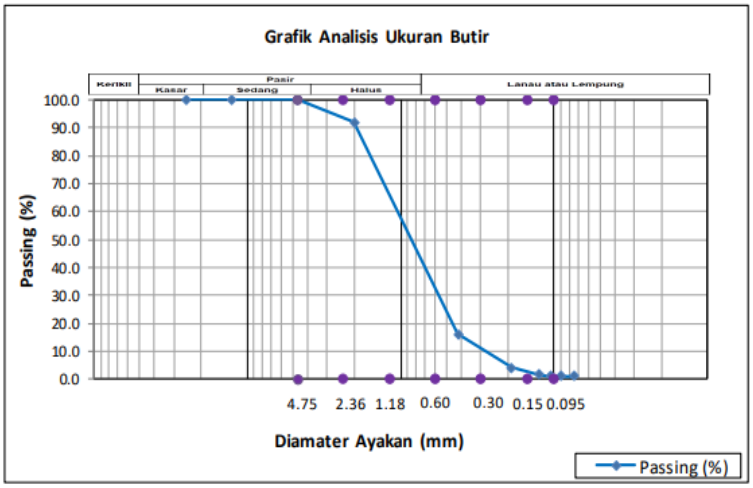
**$D_{60}$ = 0.89**

$$C_U = \frac{D_{60}}{D_{10}} = \frac{0.89}{0.19} = 4.68$$

$$C_c = \frac{(D_{30})^2}{D_{60} \times D_{10}} = \frac{(0.45)^2}{0.89 \times 0.19} = 1.20$$

## Titik 6

| Ukuran Ayakan (mm) | Berat Tertahan (gram) | Persen Tertahan (%) | Persen Kumulatif Tertahan (%) | Persen Total Lolos (%) |
|---|---|---|---|---|
| 25.00 | 0.0 | 0.0 | 0.0 | 100.0 |
| 12.50 | 0.0 | 0.0 | 0.0 | 100.0 |
| 4.75 | 0.0 | 0.0 | 0.0 | 100.0 |
| 2.00 | 24.0 | 8.0 | 8.0 | 92.0 |
| 0.43 | 227.4 | 75.8 | 83.8 | 16.2 |
| 0.19 | 36.00 | 12.0 | 95.8 | 4.2 |
| 0.13 | 7.50 | 2.50 | 98.3 | 1.7 |
| 0.11 | 1.30 | 0.43 | 98.7 | 1.3 |
| 0.09 | 0.40 | 0.13 | 98.9 | 1.1 |
| 0.075 | 0.20 | 0.07 | 98.9 | 1.1 |
| Pan | 0.30 | 0.10 | 99.0 | 1.0 |
| Total | 297.10 | **FM** | **4.84** | |




**$D_{10}$ = 0.29**

**$D_{30}$ = 0.58**

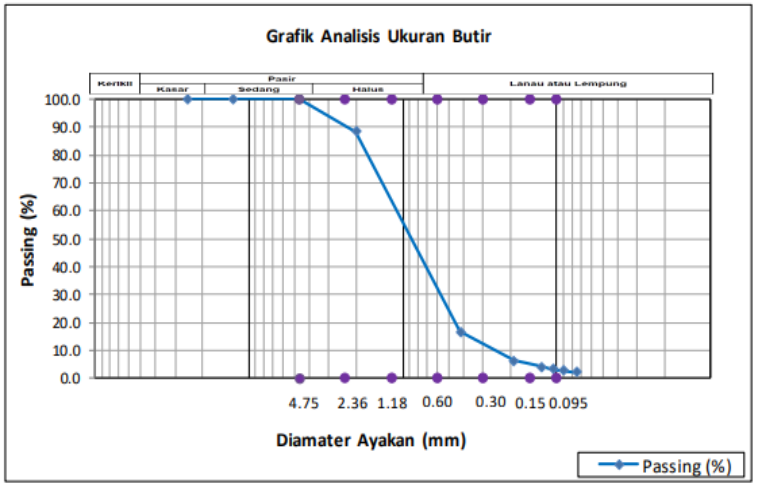
**$D_{60}$ = 1.10**

$$C_U = \frac{D_{60}}{D_{10}} = \frac{1.10}{0.29} = 3.79$$

$$C_c = \frac{(D_{30})^2}{D_{60} \times D_{10}} = \frac{(0.58)^2}{1.10 \times 0.29} = 1.05$$

## Titik 7

| Ukuran Ayakan (mm) | Berat Tertahan (gram) | Persen Tertahan (%) | Persen Kumulatif Tertahan (%) | Persen Total Lolos (%) |
|---|---|---|---|---|
| 25.00 | 0.0 | 0.0 | 0.0 | 100.0 |
| 12.50 | 0.0 | 0.0 | 0.0 | 100.0 |
| 4.75 | 0.0 | 0.0 | 0.0 | 100.0 |
| 2.00 | 34.8 | 11.6 | 11.6 | 88.4 |
| 0.43 | 214.9 | 71.6 | 83.2 | 16.8 |
| 0.19 | 31.50 | 10.5 | 93.7 | 6.3 |
| 0.13 | 6.30 | 2.10 | 95.8 | 4.2 |
| 0.11 | 2.10 | 0.70 | 96.5 | 3.5 |
| 0.09 | 2.00 | 0.67 | 97.2 | 2.8 |
| 0.075 | 1.50 | 0.50 | 97.7 | 2.3 |
| Pan | 7.50 | 2.50 | 100.2 | -0.2 |
| Total | 300.60 | **FM** | **4.78** | |




**$D_{10}$ = 0.25**

**$D_{30}$ = 0.58**

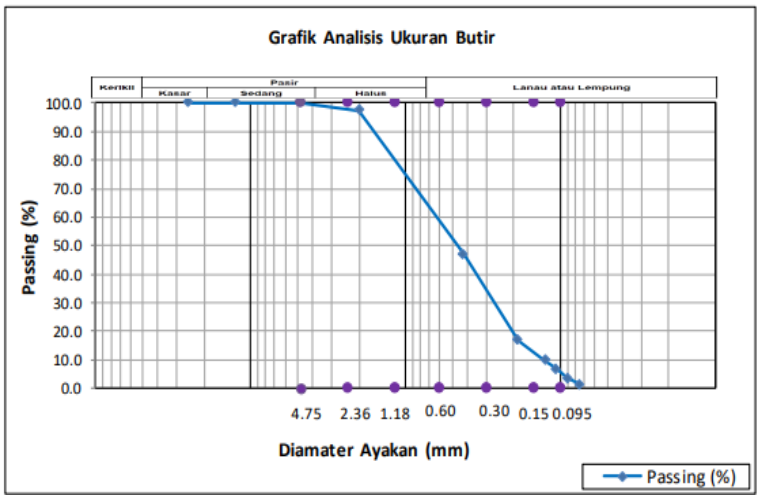
**$D_{60}$ = 1.20**

$$C_U = \frac{D_{60}}{D_{10}} = \frac{1.20}{0.25} = 4.80$$

$$C_c = \frac{(D_{30})^2}{D_{60} \times D_{10}} = \frac{(0.58)^2}{1.20 \times 0.25} = 1.12$$

## Titik 8

| Ukuran Ayakan (mm) | Berat Tertahan (gram) | Persen Tertahan (%) | Persen Kumulatif Tertahan (%) | Persen Total Lolos (%) |
|---|---|---|---|---|
| 25.00 | 0.0 | 0.0 | 0.0 | 100.0 |
| 12.50 | 0.0 | 0.0 | 0.0 | 100.0 |
| 4.75 | 0.0 | 0.0 | 0.0 | 100.0 |
| 2.00 | 8.1 | 2.7 | 2.7 | 97.3 |
| 0.43 | 150.9 | 50.3 | 53.0 | 47.0 |
| 0.19 | 90.10 | 30.0 | 83.0 | 17.0 |
| 0.13 | 22.00 | 7.33 | 90.4 | 9.6 |
| 0.11 | 8.50 | 2.83 | 93.2 | 6.8 |
| 0.09 | 9.70 | 3.23 | 96.4 | 3.6 |
| 0.075 | 6.60 | 2.20 | 98.6 | 1.4 |
| Pan | 1.90 | 0.63 | 99.3 | 0.7 |
| Total | 297.80 | **FM** | **4.19** | |




**$D_{10}$ = 0.14**

**$D_{30}$ = 0.27**

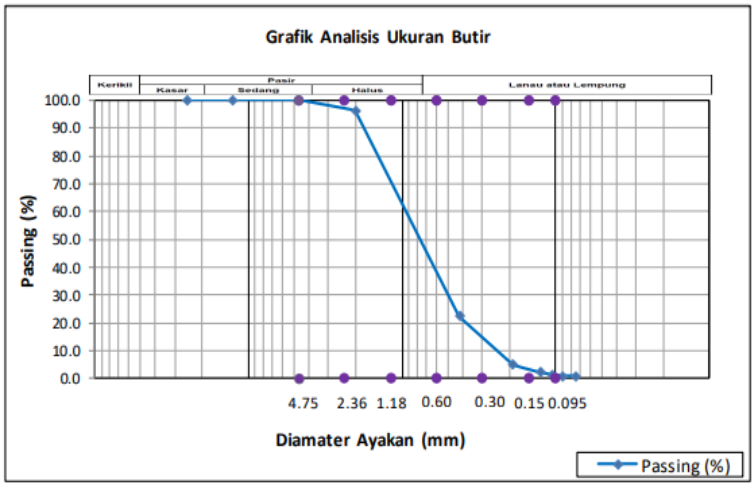
**$D_{60}$ = 0.65**

$$C_U = \frac{D_{60}}{D_{10}} = \frac{0.65}{0.14} = 4.64$$

$$C_c = \frac{(D_{30})^2}{D_{60} \times D_{10}} = \frac{(0.27)^2}{0.65 \times 0.14} = 0.80$$

## Titik 9

| Ukuran Ayakan (mm) | Berat Tertahan (gram) | Persen Tertahan (%) | Persen Kumulatif Tertahan (%) | Persen Total Lolos (%) |
|---|---|---|---|---|
| 25.00 | 0.0 | 0.0 | 0.0 | 100.0 |
| 12.50 | 0.0 | 0.0 | 0.0 | 100.0 |
| 4.75 | 0.0 | 0.0 | 0.0 | 100.0 |
| 2.00 | 11.0 | 3.7 | 3.7 | 96.3 |
| 0.43 | 221.9 | 74.0 | 77.6 | 22.4 |
| 0.19 | 52.10 | 17.4 | 95.0 | 5.0 |
| 0.13 | 8.30 | 2.77 | 97.8 | 2.2 |
| 0.11 | 2.20 | 0.73 | 98.5 | 1.5 |
| 0.09 | 1.40 | 0.47 | 99.0 | 1.0 |
| 0.075 | 0.40 | 0.13 | 99.1 | 0.9 |
| Pan | 0.40 | 0.13 | 99.2 | 0.8 |
| Total | 297.70 | **FM** | **4.72** | |




**$D_{10}$ = 0.25**

**$D_{30}$ = 0.50**

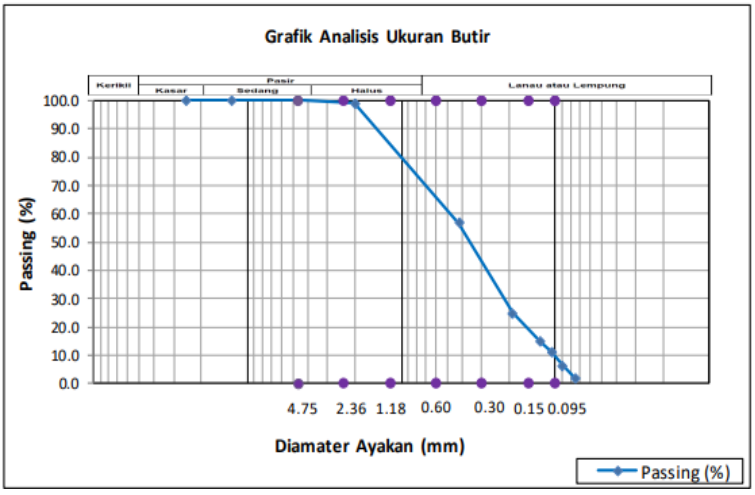
**$D_{60}$ = 0.95**

$$C_U = \frac{D_{60}}{D_{10}} = \frac{0.95}{0.25} = 3.80$$

$$C_c = \frac{(D_{30})^2}{D_{60} \times D_{10}} = \frac{(0.50)^2}{0.95 \times 0.25} = 1.05$$

## Titik 10

| Ukuran Ayakan (mm) | Berat Tertahan (gram) | Persen Tertahan (%) | Persen Kumulatif Tertahan (%) | Persen Total Lolos (%) |
|---|---|---|---|---|
| 25.00 | 0.0 | 0.0 | 0.0 | 100.0 |
| 12.50 | 0.0 | 0.0 | 0.0 | 100.0 |
| 4.75 | 0.0 | 0.0 | 0.0 | 100.0 |
| 2.00 | 3.4 | 1.1 | 1.1 | 98.9 |
| 0.43 | 126.4 | 42.1 | 43.3 | 56.7 |
| 0.19 | 95.60 | 31.9 | 75.1 | 24.9 |
| 0.13 | 30.00 | 10.00 | 85.1 | 14.9 |
| 0.11 | 10.80 | 3.60 | 88.7 | 11.3 |
| 0.09 | 14.80 | 4.93 | 93.7 | 6.3 |
| 0.075 | 12.70 | 4.23 | 97.9 | 2.1 |
| Pan | 5.80 | 1.93 | 99.8 | 0.2 |
| Total | 299.50 | **FM** | **3.87** | |




**$D_{10}$ = 0.10**

**$D_{30}$ = 0.23**

**$D_{60}$ = 0.50**

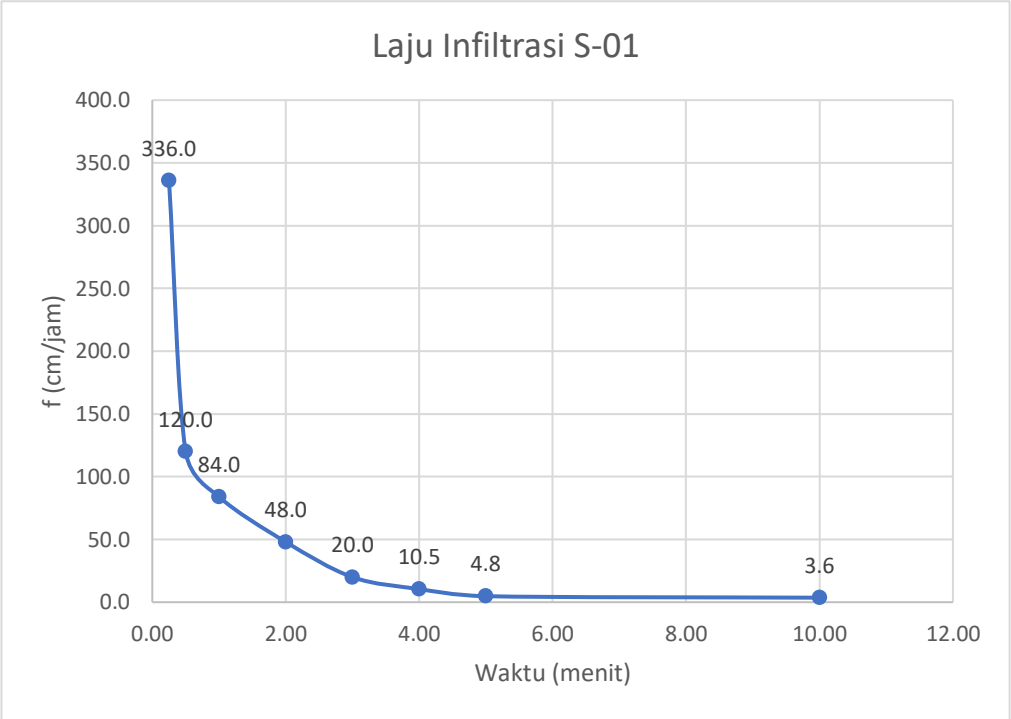
$$C_U = \frac{D_{60}}{D_{10}} = \frac{0.50}{0.10} = 5$$

$$C_c = \frac{(D_{30})^2}{D_{60} \times D_{10}} = \frac{(0.23)^2}{0.50 \times 0.10} = 1.06$$

# LAMPIRAN D
# PENGUKURAN LAJU INFILTRASI

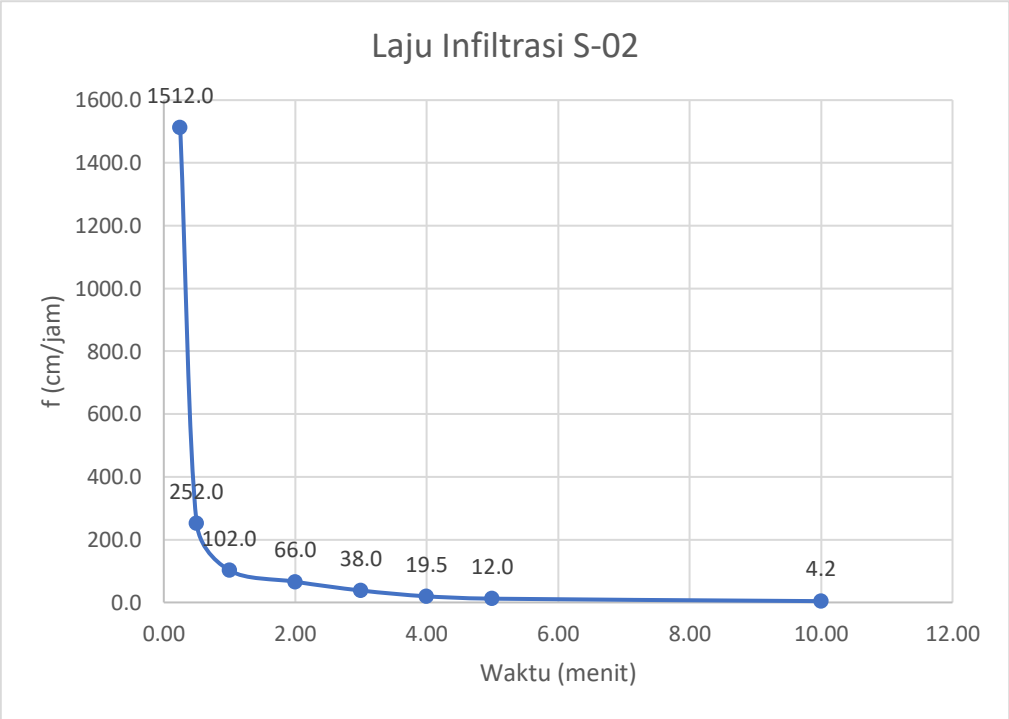
## Titik 1

| Waktu (menit) | Periode (menit) | Tinggi Air (cm) | Penurunan (cm) | f (cm/jam) | fc | f-fc | log(f-fc) | T (jam) |
|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0.25 | 0.25 | 24.6 | 1.4 | 336.0 | 3.6 | 332.4 | 2.522 | 0.0042 |
| 0.5 | 0.5 | 23.6 | 1 | 120.0 | 3.6 | 116.4 | 2.066 | 0.0083 |
| 1 | 1 | 22.2 | 1.4 | 84.0 | 3.6 | 80.4 | 1.905 | 0.0167 |
| 2 | 1 | 20.6 | 1.6 | 48.0 | 3.6 | 44.4 | 1.647 | 0.0333 |
| 3 | 1 | 19.6 | 1 | 20.0 | 3.6 | 16.4 | 1.215 | 0.0500 |
| 4 | 1 | 18.9 | 0.7 | 10.5 | 3.6 | 6.9 | 0.839 | 0.0667 |
| 5 | 5 | 18.5 | 0.4 | 4.8 | 3.6 | 1.2 | 0.079 | 0.0833 |
| 10 | 5 | 17.9 | 0.6 | 3.6 | 3.6 | 0.0 | | 0.1667 |



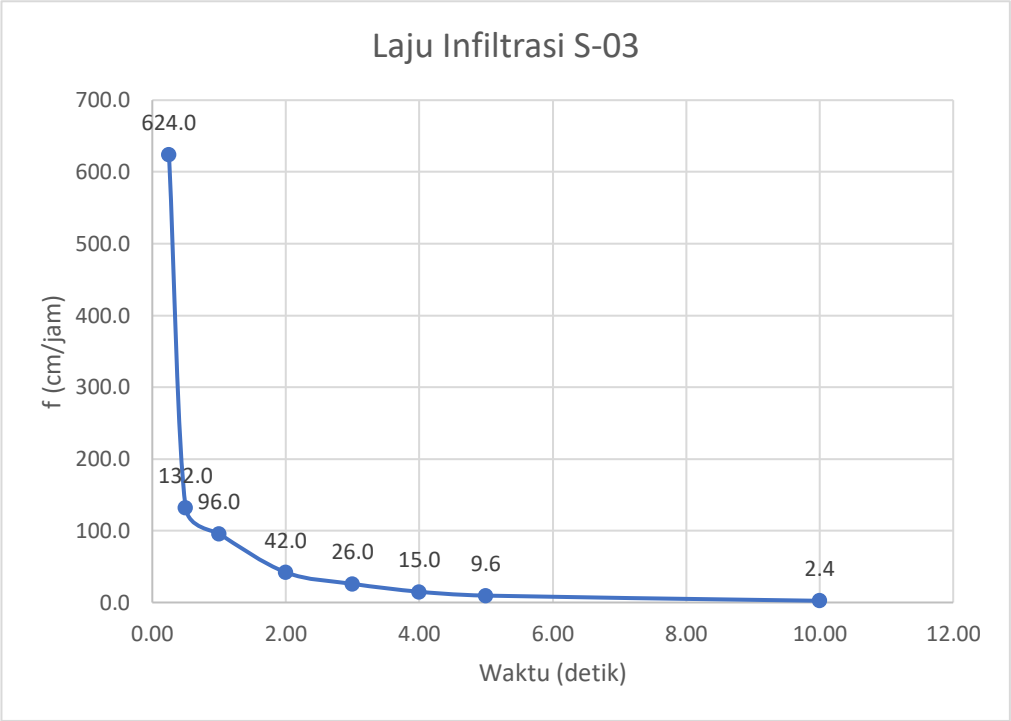
## Titik 2

| Waktu (menit) | Periode (menit) | Tinggi Air (cm) | Penurunan (cm) | f (cm/jam) | fc | f-fc | log(f-fc) | T (jam) |
|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 27.2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0.25 | 0.25 | 20.9 | 6.3 | 1512.0 | 4.2 | 1507.8 | 3.178 | 0.0042 |
| 0.5 | 0.5 | 18.8 | 2.1 | 252.0 | 4.2 | 247.8 | 2.394 | 0.0083 |
| 1 | 1 | 17.1 | 1.7 | 102.0 | 4.2 | 97.8 | 1.990 | 0.0167 |
| 2 | 1 | 14.9 | 2.2 | 66.0 | 4.2 | 61.8 | 1.791 | 0.0333 |
| 3 | 1 | 13 | 1.9 | 38.0 | 4.2 | 33.8 | 1.529 | 0.0500 |
| 4 | 1 | 11.7 | 1.3 | 19.5 | 4.2 | 15.3 | 1.185 | 0.0667 |
| 5 | 5 | 10.7 | 1 | 12.0 | 4.2 | 7.8 | 0.892 | 0.0833 |
| 10 | 5 | 10 | 0.7 | 4.2 | 4.2 | 0.0 | | 0.1667 |



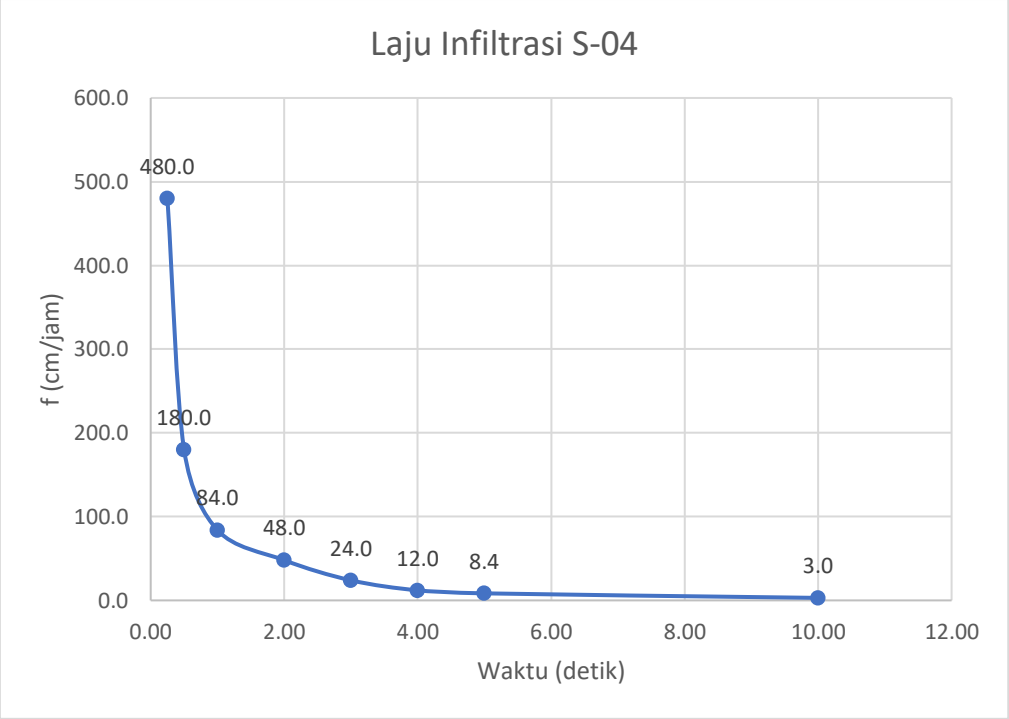
## Titik 3

| Waktu (menit) | Periode (menit) | Tinggi Air (cm) | Penurunan (cm) | f (cm/jam) | fc | f-fc | log(f-fc) | T (jam) |
|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 25.5 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0.25 | 0.25 | 22.9 | 2.6 | 624.0 | 2.4 | 622 | 2.794 | 0.0042 |
| 0.5 | 0.5 | 21.8 | 1.1 | 132.0 | 2.4 | 130 | 2.113 | 0.0083 |
| 1 | 1 | 20.2 | 1.6 | 96.0 | 2.4 | 94 | 1.971 | 0.0167 |
| 2 | 1 | 18.8 | 1.4 | 42.0 | 2.4 | 40 | 1.598 | 0.0333 |
| 3 | 1 | 17.5 | 1.3 | 26.0 | 2.4 | 24 | 1.373 | 0.0500 |
| 4 | 1 | 16.5 | 1 | 15.0 | 2.4 | 13 | 1.100 | 0.0667 |
| 5 | 5 | 15.7 | 0.8 | 9.6 | 2.4 | 7 | 0.857 | 0.0833 |
| 10 | 5 | 15.3 | 0.4 | 2.4 | 2.4 | 0 | | 0.1667 |



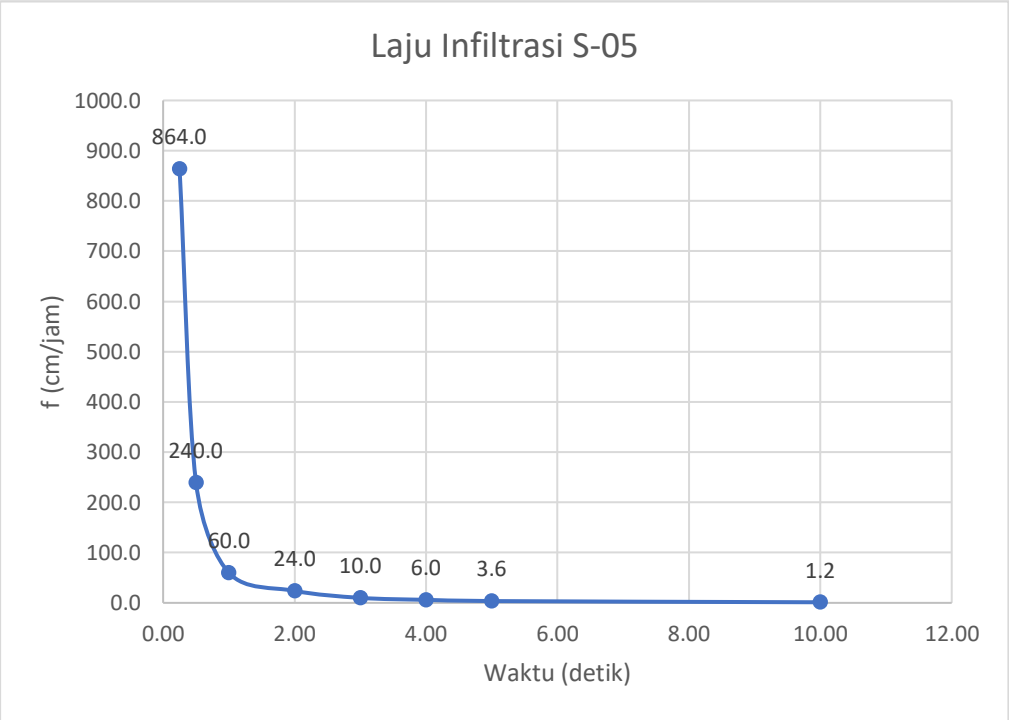
## Titik 4

| Waktu (menit) | Periode (menit) | Tinggi Air (cm) | Penurunan (cm) | f (cm/jam) | fc | f-fc | log(f-fc) | T (jam) |
|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0.25 | 0.25 | 24 | 2 | 480.0 | 3.0 | 477 | 2.679 | 0.0042 |
| 0.5 | 0.5 | 22.5 | 1.5 | 180.0 | 3.0 | 177 | 2.248 | 0.0083 |
| 1 | 1 | 21.1 | 1.4 | 84.0 | 3.0 | 81 | 1.908 | 0.0167 |
| 2 | 1 | 19.5 | 1.6 | 48.0 | 3.0 | 45 | 1.653 | 0.0333 |
| 3 | 1 | 18.3 | 1.2 | 24.0 | 3.0 | 21 | 1.322 | 0.0500 |
| 4 | 1 | 17.5 | 0.8 | 12.0 | 3.0 | 9 | 0.954 | 0.0667 |
| 5 | 5 | 16.8 | 0.7 | 8.4 | 3.0 | 5 | 0.732 | 0.0833 |
| 10 | 5 | 16.3 | 0.5 | 3.0 | 3.0 | 0 | | 0.1667 |



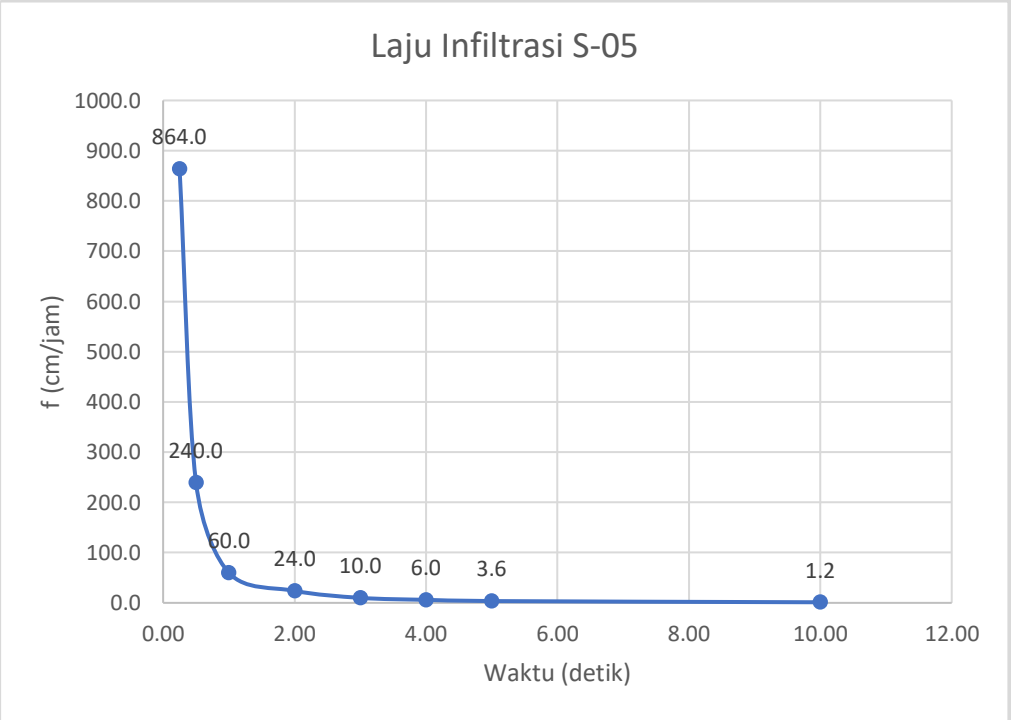
## Titik 5

| Waktu (menit) | Periode (menit) | Tinggi Air (cm) | Penurunan (cm) | f (cm/jam) | fc | f-fc | log(f-fc) | T (jam) |
|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 23.6 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0.25 | 0.25 | 20 | 3.6 | 864.0 | 1.2 | 862.8 | 2.936 | 0.0042 |
| 0.5 | 0.5 | 18 | 2 | 240.0 | 1.2 | 238.8 | 2.378 | 0.0083 |
| 1 | 1 | 17 | 1 | 60.0 | 1.2 | 58.8 | 1.769 | 0.0167 |
| 2 | 1 | 16.2 | 0.8 | 24.0 | 1.2 | 22.8 | 1.358 | 0.0333 |
| 3 | 1 | 15.7 | 0.5 | 10.0 | 1.2 | 8.8 | 0.944 | 0.0500 |
| 4 | 1 | 15.3 | 0.4 | 6.0 | 1.2 | 4.8 | 0.681 | 0.0667 |
| 5 | 5 | 15 | 0.3 | 3.6 | 1.2 | 2.4 | 0.380 | 0.0833 |
| 10 | 5 | 14.8 | 0.2 | 1.2 | 1.2 | 0.0 | | 0.1667 |



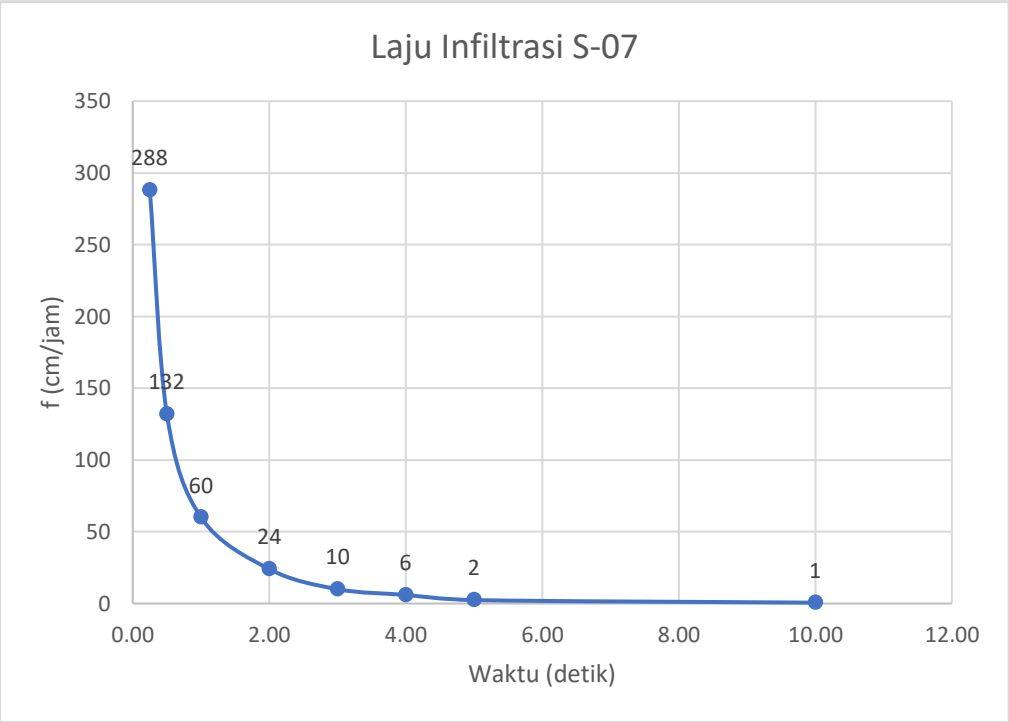
## Titik 6

| Waktu (menit) | Periode (menit) | Tinggi Air (cm) | Penurunan (cm) | f (cm/jam) | fc | f-fc | log(f-fc) | T (jam) |
|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0.25 | 0.25 | 17.8 | 3.2 | 768 | 2.0 | 766.0 | 2.884 | 0.0042 |
| 0.5 | 0.5 | 16 | 1.8 | 216 | 2.0 | 214.0 | 2.330 | 0.0083 |
| 1 | 1 | 14.5 | 1.5 | 90 | 2.0 | 88.0 | 1.944 | 0.0167 |
| 2 | 1 | 11.7 | 2.8 | 84 | 2.0 | 82.0 | 1.914 | 0.0333 |
| 3 | 1 | 10.7 | 1 | 20 | 2.0 | 18.0 | 1.255 | 0.0500 |
| 4 | 1 | 9.8 | 0.9 | 14 | 2.0 | 11.5 | 1.061 | 0.0667 |
| 5 | 5 | 9.3 | 0.5 | 6 | 2.0 | 4.0 | 0.602 | 0.0833 |
| 10 | 5 | 9 | 0.3 | 2 | 2.0 | -0.2 | | 0.1667 |



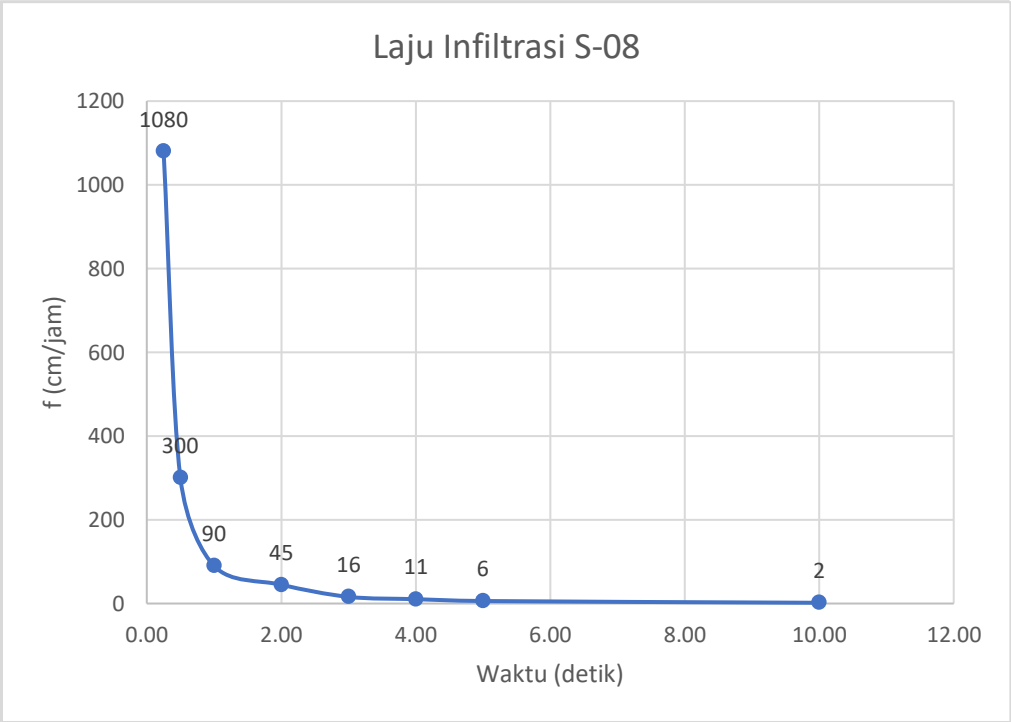
## Titik 7

| Waktu (menit) | Periode (menit) | Tinggi Air (cm) | Penurunan (cm) | f (cm/jam) | fc | f-fc | log(f-fc) | T (jam) |
|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 23.5 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0.25 | 0.25 | 22.3 | 1.2 | 288 | 1.0 | 287.0 | 2.458 | 0.0042 |
| 0.5 | 0.5 | 21.2 | 1.1 | 132 | 1.0 | 131.0 | 2.117 | 0.0083 |
| 1 | 1 | 20.2 | 1 | 60 | 1.0 | 59.0 | 1.771 | 0.0167 |
| 2 | 1 | 19.4 | 0.8 | 24 | 1.0 | 23.0 | 1.362 | 0.0333 |
| 3 | 1 | 18.9 | 0.5 | 10 | 1.0 | 9.0 | 0.954 | 0.0500 |
| 4 | 1 | 18.5 | 0.4 | 6 | 1.0 | 5.0 | 0.699 | 0.0667 |
| 5 | 5 | 18.3 | 0.2 | 2 | 1.0 | 1.4 | 0.146 | 0.0833 |
| 10 | 5 | 18.2 | 0.1 | 1 | 1.0 | -0.4 | | 0.1667 |



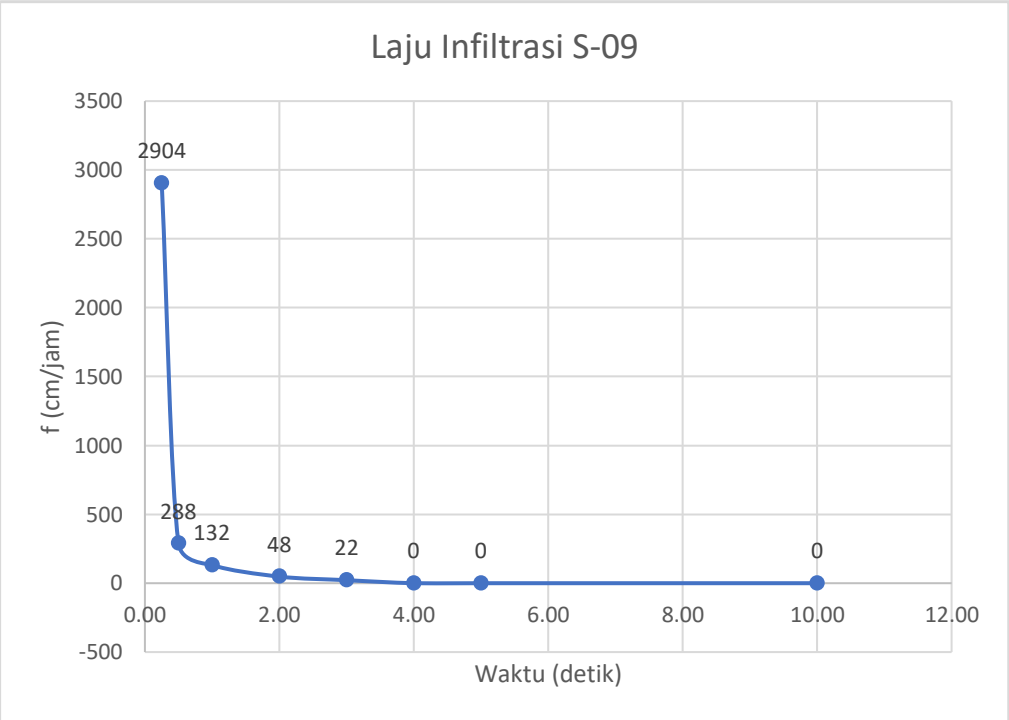
## Titik 8

| Waktu (menit) | Periode (menit) | Tinggi Air (cm) | Penurunan (cm) | f (cm/jam) | fc | f-fc | log(f-fc) | T (jam) |
|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0.25 | 0.25 | 21.5 | 4.5 | 1080 | 2.0 | 1078.0 | 3.033 | 0.0042 |
| 0.5 | 0.5 | 19 | 2.5 | 300 | 2.0 | 298.0 | 2.474 | 0.0083 |
| 1 | 1 | 17.5 | 1.5 | 90 | 2.0 | 88.0 | 1.944 | 0.0167 |
| 2 | 1 | 16 | 1.5 | 45 | 2.0 | 43.0 | 1.633 | 0.0333 |
| 3 | 1 | 15.2 | 0.8 | 16 | 2.0 | 14.0 | 1.146 | 0.0500 |
| 4 | 1 | 14.5 | 0.7 | 11 | 2.0 | 8.5 | 0.929 | 0.0667 |
| 5 | 5 | 14 | 0.5 | 6 | 2.0 | 4.0 | 0.602 | 0.0833 |
| 10 | 5 | 13.7 | 0.3 | 2 | 2.0 | -0.2 | | 0.1667 |



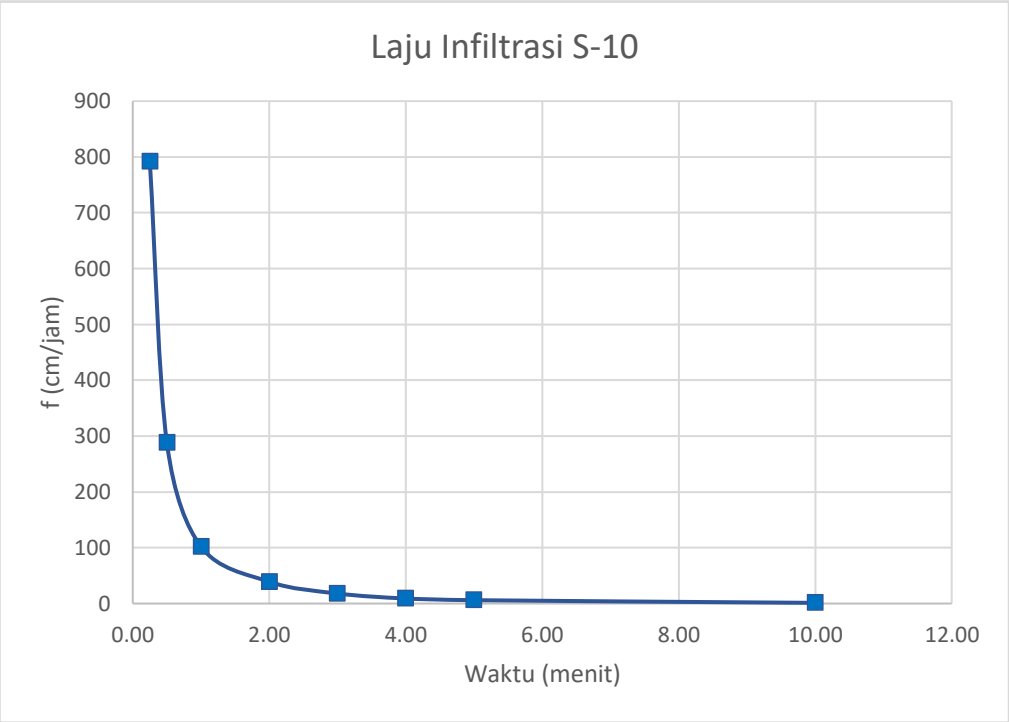
## Titik 9

| Waktu (menit) | Periode (menit) | Tinggi Air (cm) | Penurunan (cm) | f (cm/jam) | fc | f-fc | log(f-fc) | T (jam) |
|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 23.3 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0.25 | 0.25 | 11.2 | 12.1 | 2904 | 22.0 | 2882.0 | 3.460 | 0.0042 |
| 0.5 | 0.5 | 8.8 | 2.4 | 288 | 22.0 | 266.0 | 2.425 | 0.0083 |
| 1 | 1 | 6.6 | 2.2 | 132 | 22.0 | 110.0 | 2.041 | 0.0167 |
| 2 | 1 | 5 | 1.6 | 48 | 22.0 | 26.0 | 1.415 | 0.0333 |
| 3 | 1 | 3.9 | 1.1 | 22 | 22.0 | 0.0 | | 0.0500 |
| 4 | 1 | - | - | - | - | - | - | - |
| 5 | 5 | - | - | - | - | - | - | - |
| 10 | 5 | - | - | - | - | - | - | - |



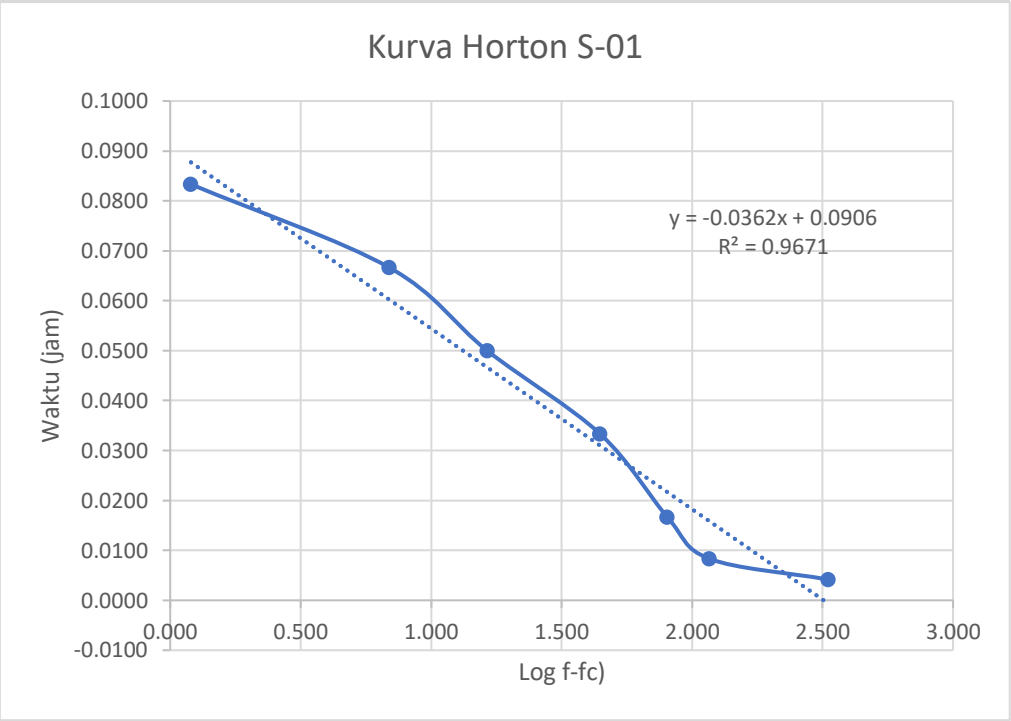
## Titik 10

| Waktu (menit) | Periode (menit) | Tinggi Air (cm) | Penurunan (cm) | f (cm/jam) | fc | f-fc | log(f-fc) | T (jam) |
|---|---|---|---|---|---|---|---|---|
| 0 | 0 | 27.7 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0.25 | 0.25 | 24.4 | 3.3 | 792 | 1.0 | 791.0 | 2.898 | 0.0042 |
| 0.5 | 0.5 | 22 | 2.4 | 288 | 1.0 | 287.0 | 2.458 | 0.0083 |
| 1 | 1 | 20.3 | 1.7 | 102 | 1.0 | 101.0 | 2.004 | 0.0167 |
| 2 | 1 | 19 | 1.3 | 39 | 1.0 | 38.0 | 1.580 | 0.0333 |
| 3 | 1 | 18.1 | 0.9 | 18 | 1.0 | 17.0 | 1.230 | 0.0500 |
| 4 | 1 | 17.5 | 0.6 | 9 | 1.0 | 8.0 | 0.903 | 0.0667 |
| 5 | 5 | 17 | 0.5 | 6 | 1.0 | 5.0 | 0.699 | 0.0833 |
| 10 | 5 | 16.8 | 0.2 | 1 | 1.0 | 0.2 | | 0.1667 |



# LAMPIRAN E
# PERHITUNGAN LAJU INFILTRASI

## Titik 1




Berdasarkan persamaan linier diatas, maka didapatkan gradien, m = -0.0362 dan nilai konstanta jenis tanah (K) = 63.61 menggunakan rumus, k= -1/(m log 2.718).

- Perhitungan laju infiltrasi pada saat waktu konstan

  $f = f_c + (f_0 - f_c)\, e^{-Kt}$

  $f = 3.6 + (336 - 3.6)\, 2.718^{-63.61(0.1667)}$

  $f = 3.608$ cm/jam

  $f = 36.08$ mm/jam

- Perhitungan volume infiltrasi

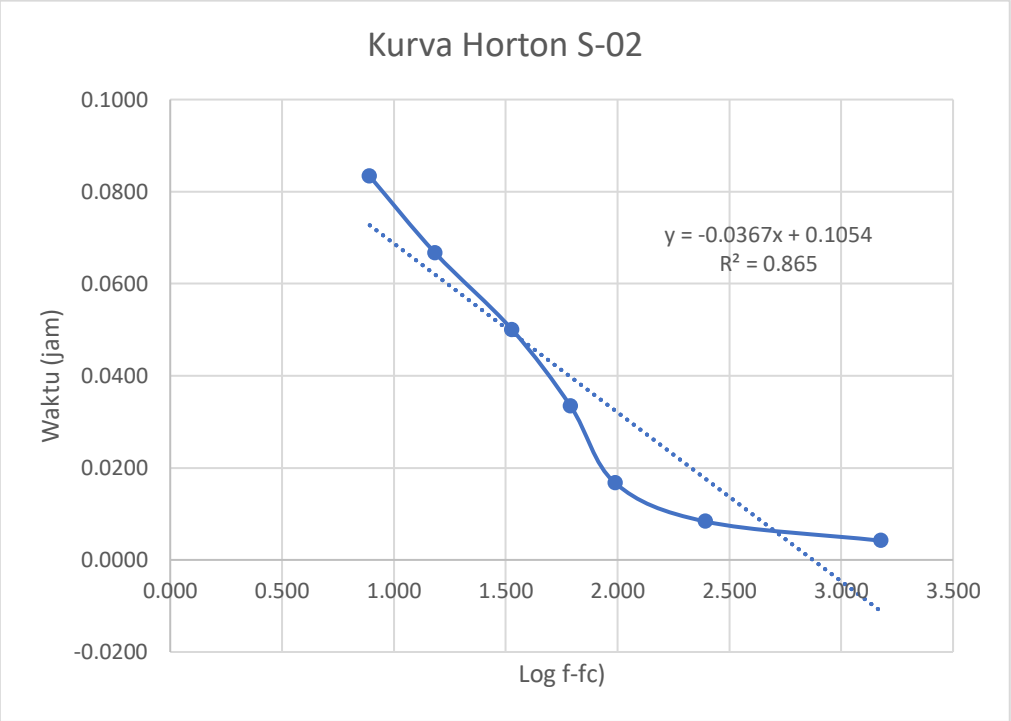
  $f(t) = f_c.t + 1/K\,(f_0 - f_c)(1- e^{-Kt})$

  $f(0.1667) = (3.6 \times 0.1667) + (1/63.61)(336 - 3.6)(1- 2.718^{-63.61(0.1667)})$

  $= 5.825$ cm/jam

  $= 58.25$ mm/jam

## Titik 2




Berdasarkan persamaan linier diatas, maka didapatkan gradien, m = -0.0367 dan nilai konstanta jenis tanah (K) = 62.75 menggunakan rumus, k= -1/(m log 2.718).

- Perhitungan laju infiltrasi pada saat waktu konstan

  $f = f_c + (f_0 - f_c)\, e^{-Kt}$

  $f = 4.2 + (1512 - 4.2)\, 2.718^{-62.75(0.1667)}$

  $f = 4.243$ cm/jam

  $f = 42.43$ mm/jam

- Perhitungan volume infiltrasi

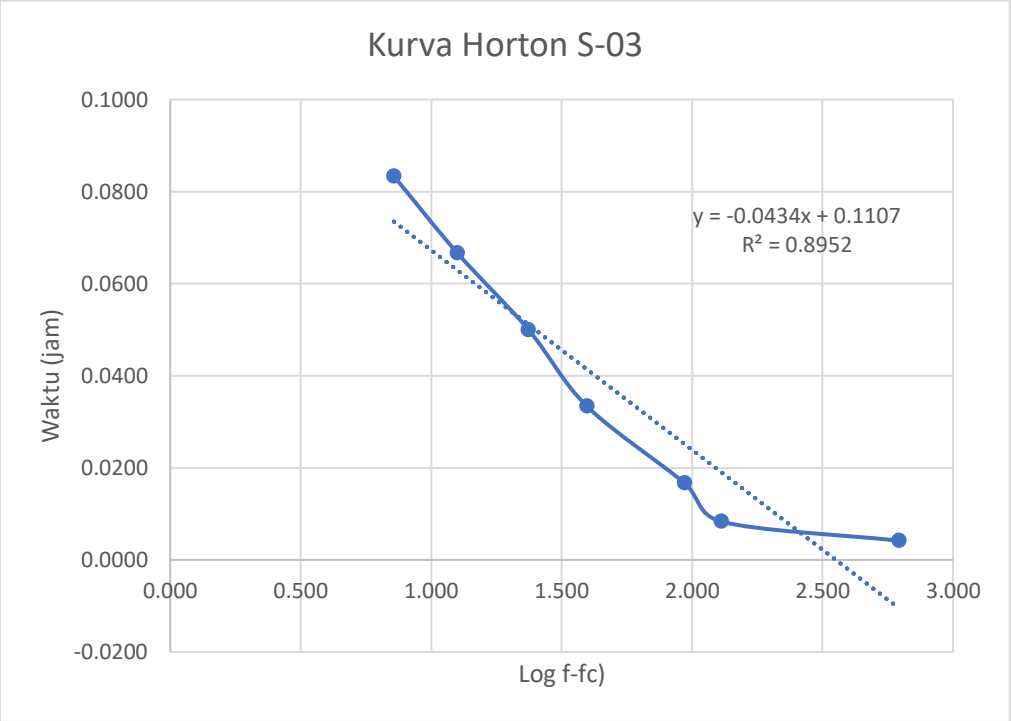
  $f(t) = f_c.t + 1/K\,(f_0 - f_c)(1- e^{-Kt})$

  $f(0.1667) = (4.2 \times 0.1667) + (1/62.75)(1512 - 4.2)(1- 2.718^{-62.75(0.1667)})$

  $= 24.729$ cm/jam

  $= 247.29$ mm/jam

## Titik 3




Berdasarkan persamaan linier diatas, maka didapatkan gradien, m = -0.0434 dan nilai konstanta jenis tanah (K) = 53.06 menggunakan rumus, k= -1/(m log 2.718).

- Perhitungan laju infiltrasi pada saat waktu konstan

  $f = f_c + (f_0 - f_c)\, e^{-Kt}$

  $f = 2.4 + (624 - 2.4)\, 2.718^{-53.06(0.1667)}$

  f = 2.490 cm/jam

  f = 24.90 mm/jam

- Perhitungan volume infiltrasi

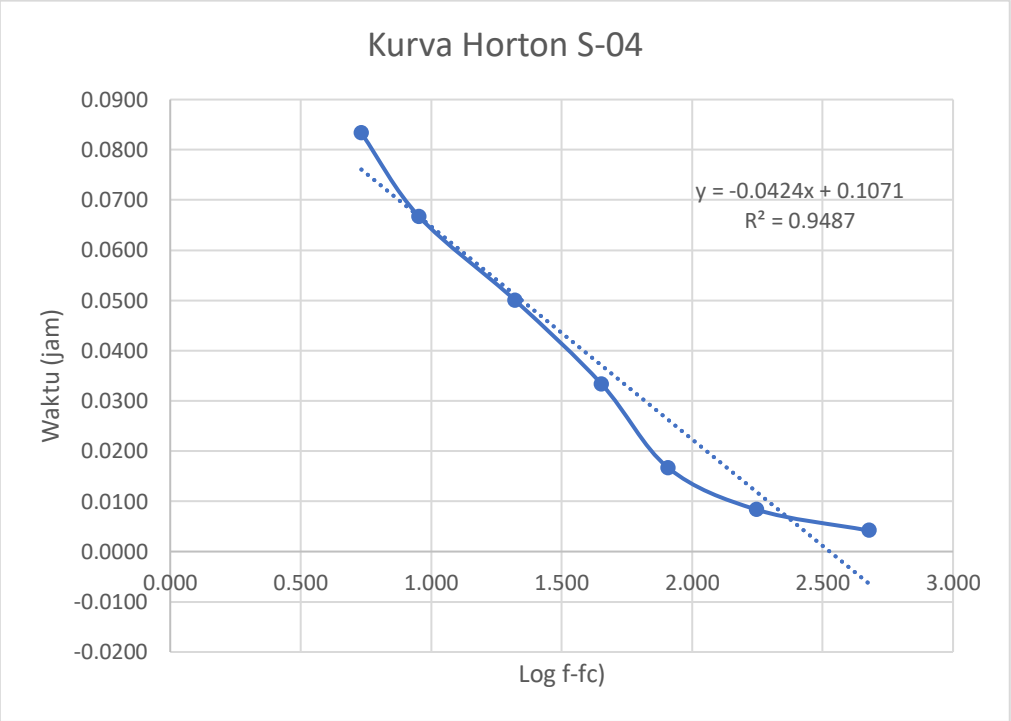
  $f(t) = f_c.t + 1/K\,(f_0 - f_c)(1- e^{-Kt})$

  $f(0.1667) = (2.4 \times 0.1667) + (1/53.06)(624 - 2.4)(1- 2.718^{-53.06(0.1667)})$

  = 12.113 cm/jam

  = 121.13 mm/jam

## Titik 4




Berdasarkan persamaan linier diatas, maka didapatkan gradien, m = -0.0424 dan nilai konstanta jenis tanah (K) = 54.31 menggunakan rumus, k= -1/(m log 2.718).

- Perhitungan laju infiltrasi pada saat waktu konstan

  $f = f_c + (f_0 - f_c)\, e^{-Kt}$

  $f = 3.0 + (480 - 3.0)\, 2.718^{-54.31(0.1667)}$

  f = 3.056 cm/jam

  f = 30.56 mm/jam

- Perhitungan volume infiltrasi

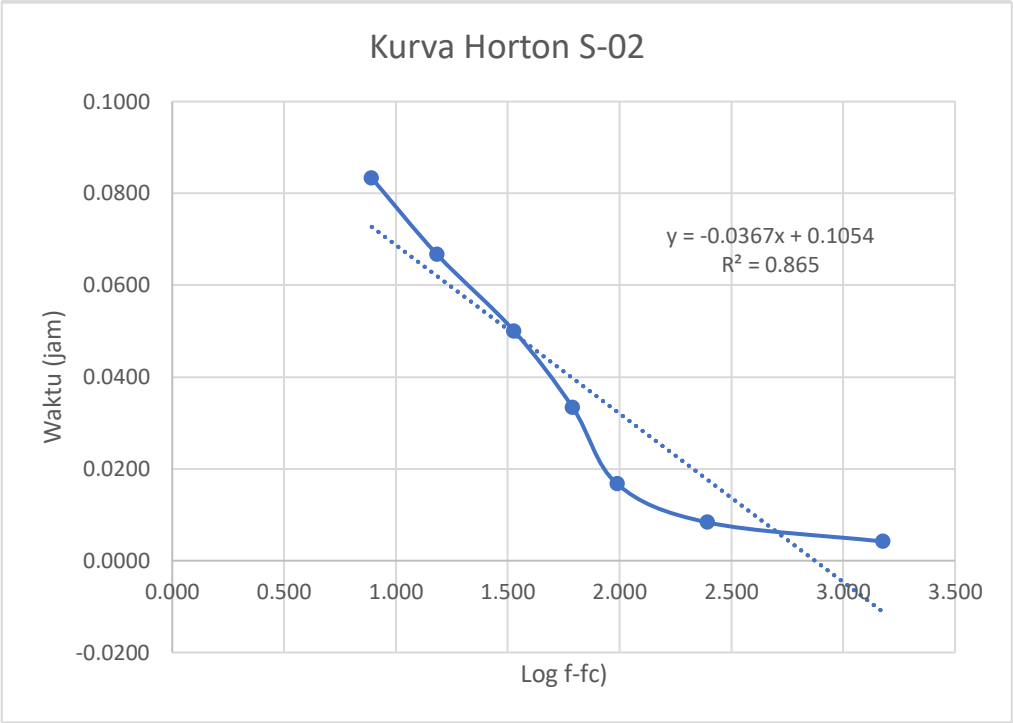
  $f(t) = f_c.t + 1/K\,(f_0 - f_c)(1- e^{-Kt})$

  $f(0.1667) = (3.0 \times 0.1667) + (1/54.31)(480 - 3.0)(1- 2.718^{-54.31(0.1667)})$

  = 9.282 cm/jam

  = 92.82 mm/jam

## Titik 5




Berdasarkan persamaan linier diatas, maka didapatkan gradien, m = -0.0311 dan nilai konstanta jenis tanah (K) = 74.05 menggunakan rumus, k= -1/(m log 2.718).

- Perhitungan laju infiltrasi pada saat waktu konstan

  $f = f_c + (f_0 - f_c)\, e^{-Kt}$

  $f = 1.2 + (864 - 1.2)\, 2.718^{-74.05(0.1667)}$

  f = 1.204 cm/jam

  f = 12.04 mm/jam

- Perhitungan volume infiltrasi

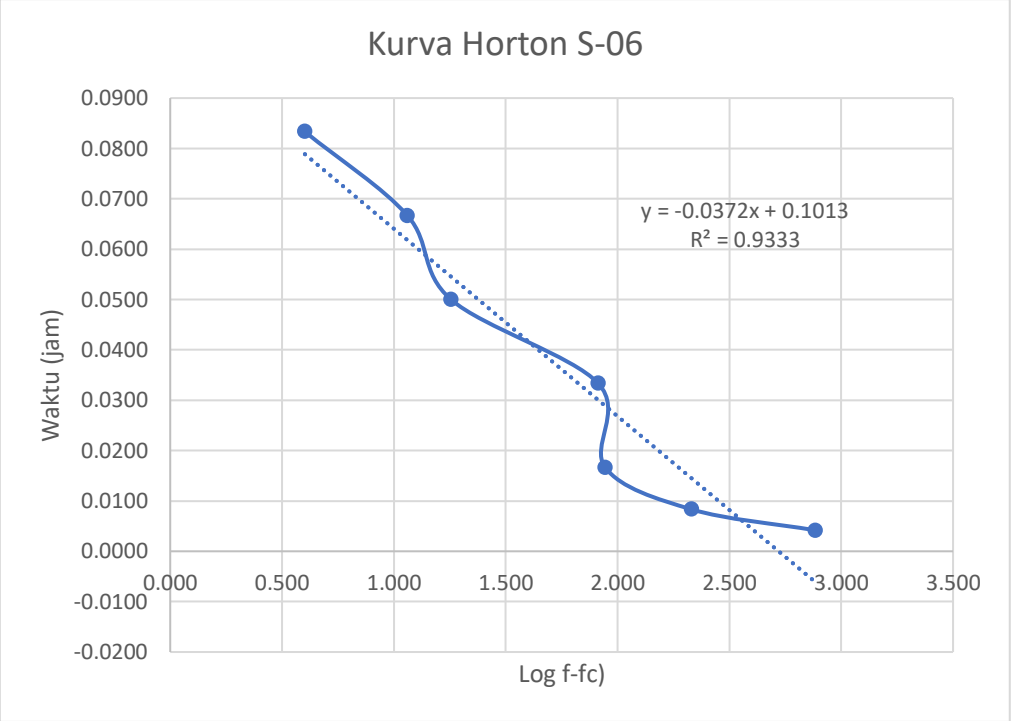
  $f(t) = f_c.t + 1/K\,(f_0 - f_c)(1- e^{-Kt})$

  $f(0.1667) = (1.2 \times 0.1667) + (1/74.05)(864 - 1.2)(1- 2.718^{-74.05(0.1667)})$

  = 11.852 cm/jam

  = 118.52 mm/jam

## Titik 6




Berdasarkan persamaan linier diatas, maka didapatkan gradien, m = -0.0372 dan nilai konstanta jenis tanah (K) = 61.90 menggunakan rumus, k= -1/(m log 2.718).

- Perhitungan laju infiltrasi pada saat waktu konstan

  $f = f_c + (f_0 - f_c)\, e^{-Kt}$

  $f = 2.0 + (768 - 2.0)\, 2.718^{-61.90(0.1667)}$

  f = 2.025 cm/jam

  f = 20.25 mm/jam

- Perhitungan volume infiltrasi

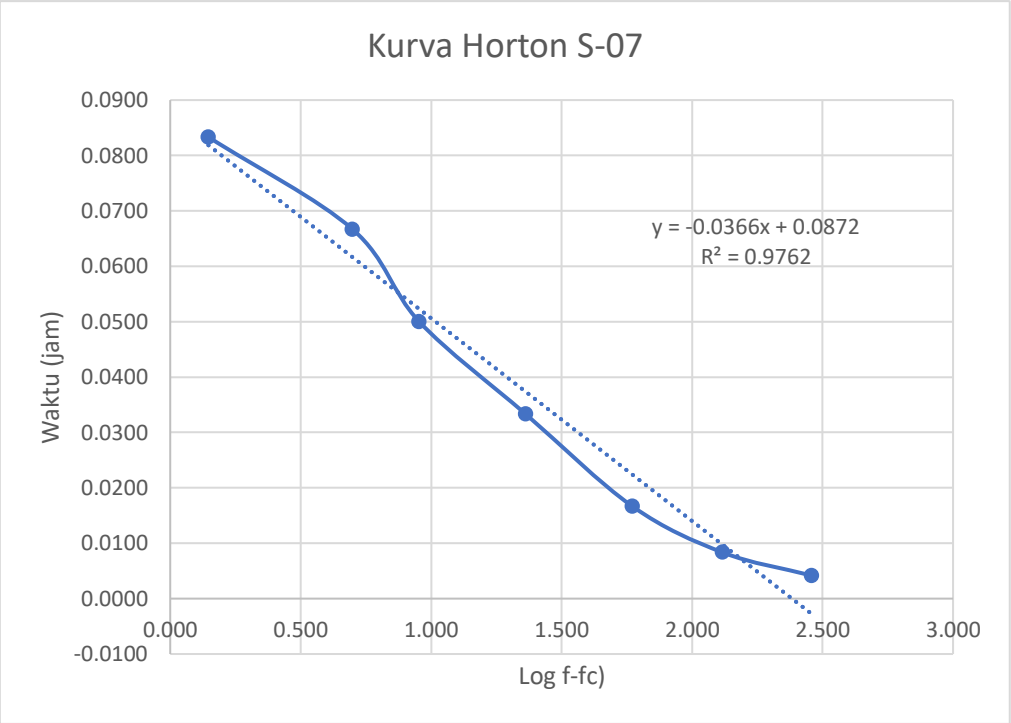
  $f(t) = f_c.t + 1/K\,(f_0 - f_c)(1- e^{-Kt})$

  $f(0.1667) = (2.0 \times 0.1667) + (1/61.90)(768 - 2.0)(1- 2.718^{-61.90(0.1667)})$

  = 12.707 cm/jam

  = 127.07 mm/jam

## Titik 7




Berdasarkan persamaan linier diatas, maka didapatkan gradien, m = -0.0366 dan nilai konstanta jenis tanah (K) = 62.92 menggunakan rumus, k= -1/(m log 2.718).

- Perhitungan laju infiltrasi pada saat waktu konstan

  $f = f_c + (f_0 - f_c)\, e^{-Kt}$

  $f = 1.0 + (288 - 1.0)\, 2.718^{-62.92(0.1667)}$

  $f = 1.008$ cm/jam

  $f = 10.08$ mm/jam

- Perhitungan volume infiltrasi

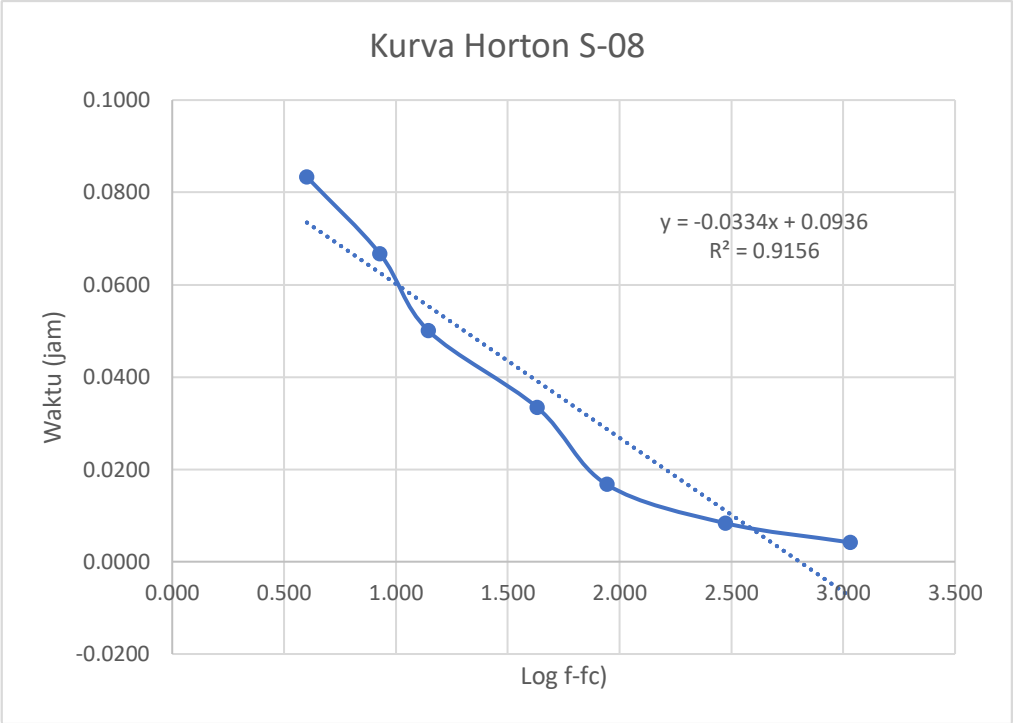
  $f(t) = f_c.t + 1/K\,(f_0 - f_c)(1- e^{-Kt})$

  $f(0.1667) = (1.0 \times 0.1667) + (1/62.92)(288 - 1.0)(1- 2.718^{-62.92(0.1667)})$

  $= 4.728$ cm/jam

  $= 47.28$ mm/jam

## Titik 8




Berdasarkan persamaan linier diatas, maka didapatkan gradien, m = -0.0334 dan nilai konstanta jenis tanah (K) = 68.95 menggunakan rumus, k= -1/(m log 2.718).

- Perhitungan laju infiltrasi pada saat waktu konstan

  $f = f_c + (f_0 - f_c)\, e^{-Kt}$

  $f = 2.0 + (1080 - 2.0)\, 2.718^{-68.95(0.1667)}$

  $f = 2.011$ cm/jam

  $f = 20.11$ mm/jam

- Perhitungan volume infiltrasi

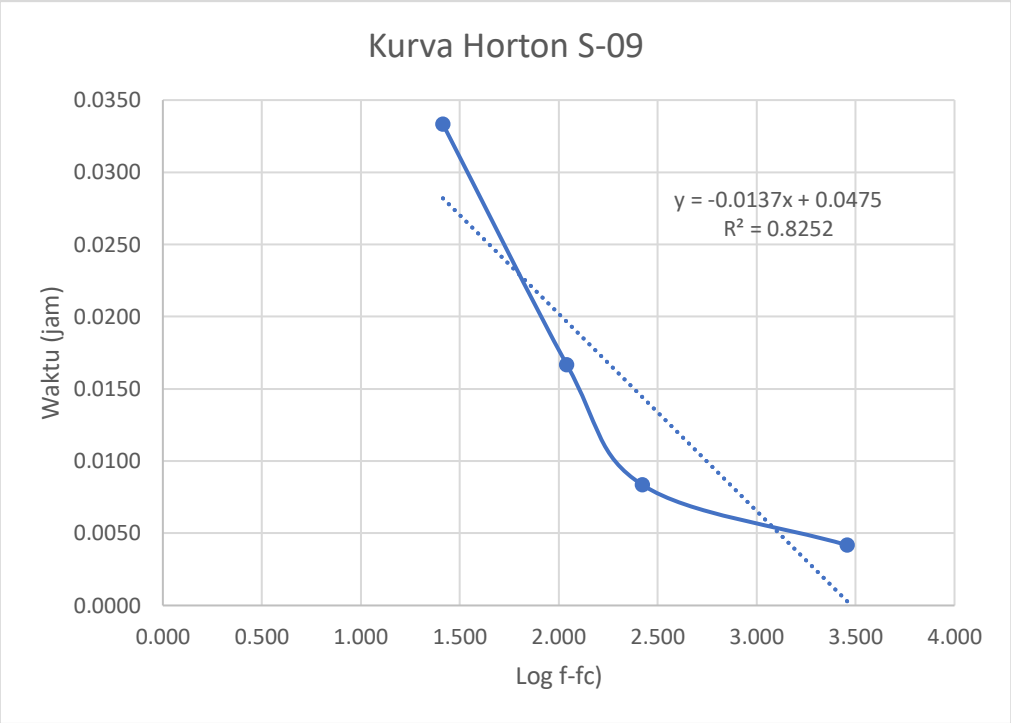
  $f(t) = f_c.t + 1/K\,(f_0 - f_c)(1- e^{-Kt})$

  $f(0.1667) = (2.0 \times 0.1667) + (1/68.95)(1080 - 2.0)(1- 2.718^{-68.95(0.1667)})$

  $= 15.968$ cm/jam

  $= 159.68$ mm/jam

## Titik 9




Berdasarkan persamaan linier diatas, maka didapatkan gradien, m = -0.0137 dan nilai konstanta jenis tanah (K) = 168.09 menggunakan rumus, k= -1/(m log 2.718).

- Perhitungan laju infiltrasi pada saat waktu konstan

  $f = f_c + (f_0 - f_c)\, e^{-Kt}$

  $f = 22.0 + (2904 - 22.0)\, 2.718^{-168.09(0.05)}$

  $f = 22.646$ cm/jam

  $f = 226.46$ mm/jam

- Perhitungan volume infiltrasi

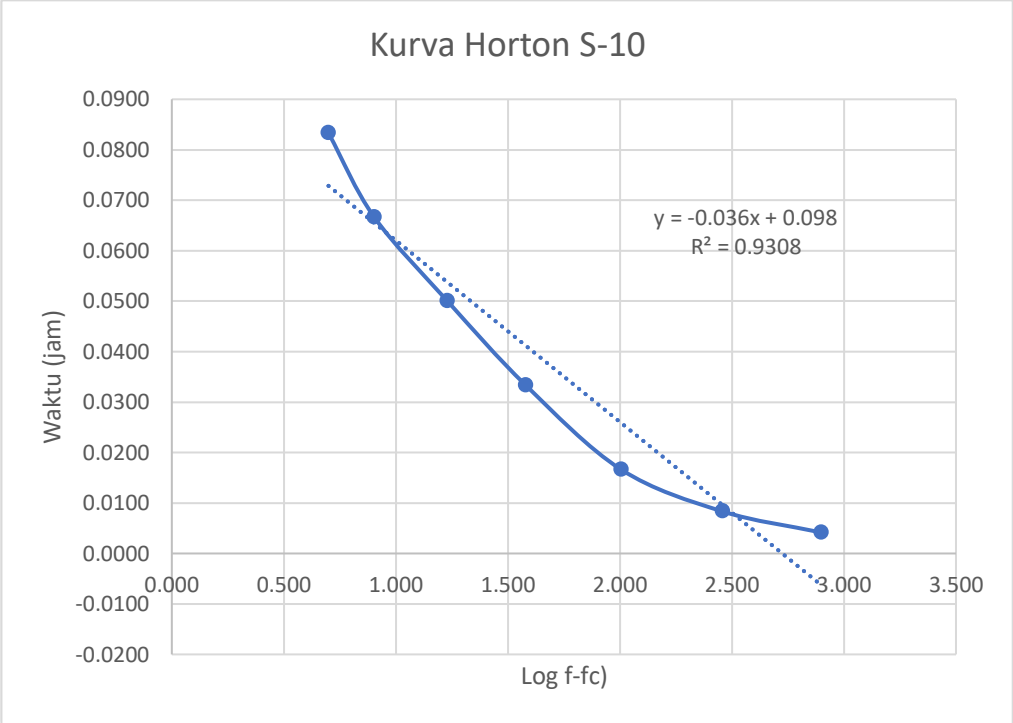
  $f(t) = f_c.t + 1/K\,(f_0 - f_c)(1- e^{-Kt})$

  $f(0.05) = (22.0 \times 0.05) + (1/168.09)(2904 - 22.0)(1- 2.718^{-168.09(0.05)})$

  $= 18.242$ cm/jam

  $= 182.42$ mm/jam

## Titik 10




Berdasarkan persamaan linier diatas, maka didapatkan gradien, m = -0.036 dan nilai konstanta jenis tanah (K) = 63.97 menggunakan rumus, k= -1/(m log 2.718).

- Perhitungan laju infiltrasi pada saat waktu konstan

  $f = f_c + (f_0 - f_c)\, e^{-Kt}$

  $f = 1.0 + (792 - 1.0)\, 2.718^{-63.97(0.1667)}$

  $f = 1.019$ cm/jam

  $f = 10.19$ mm/jam

- Perhitungan volume infiltrasi

  $f(t) = f_c.t + 1/K\,(f_0 - f_c)(1- e^{-Kt})$

  $f(0.1667) = (1.0 \times 0.1667) + (1/63.97)(792 - 1.0)(1- 2.718^{-63.97(0.1667)})$

  $= 12.532$ cm/jam

  $= 125.32$ mm/jam

# LAMPIRAN F
# PERHITUNGAN CURAH HUJAN

| Tahun/Bulan | Jan | Feb | Mar | Apr | Mei | Jun | Jul | Agu | Sep | Okt | Nov | Des | Curah Hujan Maksimal |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 2013 | 982 | 418 | 336 | 270 | 137 | 275 | 94 | 1 | 2 | 24 | 203 | 675 | 982 |
| 2014 | 836 | 313 | 311 | 282 | 105 | 134 | 30 | 6 | - | - | 117 | 673 | 836 |
| 2015 | 962 | 355 | 306 | 204 | 9 | 55 | - | - | - | - | 148 | 619 | 962 |
| 2016 | 384 | 724 | 221 | 119 | 44 | 47 | 13 | 0 | 79 | 425 | 149 | 545 | 724 |
| 2017 | 735 | 405 | 448 | 225 | 75 | 196 | 23 | 52 | 68 | 91 | 459 | 955 | 955 |
| 2018 | 787 | 714 | 574 | 167 | 32 | 121 | 49 | 1 | 1 | 12 | 156 | 858 | 858 |
| 2019 | 642 | 239 | 445 | 354 | 60 | 61 | 2 | 0 | 0 | 0 | 78 | 281 | 642 |
| 2020 | 572 | 539 | 264 | 100 | 186 | 73 | 9 | 16 | 23 | 54 | 249 | 924 | 924 |
| 2021 | 1195 | 434 | 680 | 430 | 65 | 75 | 43 | 64 | 115 | 108 | 328 | 964 | 1195 |

Pada nilai curah hujan maksimal, diambil curah hujan yang paling tinggi pada tiap-tiap tahun.

| Tahun | Xi | X | Xi-X | (Xi-X)^2 | (Xi-X)^3 | (Xi-X)^4 |
|---|---|---|---|---|---|---|
| 2013 | 982 | 884.3 | 97.7 | 9545.3 | 932574.8 | 91112561.2 |
| 2014 | 836 | 884.3 | -48.3 | 2332.9 | -112678.6 | 5442375.8 |
| 2015 | 962 | 884.3 | 77.7 | 6037.3 | 469097.4 | 36448870.5 |
| 2016 | 724 | 884.3 | -160.3 | 25696.1 | -4119083.2 | 660289041.3 |
| 2017 | 955 | 884.3 | 70.7 | 4998.5 | 353393.2 | 24984902.3 |
| 2018 | 858 | 884.3 | -26.3 | 691.7 | -18191.4 | 478435.1 |
| 2019 | 642 | 884.3 | -242.3 | 58709.3 | -14225261.0 | 3446780732.3 |
| 2020 | 924 | 884.3 | 39.7 | 1576.1 | 62570.8 | 2484059.7 |
| 2021 | 1195 | 884.3 | 310.7 | 96534.5 | 29993266.0 | 9318907759.6 |
| 2022 | 765 | 884.3 | -119.3 | 14232.5 | -1697936.1 | 202563771.6 |

Perhitungan rata-rata (X) =

$$= \frac{\Sigma Xi}{n} = \frac{8843}{10} = 884.3$$

Perhitungan standar deviasi (S) (dalam excel) = SQRT (Σ(Xi-X)^2/29)
= SQRT (220354.1/29)
= 87.2

Hujan rencana tahun metode GUMBELL

| Tahun | Yn | Sn | Yt | K | S | X | Xt |
|---|---|---|---|---|---|---|---|
| 2 | 0.5 | 0.9 | 0.4 | -0.1 | 87.2 | 884.3 | 872.5 |
| 5 | 0.5 | 0.9 | 1.5 | 1.1 | 87.2 | 884.3 | 976.5 |
| 10 | 0.5 | 0.9 | 2.3 | 1.8 | 87.2 | 884.3 | 1045.4 |
| 50 | 0.5 | 0.9 | 3.9 | 3.6 | 87.2 | 884.3 | 1197.0 |
| 100 | 0.5 | 0.9 | 4.6 | 4.3 | 87.2 | 884.3 | 1261.1 |

Perhitungan nilai K =

- Tahun 2 = (0.4-0.5)/0.9 = -0.1
- Tahun 5 = (1.5-0.5)/0.9 = 1.1

ıun 10 = (2.3-0.5)/0.9 = 1.8

ıun 50 = (3.9-0.5)/0.9 = 3.6

ıun 100 = (4.6-0.5)/0.9 = 4.3

Perhitungan nilai curah hujan (Xt) =

- Tahun 2 = 884.3+(-0.1 x 87.2) = 872.5
- Tahun 5 = 884.3+(1.1 x 87.2) = 976.5
- Tahun 10 = 884.3+(1.8 x 87.2) = 1045.4
- Tahun 50 = 884.3+(3.6 x 87.2) = 1197
- Tahun 100 = 884.3+(4.3 x 87.2) = 1261.1

# LAMPIRAN G
# DATA PENGUKURAN GEOLISTRIK

## Titik 1

Koordinat : (-5.075614, 119.523908)  Lokasi : Bumi Permata Sudiang
Arah lintasan : N 314$^{o}$ E
Tanggal : 12 September 2023

| NO | MN/2 (m) | AB/2 (m) | K | V1 mVolt | V2 mVolt | V rata-rata mVolt | I1 mA | I2 mA | I Rata-rata mA | $\rho_a$ ohm-m |
|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 0.5 | 1.5 | 6.286 | 364.8 | 355.0 | 359.9 | 98.4 | 98.3 | 98.4 | 23.00 |
| 2 | 0.5 | 2.5 | 18.857 | 195.9 | 284.7 | 240.3 | 87.9 | 87.6 | 87.8 | 51.64 |
| 3 | 0.5 | 4 | 49.500 | 66.9 | 67.7 | 67.3 | 101.4 | 101.3 | 101.4 | 32.87 |
| 4 | 0.5 | 6 | 112.357 | 7.8 | 7.1 | 7.5 | 84.8 | 85.9 | 85.4 | 9.81 |
| 5 | 0.5 | 8 | 200.357 | 1.3 | 2.2 | 1.8 | 95.8 | 95.5 | 95.7 | 3.67 |
| 6 | 2.5 | 8 | 36.300 | 38.9 | 38.8 | 38.9 | 95.3 | 95.5 | 95.4 | 14.78 |
| 7 | 2.5 | 10 | 58.929 | 14.9 | 15.9 | 15.4 | 102.8 | 102.8 | 102.8 | 8.83 |
| 8 | 2.5 | 15 | 137.500 | 3.5 | 2.7 | 3.1 | 81.2 | 80.0 | 80.6 | 5.29 |
| 9 | 2.5 | 20 | 247.500 | 0.9 | 0.6 | 0.8 | 95.4 | 95.0 | 95.2 | 1.95 |
| 10 | 2.5 | 30 | 561.786 | 0.2 | 0.7 | 0.5 | 78.5 | 79.9 | 79.2 | 3.19 |
| 11 | 10 | 30 | 125.714 | 1.0 | 1.8 | 1.4 | 74.2 | 74.5 | 74.4 | 2.37 |
| 12 | 10 | 40 | 235.714 | 0.2 | 0.3 | 0.3 | 103.2 | 103.2 | 103.2 | 0.57 |
| 13 | 10 | 50 | 377.143 | 1.4 | 0.1 | 0.8 | 106.4 | 106.4 | 106.4 | 2.66 |
| 14 | 10 | 60 | 550.000 | 0.2 | 0.1 | 0.2 | 108.3 | 107.3 | 107.8 | 0.77 |
| 15 | 10 | 75 | 868.214 | 0.8 | 0.3 | 0.6 | 108.5 | 108.5 | 108.5 | 4.40 |
|  |  | 75 | 314.286 | 0.5 | 0.7 | 0.6 | 108.5 | 108.5 | 108.5 | 1.74 |
|  |  | 100 | 589.286 | 0.9 | 0.1 | 0.5 | 109.4 | 109.3 | 109.4 | 2.69 |
|  |  | 150 | 1375.000 |  |  |  |  |  |  |  |
|  |  | 200 | 2475.000 |  |  |  |  |  |  |  |

## Titik 2

Koordinat : (-5.081235, 119.530381)  Lokasi : Bumi Permata Sudiang
Arah lintasan : N 269° E
Tanggal : 12 September 2023

| NO | MN/2 (m) | AB/2 (m) | K | V1 mVolt | V2 mVolt | V rata-rata mVolt | I1 mA | I2 mA | I Rata-rata mA | $\rho_a$ ohm-m |
|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 0.5 | 1.5 | 6.286 | 127.2 | 1,168.0 | 1,167.0 | 105.8 | 100.1 | 100.0 | 73.35 |
| 2 | 0.5 | 2.5 | 18.857 | 151.2 | 168.5 | 159.9 | 102.8 | 102.5 | 102.7 | 29.36 |
| 3 | 0.5 | 4 | 49.500 | 41.3 | 47.8 | 44.6 | 103.5 | 104.6 | 104.1 | 21.19 |
| 4 | 0.5 | 6 | 112.357 | 9.8 | 13.8 | 11.8 | 98.0 | 97.8 | 97.9 | 13.54 |
| 5 | 0.5 | 8 | 200.357 | 3.5 | 6.8 | 5.2 | 105.9 | 105.7 | 105.8 | 9.75 |
| 6 | 2.5 | 8 | 36.300 | 54.0 | 56.7 | 55.4 | 105.9 | 105.8 | 105.9 | 18.98 |
| 7 | 2.5 | 10 | 58.929 | 28.1 | 30.6 | 29.4 | 105.4 | 104.7 | 105.1 | 16.46 |
| 8 | 2.5 | 15 | 137.500 | 9.2 | 12.0 | 10.6 | 105.6 | 105.3 | 105.5 | 13.82 |
| 9 | 2.5 | 20 | 247.500 | 4.8 | 6.0 | 5.4 | 104.7 | 104.6 | 104.7 | 12.77 |
| 10 | 2.5 | 30 | 561.786 | 2.0 | 1.3 | 1.7 | 105.5 | 105.1 | 105.3 | 8.80 |
| 11 | 10 | 30 | 125.714 | 10.3 | 12.7 | 11.5 | 105.3 | 105.4 | 105.4 | 13.72 |
| 12 | 10 | 40 | 235.714 | 5.3 | 4.6 | 5.0 | 106.8 | 106.7 | 106.8 | 10.93 |
| 13 | 10 | 50 | 377.143 | 2.3 | 1.9 | 2.1 | 102.6 | 102.6 | 102.6 | 7.72 |
| 14 | 10 | 60 | 550.000 | 2.2 | 0.5 | 1.4 | 101.0 | 100.9 | 101.0 | 7.36 |
| [illegible] | [illegible] | 75 | 868.214 | 2.6 | 0.3 | 1.5 | 105.9 | 105.7 | 105.8 | 11.90 |
| [illegible] | [illegible] | 75 | 314.286 | 1.1 | 1.9 | 1.5 | 105.8 | 105.7 | 105.8 | 4.46 |
| [illegible] | [illegible] | 100 | 589.286 | 1.8 | 0.2 | 1.0 | 107.8 | 107.8 | 107.8 | 5.47 |
| [illegible] | [illegible] | 150 | 1375.000 | | | | | | | |
| [illegible] | [illegible] | 200 | 2475.000 | | | | | | | |

# LAMPIRAN H
# KARTU KONSULTASI TUGAS AKHIR

## Lampiran B 10

## Kartu Konsultasi Tugas Akhir

**JUDUL:** Analisis Laju Infiltrasi untuk Rancangan Sumur Resapan di Daerah Bumi Permata Sudiang

(Konsultasi minimal 8 kali)

| TANGGAL | MATERI KONSULTASI | PARAF DOSEN |
|---|---|---|
| 13/03/2024 | - JUDUL<br>- PETA LOKASI<br>- DATA AYAKAN<br>- PETA GEOLOGI<br>- BAB IV (PENGOLAHAN DATA PADA GEOLISTRIK DAN GEOSTUDIO) | |
| 22/03/2024 | - DATA AYAKAN (GRAFIK)<br>- PETA GEOLOGI<br>- PEMODELAN GEOSTUDIO | |
| 28/03/2024 | - BAGAN ALIR<br>- PETA GEOLOGI<br>- PEMODELAN GEOSTUDIO | |
| 29/03/2024 | - ARTIKEL<br>- POSTER | |
| 30/03/2024 | - ARTIKEL | |
| 26/04/2024 | - TYPO<br>- BAGAN ALIR<br>- PETA GEOLOGI<br>- TABEL<br>- BAB 4 PEMBAHASAN<br>- PEMODELAN PAKAI GEOSTUDIO<br>- LAMPIRAN | |

| TANGGAL | MATERI KONSULTASI | PARAF DOSEN |
|---|---|---|
| 19/06/2024 | - Kesimpulan<br>- Peta Geologi<br>- Pemodelan<br>- Artikel | |
| 25/06/2024 | - Grafik Perubahan Elevasi MAT<br>- Judul<br>- Artikel | |
| | - Artikel | |
| | - Artikel | |