

DAFTAR PUSTAKA

- Adji, S. (2009). *Resistance & Propulsion Modul 1: Introduction to Ship Resistance*. Surabaya: ITS.
- Alfian, Abi, D., & Chrismianto, D. (2016). Analisa Hambatan Penambahan Stern Wedge pada KRI Todak menggunakan metode CFD (Computational Fluid Dynamic). *Jurnal Perkapalan*.
- Avicenna, H., & Utama, P. I. (2016). Analisa Pengaruh Konfigurasi Skeg Terhadap Hambatan Dan Gerak Kapal Dengan Metode Computational Fluid Dynamics. *Jurnal Teknik ITS*.
- Bambang, T., Jadmiko, E., & Triyono. (n.d.). Kajian Teknis Penambahan Skeg pada Kapal Patroli Tipe 36m dengan Metode CFD.
- Baso, S., Ardianti, A., Rosmani, & A., A. (2021). An Extended Validation of Free CFD Application to Ship Resistance Prediction for Using In Preliminary Design Stage. *Journal of Engineering Science and Technology*, 16(3), 2544-2561.
- Djabbar, M., & Rosmani. (2011). *Buku Ajar Tahanan Kapal*. Makassar: Departemen Teknik Perkapalan, Universitas Hasanuddin.
- Dwitara, I., Santoso, A., & Amiadji. (2013). Analisa Aliran dan Tekanan pada Perubahan Bentuk Skeg Kapal Tongkang dengan Pendekatan CFD. *Jurnal Teknik POMITS*.
- Harvald, S. A. (1983). *Resistance and Propulsion Of Ships*. Denmark, Lyngby: Departement of Ocean Engineering, The Technical Univercsity of Denmark.
- Hilmi. (2009). *Simulasi Uji Tarik Kapal Model Untuk Mengetahui Hambatan dan Daya Efektif Pada Kapal Sebenarnya*. Depok: FT, UI.
- Holtrop, J., & Mannen, G. G. (1982). *An Approximate Power Prediction Method*. *Internasional Shipbuilding Progress*.
- IHL. (2021). *Pengujian Resistance Model Kapal Ferry Ro-Ro 1500 GT*. Surabaya: Badan Pengkajian dan Penerapan Teknologi, Balai Teknologi Hidrodinamika.
- Kim, K., Tillig, F., Bathfield, N., & Liljenberg, H. (2014). Optimalisasi Hidrodinamik Kapal LNG Twin-Skeg melalui CFD dan Pengujian Model. *International Journal of Naval Architecture and Ocean Engineering*, 392-405.
- Lammeren, V. (1962). *Resistance, Propulsion and Steering of Ships*. Technical Publishing Company H. Stam.
- Lewis, E. V. (1988). *Principles of Naval Architecture*. Jersey City: The Society of Naval Architects and Marine Engineers.
- Maulana, A. (2011). *Optimalisasi Hambatan Kapal Skala Penuh Berdasarkan Analisa Uji Tarik Kapal Model*. Depok: FT, UI.
- Putra, A. P., Munazid, A., & Suwasono, S. (2017). Performance Pemasangan Skeg Di Linggi Haluan Pada Kapal. *Seminar Nasional Kelautan XII*.
- Rosmani. (2013). Pengaruh Bentuk Lambung Kapal Terhadap Tahanan Kapal. *Proceeding Hasil Penelitian, Fakultas Teknik Universitas Hasanuddin*.
- Sardjadi, D. (2003). *Mekanika Fluida*. Bandung.

- Slade, S. (2017, December 20). *NavWeaps*. Retrieved from History and Technology Skeg Design: http://www.navweaps.com/index_tech/tech-014.php
- Sutiyo. (2014). *Studi Pengaruh Intervensi Terhadap Hambatan Pada Kapal Katamaran Simetri melalui CFD (Computational FLuid Dynamic)*. Surabaya.
- Wibawa, N. A., & Kurniawati, H. A. (2017). Desain Kapal Ro-Ro (Roll on-Roll off) sebagai Sarana Penyeberangan Rute Pelabuhan Benoa-Nusa Penida Bali. *Jurnal Teknik ITS*, Vol.6, No.2.
- Widodo, Yasim, A., Rina, & Ghofur, A. (2018). Studi Variasi Model Skeg berdasarkan Tahanan dan Pola Aliran yang Melewati Lambung Barge Berpengerak Sendiri-Kasus pada Desain Wahana Pembongkaran Alpo. *Jurnal Wave*, 73-80.

LAMPIRAN

Lampiran 1 Penentuan nilai kecepatan model kapal (V_m)

Berdasarkan Persamaan 23 dimana $\frac{V_m}{\sqrt{g \cdot L_m}} = \frac{V_s}{\sqrt{g \cdot L_s}}$ maka dalam menentukan kecepatan model kapal sebagai berikut.

a. Kecepatan 9 knot

$$\begin{aligned} F_{n_s} &= \frac{V_s}{\sqrt{g \cdot L_s}} \\ &= \frac{4,630}{\sqrt{9,81 \times 76,6}} \\ &= 0,169 \end{aligned}$$

$$F_{n_s} = F_{n_m} = 0,169$$

Maka,

$$\begin{aligned} F_{n_m} &= \frac{V_m}{\sqrt{g \cdot L_m}} \\ 0,169 &= \frac{V_m}{\sqrt{9,81 \times 1,92}} \\ V_m &= 0,732 \text{ m/s} \end{aligned}$$

b. Kecepatan 10 knot

$$\begin{aligned} F_{n_s} &= \frac{V_s}{\sqrt{g \cdot L_s}} \\ &= \frac{5,144}{\sqrt{9,81 \times 76,6}} \\ &= 0,188 \end{aligned}$$

$$F_{n_s} = F_{n_m} = 0,188$$

Maka,

$$\begin{aligned} F_{n_m} &= \frac{V_m}{\sqrt{g \cdot L_m}} \\ 0,188 &= \frac{V_m}{\sqrt{9,81 \times 1,92}} \\ V_m &= 0,813 \text{ m/s} \end{aligned}$$

c. Kecepatan 11 knot

$$\begin{aligned} F_{n_s} &= \frac{V_s}{\sqrt{g \cdot L_s}} \\ &= \frac{5,658}{\sqrt{9,81 \times 76,6}} \\ &= 0,207 \end{aligned}$$

$$F_{n_s} = F_{n_m} = 0,207$$

Maka,

$$Fn_m = \frac{V_m}{\sqrt{g \cdot L_m}}$$

$$0,207 = \frac{V_m}{\sqrt{9,81 \times 1,92}}$$

$$V_m = 0,895 \text{ m/s}$$

d. Kecepatan 12 knot

$$Fn_s = \frac{V_s}{\sqrt{g \cdot L_s}}$$

$$= \frac{6,173}{\sqrt{9,81 \times 76,6}}$$

$$= 0,225$$

$$Fn_s = Fn_m = 0,225$$

Maka,

$$Fn_m = \frac{V_m}{\sqrt{g \cdot L_m}}$$

$$0,225 = \frac{V_m}{\sqrt{9,81 \times 1,92}}$$

$$V_m = 0,976 \text{ m/s}$$

e. Kecepatan 13 knot

$$Fn_s = \frac{V_s}{\sqrt{g \cdot L_s}}$$

$$= \frac{6,687}{\sqrt{9,81 \times 76,6}}$$

$$= 0,244$$

$$Fn_s = Fn_m = 0,244$$

Maka,

$$Fn_m = \frac{V_m}{\sqrt{g \cdot L_m}}$$

$$0,244 = \frac{V_m}{\sqrt{9,81 \times 1,92}}$$

$$V_m = 1,057 \text{ m/s}$$

f. Kecepatan 14 knot

$$Fn_s = \frac{V_s}{\sqrt{g \cdot L_s}}$$

$$= \frac{7,202}{\sqrt{9,81 \times 76,6}}$$

$$= 0,263$$

$$Fn_s = Fn_m = 0,263$$

Maka,

$$Fn_m = \frac{V_m}{\sqrt{g \cdot L_m}}$$

$$0,263 = \frac{V_m}{\sqrt{9,81 \times 1,92}}$$

$$V_m = 1,139 \text{ m/s}$$

g. Kecepatan 15 knot

$$Fn_s = \frac{V_s}{\sqrt{g \cdot L_s}}$$

$$= \frac{7,716}{\sqrt{9,81 \times 76,6}}$$

$$= 0,282$$

$$Fn_s = Fn_m = 0,282$$

Maka,

$$Fn_m = \frac{V_m}{\sqrt{g \cdot L_m}}$$

$$0,282 = \frac{V_m}{\sqrt{9,81 \times 1,92}}$$

$$V_m = 1,220 \text{ m/s}$$

h. Kecepatan 16 knot

$$Fn_s = \frac{V_s}{\sqrt{g \cdot L_s}}$$

$$= \frac{8,230}{\sqrt{9,81 \times 76,6}}$$

$$= 0,300$$

$$Fn_s = Fn_m = 0,300$$

Maka,

$$Fn_m = \frac{V_m}{\sqrt{g \cdot L_m}}$$

$$0,300 = \frac{V_m}{\sqrt{9,81 \times 1,92}}$$

$$V_m = 1,301 \text{ m/s}$$

i. Kecepatan 17 knot

$$Fn_s = \frac{V_s}{\sqrt{g \cdot L_s}}$$

$$= \frac{8,745}{\sqrt{9,81 \times 76,6}}$$

$$= 0,319$$

$$Fn_s = Fn_m = 0,319$$

Maka,

$$Fn_m = \frac{V_m}{\sqrt{g \cdot L_m}}$$

$$0,319 = \frac{V_m}{\sqrt{9,81 \times 1,92}}$$

$$V_m = 1,383 \text{ m/s}$$

j. Kecepatan 18 knot

$$Fn_s = \frac{V_s}{\sqrt{g \cdot L_s}}$$

$$= \frac{9,259}{\sqrt{9,81 \times 76,6}}$$

$$= 0,338$$

$$Fn_s = Fn_m = 0,338$$

Maka,

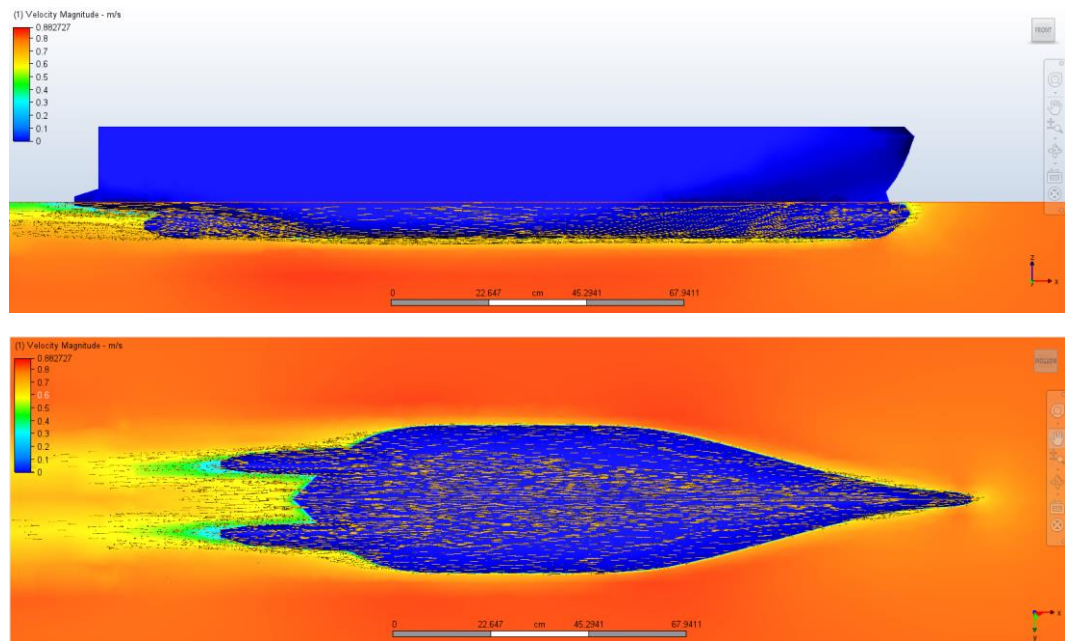
$$Fn_m = \frac{V_m}{\sqrt{g \cdot L_m}}$$

$$0,338 = \frac{V_m}{\sqrt{9,81 \times 1,92}}$$

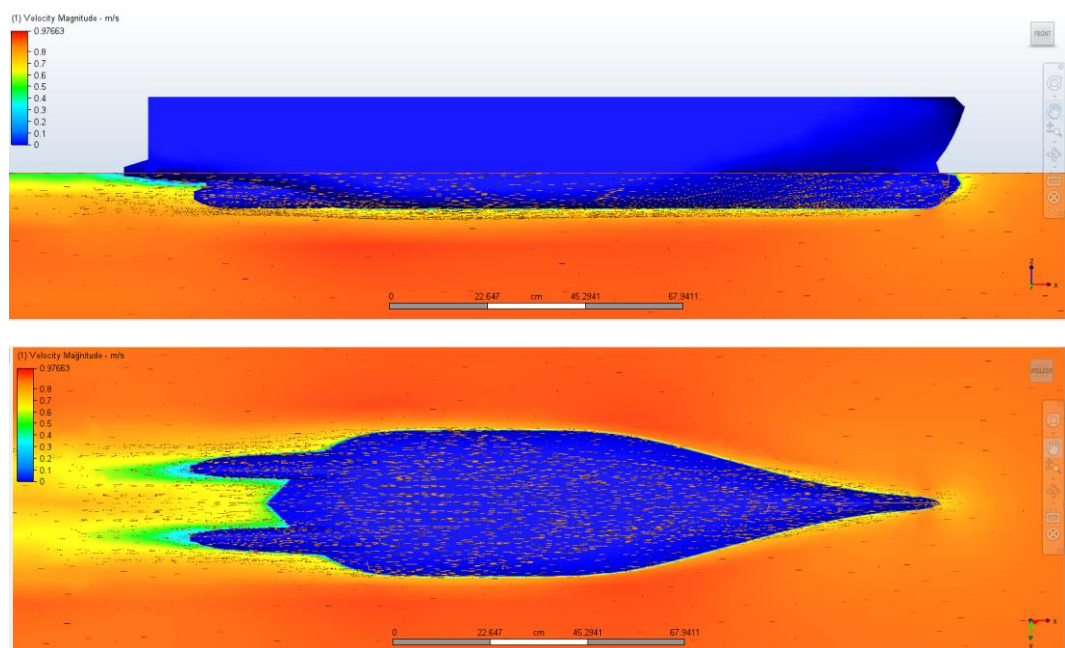
$$V_m = 1,464 \text{ m/s}$$

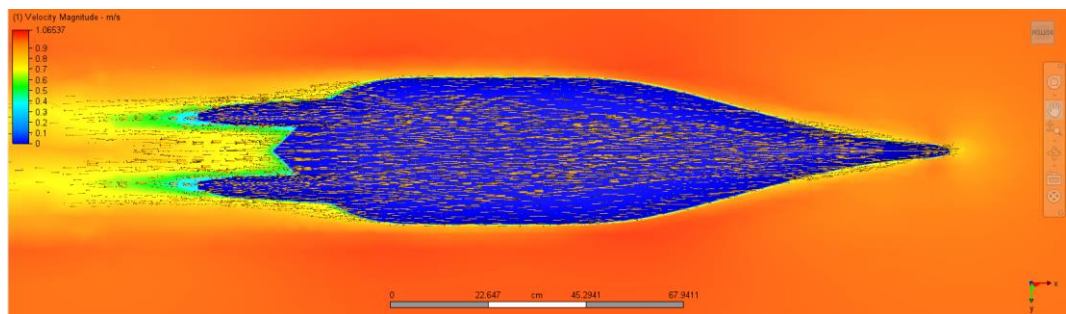
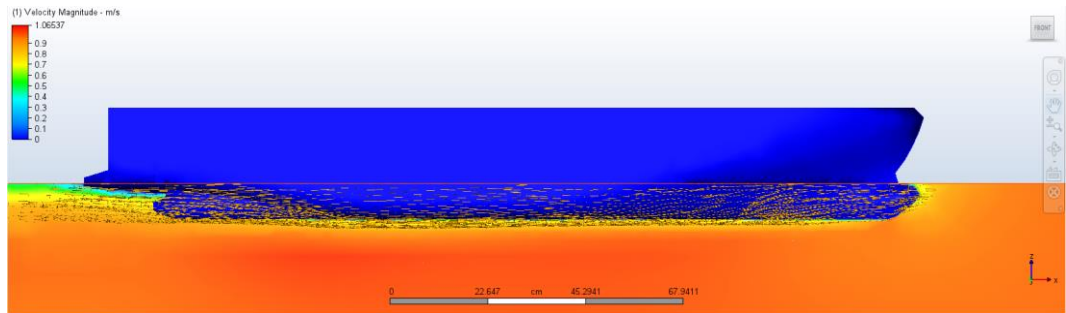
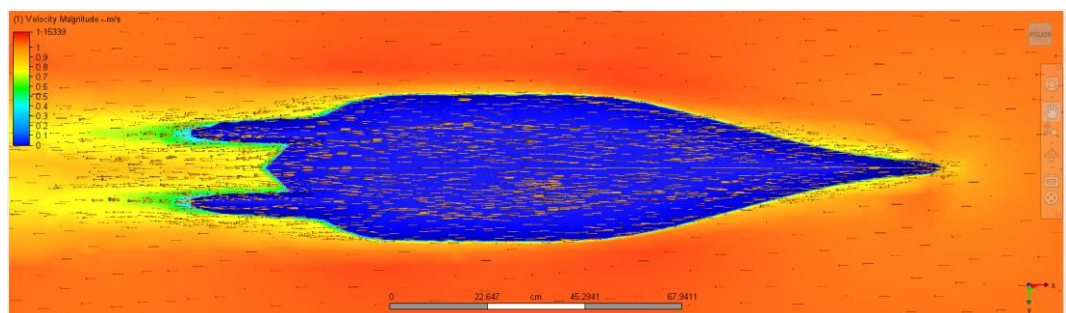
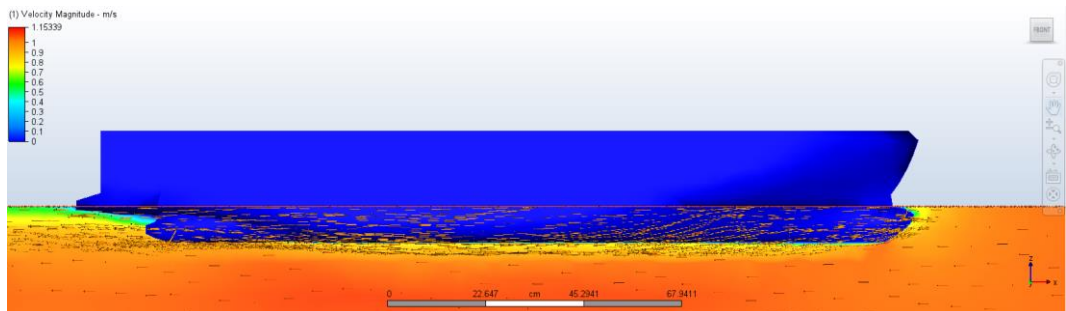
Lampiran 2 Visualisasi *velocity magnitude* pada setiap variasi kecepatan

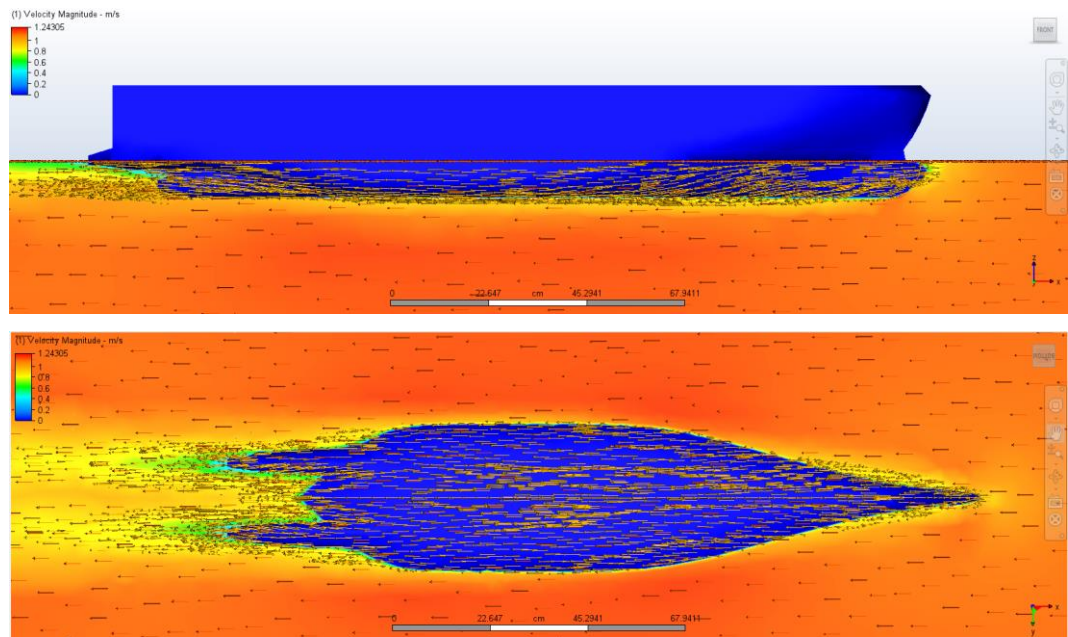
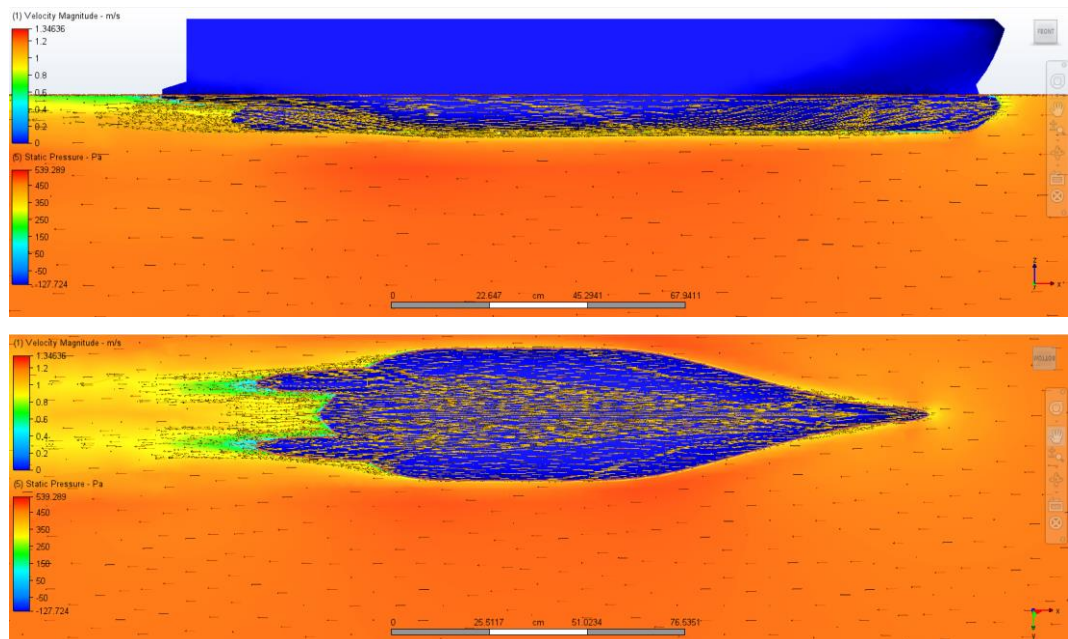
a. Kecepatan 0,813 m/s

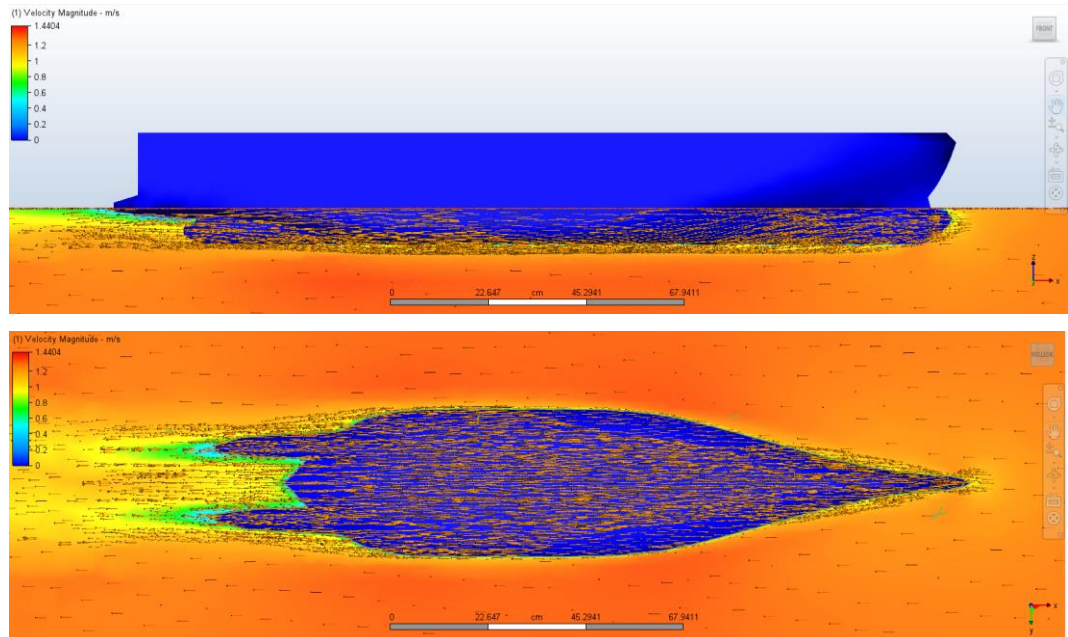
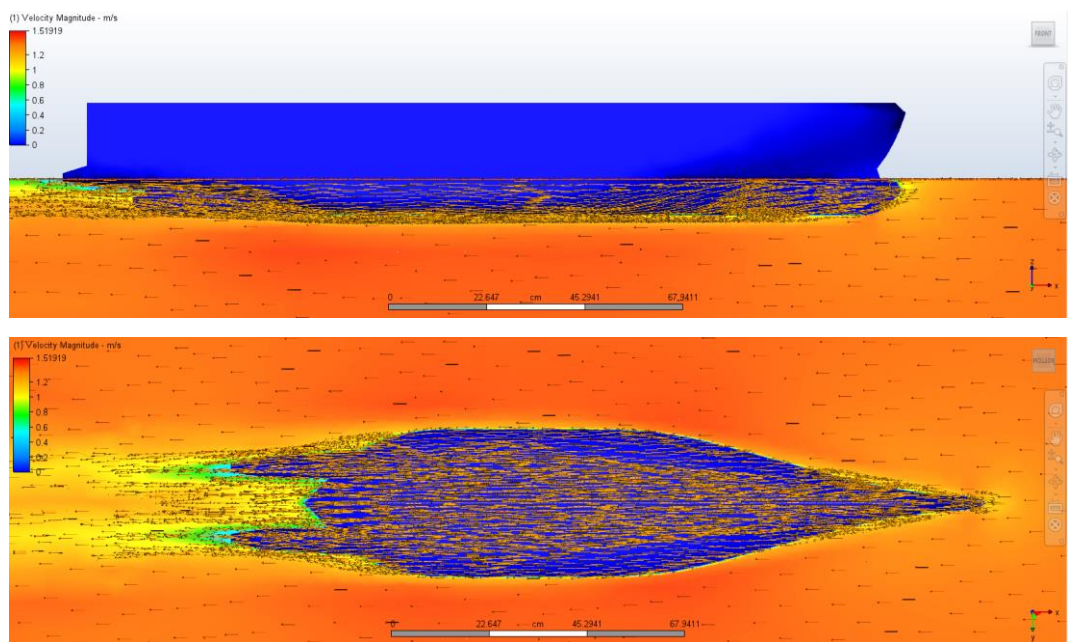


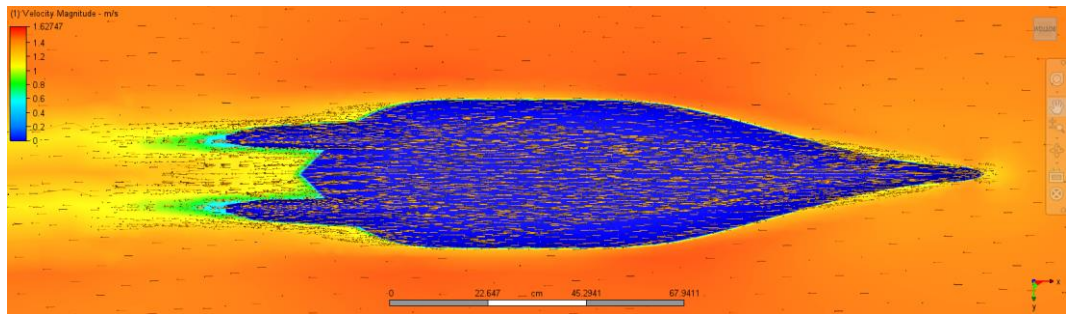
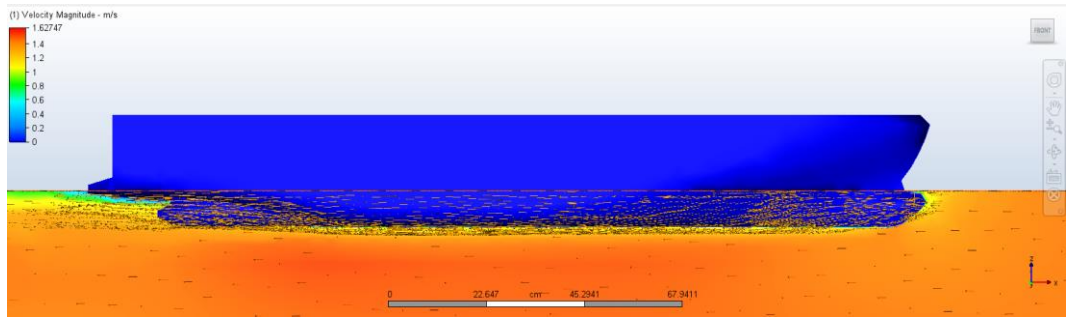
b. Kecepatan 0,895 m/s



c. Kecepatan 0,976 m/s**d. Kecepatan 1,057 m/s**

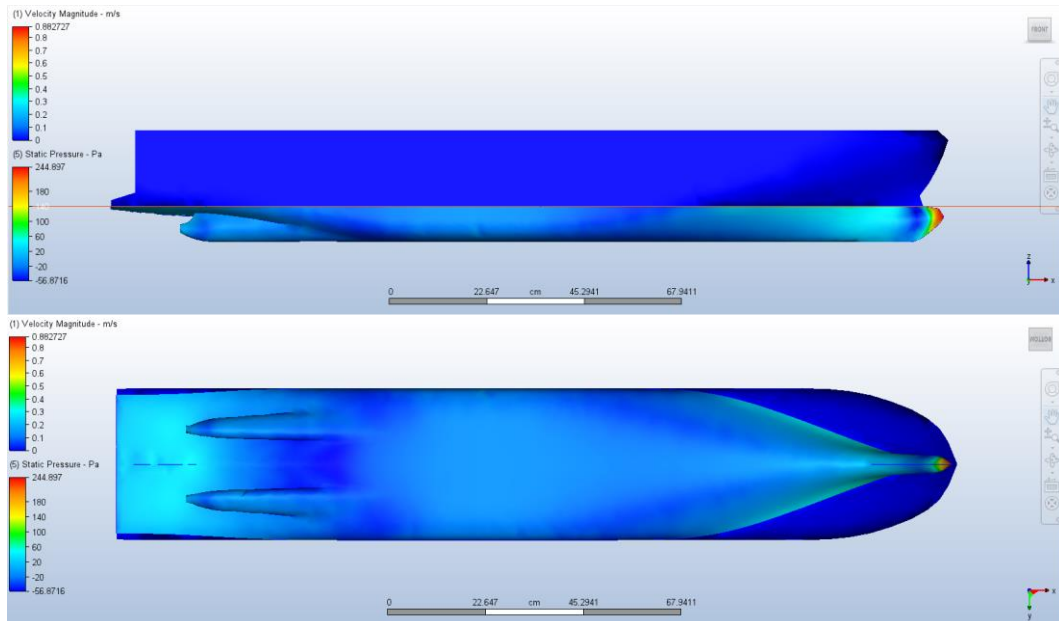
e. Kecepatan 1,139 m/s**f. Kecepatan 1,220 m/s**

g. Kecepatan 1,301 m/s**h. Kecepatan 1,383 m/s**

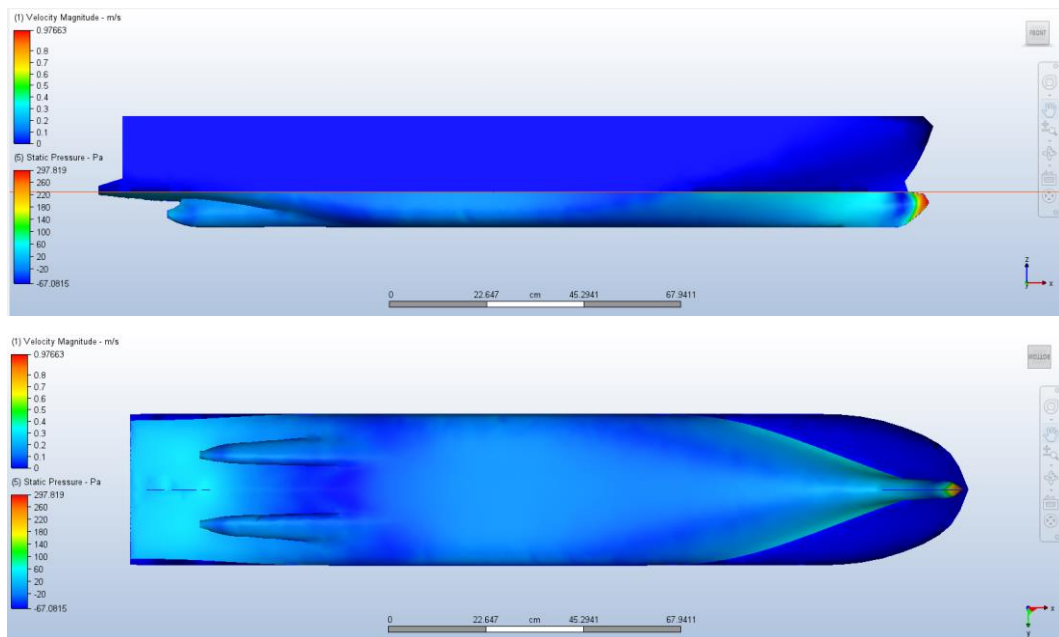
i. Kecepatan 1,464 m/s

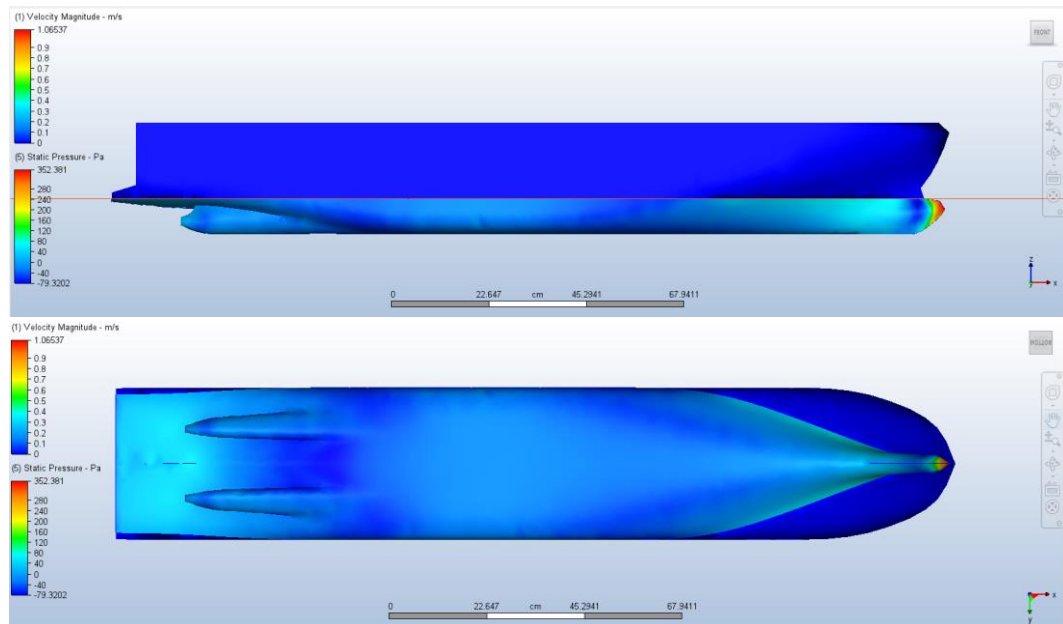
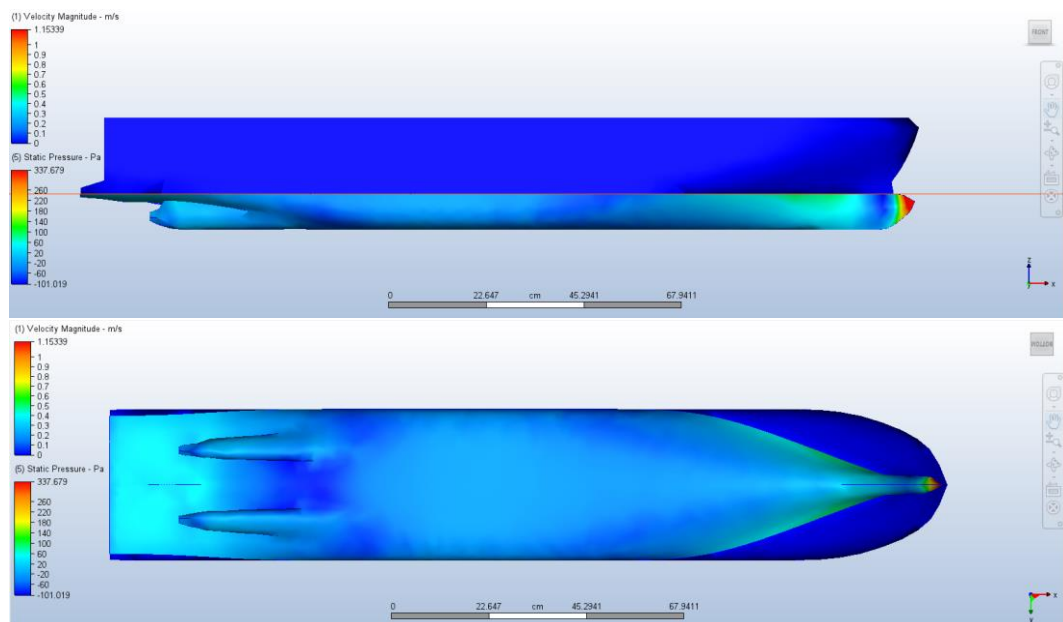
Lampiran 3 Visualisasi *Static Pressure* pada setiap variasi kecepatan

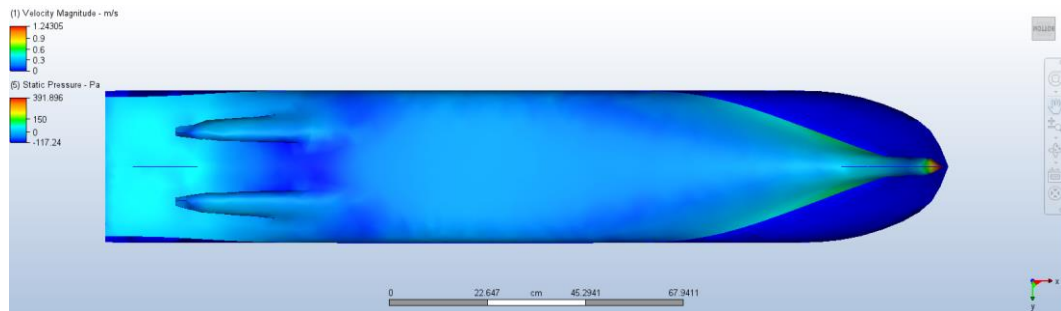
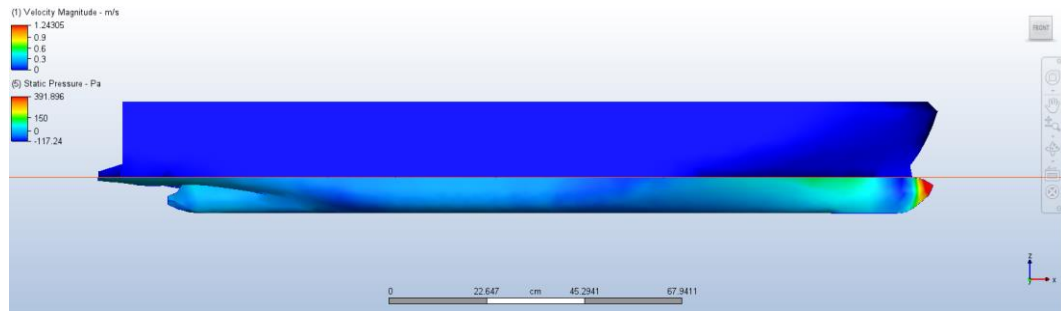
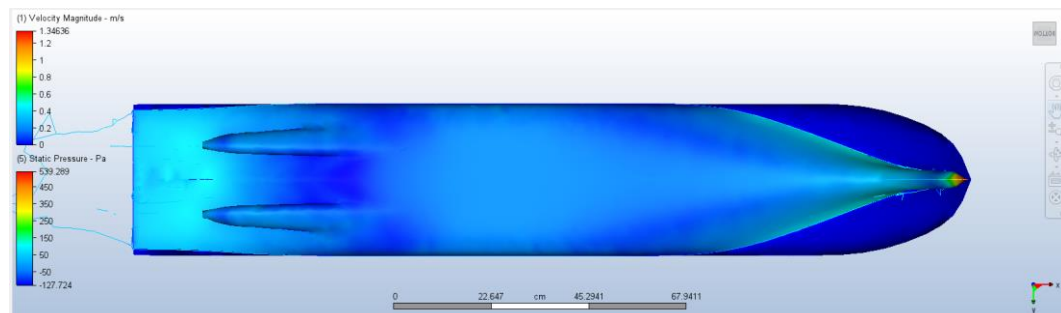
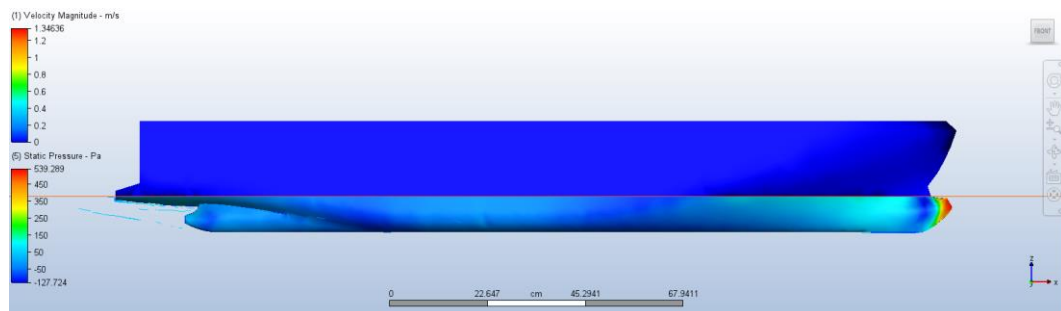
a. Kecepatan 0,813 m/s

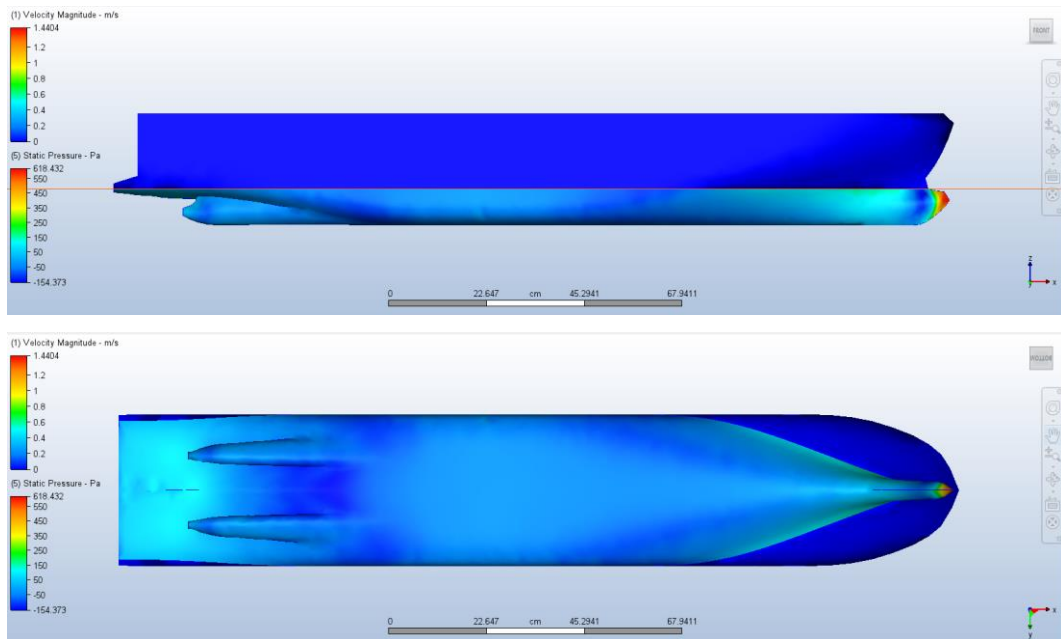
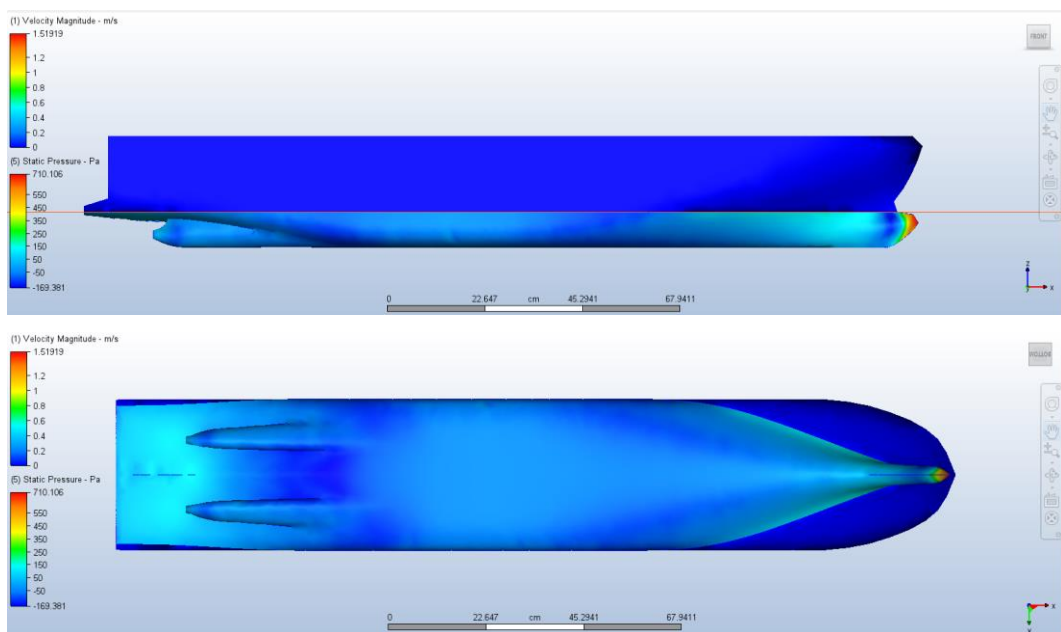


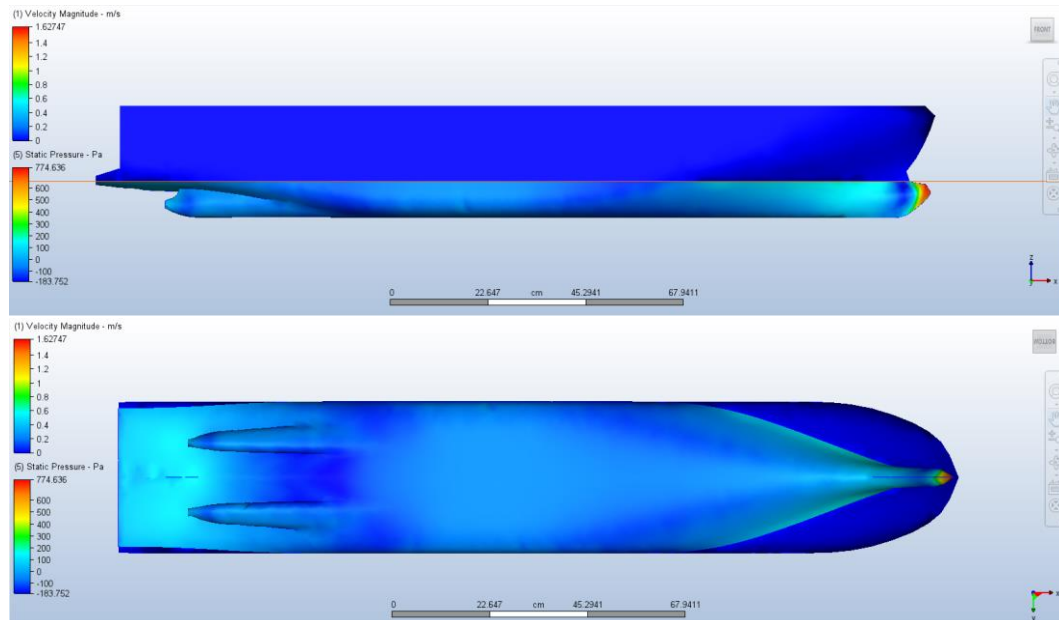
b. Kecepatan 0,895 m/s



c. Kecepatan 0,976 m/s**d. Kecepatan 1,057 m/s**

e. Kecepatan 1,139 m/s**f. Kecepatan 1,220 m/s**

g. Kecepatan 1,301 m/s**h. Kecepatan 1,383 m/s**

i. Kecepatan 1,464 m/s

Lampiran 4 Nilai *Static Pressure* pada setiap variasi kecepatan

a. Kecepatan 0,813 m/s

Var	Mean	at	Max	at	Min
Vx Vel	-8.02895e+01	42602	+2.67274e+01	54111	-8.67088e+01 cm/s
Vy Vel	+3.84330e-03	59817	+3.01456e+01	54873	-3.30902e+01 cm/s
Vz Vel	-1.58166e-02	285404	+1.36126e+01	56574	-2.67783e+01 cm/s
Press	-5.68094e+00	1492	+2.44897e+03	104	-5.68716e+02 dyne/cm ²
Temp	+0.00000e+00	1232	+0.00000e+00	1243	+0.00000e+00 C
TurbK	+2.94748e+00	52585	+3.70445e+02	1722	+1.14040e-05 cm ² /s ²
TurbD	+1.79264e+01	1561	+9.43864e+04	227885	+4.08184e-03 cm ² /s ³

b. Kecepatan 0,895 m/s

Var	Mean	at	Max	at	Min
Vx Vel	-8.83497e+01	42602	+2.79660e+01	54111	-9.61679e+01 cm/s
Vy Vel	+1.88014e-03	59817	+3.39816e+01	54873	-3.64537e+01 cm/s
Vz Vel	-2.06974e-02	285404	+1.45624e+01	55728	-2.80923e+01 cm/s
Press	-6.80169e+00	1507	+2.97819e+03	2148	-6.70815e+02 dyne/cm ²
Temp	+0.00000e+00	1232	+0.00000e+00	1243	+0.00000e+00 C
TurbK	+3.34310e+00	52585	+4.61543e+02	1722	+1.14040e-05 cm ² /s ²
TurbD	+2.16835e+01	1561	+9.95059e+04	227885	+3.29780e-03 cm ² /s ³

c. Kecepatan 0,976 m/s

Var	Mean	at	Max	at	Min
Vx Vel	-9.63526e+01	42602	+3.04012e+01	54111	-1.04664e+02 cm/s
Vy Vel	-1.15678e-03	59817	+3.67998e+01	54873	-3.97633e+01 cm/s
Vz Vel	-2.08858e-02	285404	+1.60846e+01	56574	-3.23658e+01 cm/s
Press	-8.21953e+00	1530	+3.52381e+03	2148	-7.93202e+02 dyne/cm ²
Temp	+0.00000e+00	1232	+0.00000e+00	1243	+0.00000e+00 C
TurbK	+3.69735e+00	52591	+5.68379e+02	1722	+1.14040e-05 cm ² /s ²
TurbD	+2.65969e+01	1561	+1.17376e+05	227885	+3.93534e-03 cm ² /s ³

d. Kecepatan 1,057 m/s

Var	Mean	at	Max	at	Min
Vx Vel	-9.75262e+01	15052	+3.54092e+01	26929	-1.13428e+02 cm/s
Vy Vel	-1.78249e-02	32635	+4.21947e+01	27691	-4.35847e+01 cm/s
Vz Vel	-9.33008e-02	54848	+1.88288e+01	28540	-3.27078e+01 cm/s
Press	-4.92046e+01	1104	+4.24082e+03	1401	-1.00130e+03 dyne/cm ²
Temp	+0.00000e+00	906	+0.00000e+00	910	+0.00000e+00 C
TurbK	+1.32560e+01	25406	+3.95242e+02	1320	+1.14040e-05 cm ² /s ²
TurbD	+2.33172e+02	25324	+1.06681e+05	64836	+9.23481e-03 cm ² /s ³

e. Kecepatan 1,139 m/s

Var	Mean	at	Max	at	Min
Vx Vel	-1.05187e+02	15052	+3.88958e+01	26929	-1.22425e+02 cm/s
Vy Vel	-1.93748e-02	32635	+4.55220e+01	27691	-4.69997e+01 cm/s
Vz Vel	-8.91046e-02	54848	+2.08218e+01	28540	-3.52942e+01 cm/s
Press	-5.79807e+01	1109	+4.92842e+03	1401	-1.17930e+03 dyne/cm ²
Temp	+0.00000e+00	31	+0.00000e+00	615	+0.00000e+00 C
TurbK	+1.52303e+01	25406	+4.67438e+02	1112	+1.14040e-05 cm ² /s ²
TurbD	+2.86987e+02	1159	+1.22508e+05	55276	+1.00092e-02 cm ² /s ³

f. Kecepatan 1,220 m/s

Var	Mean	at	Max	at	Min
Vx Vel	-1.21020e+02	47260	+4.21603e+01	58723	-1.31516e+02 cm/s
Vy Vel	-9.43411e-04	64429	+4.94433e+01	59485	-4.94085e+01 cm/s
Vz Vel	-5.13945e-02	248895	+2.24440e+01	60340	-3.84050e+01 cm/s
Press	-6.25157e+00	1574	+5.53210e+03	1847	-1.33083e+03 dyne/cm ²
Temp	+2.69393e+01	51941	+3.73479e+01	56894	-2.68202e+01 C
TurbK	+5.52301e+00	57198	+7.08733e+02	1766	+1.14040e-05 cm ² /s ²
TurbD	+3.99637e+01	1605	+1.75765e+05	248644	+5.29392e-03 cm ² /s ³

g. Kecepatan 1,301 m/s

Var	Mean	at	Max	at	Min
Vx Vel	-1.28465e+02	35423	+4.49708e+01	46900	-1.41616e+02 cm/s
Vy Vel	+5.17062e-04	52606	+5.01372e+01	47662	-5.20151e+01 cm/s
Vz Vel	-2.51781e-02	222254	+2.23882e+01	48517	-4.22020e+01 cm/s
Press	-1.51241e+01	1426	+6.18432e+03	35425	-1.54373e+03 dyne/cm ²
Temp	+0.00000e+00	881	+0.00000e+00	34	+0.00000e+00 C
TurbK	+5.90355e+00	45374	+7.44473e+02	1612	+1.14040e-05 cm ² /s ²
TurbD	+6.32639e+01	45373	+1.80397e+05	34191	+1.82173e-02 cm ² /s ³

h. Kecepatan 1,383 m/s

Var	Mean	at	Max	at	Min
Vx Vel	-1.36607e+02	42602	+4.95602e+01	54111	-1.49545e+02 cm/s
Vy Vel	+4.49996e-03	59817	+5.27595e+01	54873	-5.64429e+01 cm/s
Vz Vel	-2.27398e-02	285404	+2.42997e+01	55728	-4.30981e+01 cm/s
Press	-1.68815e+01	1511	+7.10106e+03	104	-1.69381e+03 dyne/cm ²
Temp	+0.00000e+00	1232	+0.00000e+00	1243	+0.00000e+00 C
TurbK	+6.18823e+00	52585	+8.57941e+02	1722	+1.14040e-05 cm ² /s ²
TurbD	+6.96067e+01	1561	+2.08615e+05	228200	+2.07665e-02 cm ² /s ³

i. Kecepatan 1,464 m/s

Var	Mean	at	Max	at	Min
Vx Vel	-1.35299e+02	15052	+5.09632e+01	26929	-1.58337e+02 cm/s
Vy Vel	+7.51843e-03	32635	+5.86778e+01	27691	-6.06335e+01 cm/s
Vz Vel	-1.17503e-01	54848	+2.69940e+01	28540	-4.55993e+01 cm/s
Press	-9.60061e+01	1128	+8.17798e+03	1401	-1.95359e+03 dyne/cm ²
Temp	+0.00000e+00	31	+0.00000e+00	615	+0.00000e+00 C
TurbK	+2.32421e+01	25406	+6.51434e+02	16	+1.14040e-05 cm ² /s ²
TurbD	+5.56907e+02	1159	+1.73711e+05	97	+2.76839e-03 cm ² /s ³

Lampiran 5 Hasil nilai perhitungan *wall calculator* tahanan model kapal di setiap variasi kecepatan menggunakan *software CFD (Computational Fluid Dynamic)*

a. Kecepatan 0,813 m/s

Summary

```
-----
Total area, 13186.3, cm^2
TOTAL FX, -1.56276, Newton
TOTAL FY, -0.116486, Newton
TOTAL FZ, -8.53795, Newton
Center of Force about X-Axis (Y-Z), -8335.3, -11041, cm
Center of Force about Y-Axis (X-Z), 15274.7, -11039.5, cm
Center of Force about Z-Axis (X-Y), 15245.5, -8335.56, cm
```

b. Kecepatan 0,895 m/s

Summary

```
-----
Total area, 13186.3, cm^2
TOTAL FX, -1.80305, Newton
TOTAL FY, -0.072729, Newton
TOTAL FZ, -10.311, Newton
Center of Force about X-Axis (Y-Z), -8335.56, -11041, cm
Center of Force about Y-Axis (X-Z), 15236, -11041.4, cm
Center of Force about Z-Axis (X-Y), 15244.9, -8335.5, cm
```

c. Kecepatan 0,976 m/s

Summary

```
-----
Total area, 13186.3, cm^2
TOTAL FX, -2.0809, Newton
TOTAL FY, -0.0157407, Newton
TOTAL FZ, -12.3232, Newton
Center of Force about X-Axis (Y-Z), -8335.71, -11041, cm
Center of Force about Y-Axis (X-Z), 14866.1, -11044.7, cm
Center of Force about Z-Axis (X-Y), 15245.3, -8335.46, cm
```

d. Kecepatan 1,057 m/s

Summary

Total area, 13168.2, cm²
 TOTAL FX, -2.45336, Newton
 TOTAL FY, 0.0341124, Newton
 TOTAL FZ, -14.3794, Newton
 Center of Force about X-Axis (Y-Z), -8335.41, -11041.1, cm
 Center of Force about Y-Axis (X-Z), 15102, -11043.4, cm
 Center of Force about Z-Axis (X-Y), 15244.3, -8335.44, cm

e. Kecepatan 1,139 m/s

Summary

Total area, 13168.2, cm²
 TOTAL FX, -2.81138, Newton
 TOTAL FY, 0.0875541, Newton
 TOTAL FZ, -16.7129, Newton
 Center of Force about X-Axis (Y-Z), -8335.49, -11041.1, cm
 Center of Force about Y-Axis (X-Z), 15201.9, -11040.8, cm
 Center of Force about Z-Axis (X-Y), 15244.5, -8335.43, cm

f. Kecepatan 1,220 m/s

Summary

Total area, 13186.3, cm²
 TOTAL FX, -3.17713, Newton
 TOTAL FY, 0.0125398, Newton
 TOTAL FZ, -19.4284, Newton
 Center of Force about X-Axis (Y-Z), -8335.71, -11041, cm
 Center of Force about Y-Axis (X-Z), 16433.2, -11025.9, cm
 Center of Force about Z-Axis (X-Y), 15246.2, -8335.47, cm

g. Kecepatan 1,301 m/s

Summary

Total area, 13186.3, cm²
 TOTAL FX, -3.79748, Newton
 TOTAL FY, -0.236724, Newton
 TOTAL FZ, -22.0421, Newton
 Center of Force about X-Axis (Y-Z), -8335.42, -11041, cm
 Center of Force about Y-Axis (X-Z), 15265.2, -11040.8, cm
 Center of Force about Z-Axis (X-Y), 15245.5, -8335.56, cm

h. Kecepatan 1,383 m/s

Summary

```

-----
Total area, 13186.3, cm^2
TOTAL FX, -4.48367, Newton
TOTAL FY, -0.121817, Newton
TOTAL FZ, -24.0411, Newton
Center of Force about X-Axis (Y-Z), -8335.45, -11041, cm
Center of Force about Y-Axis (X-Z), 15258.5, -11039.8, cm
Center of Force about Z-Axis (X-Y), 15243.2, -8335.49, cm

```

i. Kecepatan 1,464 m/s

Summary

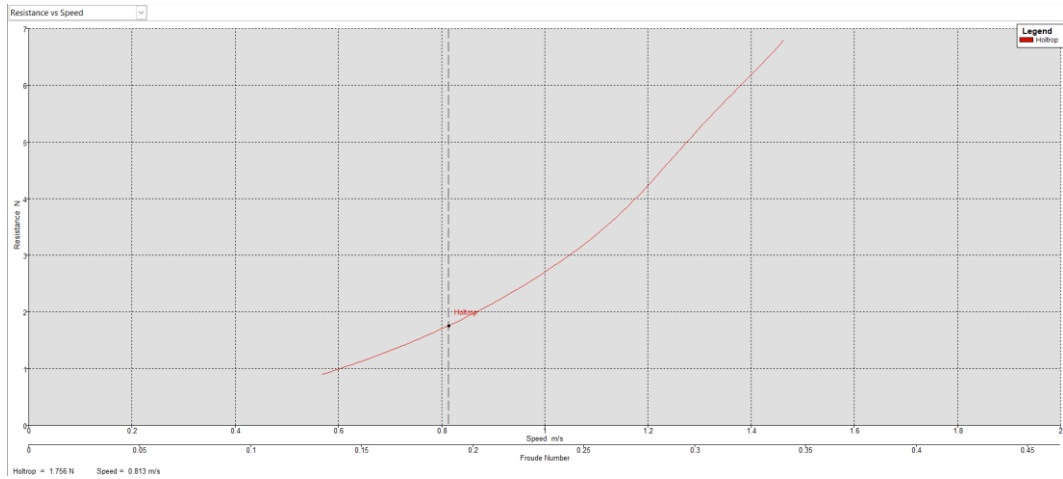
```

-----
Total area, 13186.3, cm^2
TOTAL FX, -5.24849, Newton
TOTAL FY, -0.270132, Newton
TOTAL FZ, -27.8918, Newton
Center of Force about X-Axis (Y-Z), -8335.37, -11041, cm
Center of Force about Y-Axis (X-Z), 15282.2, -11039.4, cm
Center of Force about Z-Axis (X-Y), 15242.7, -8335.51, cm

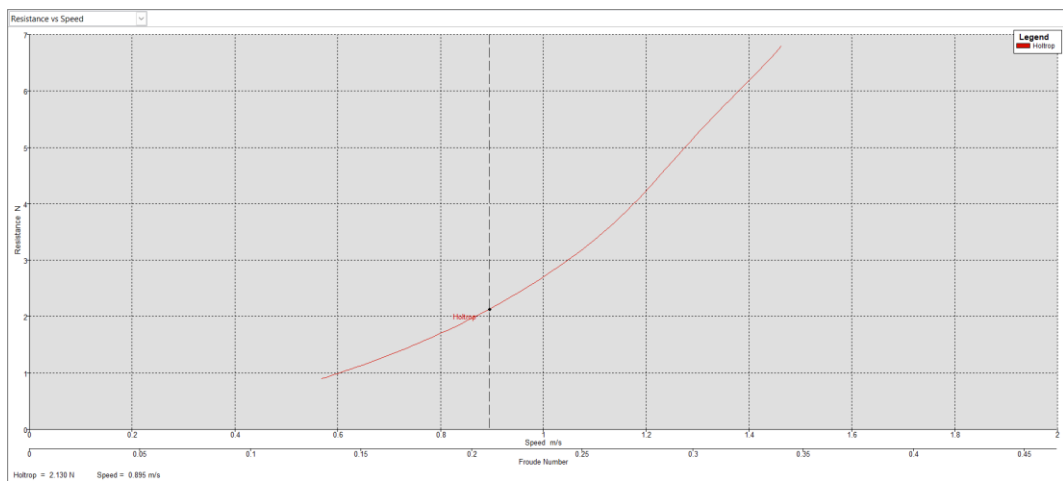
```

Lampiran 6 Hasil nilai perhitungan *wall calculator* tahanan model kapal di setiap variasi kecepatan menggunakan *software Maxsurf*.

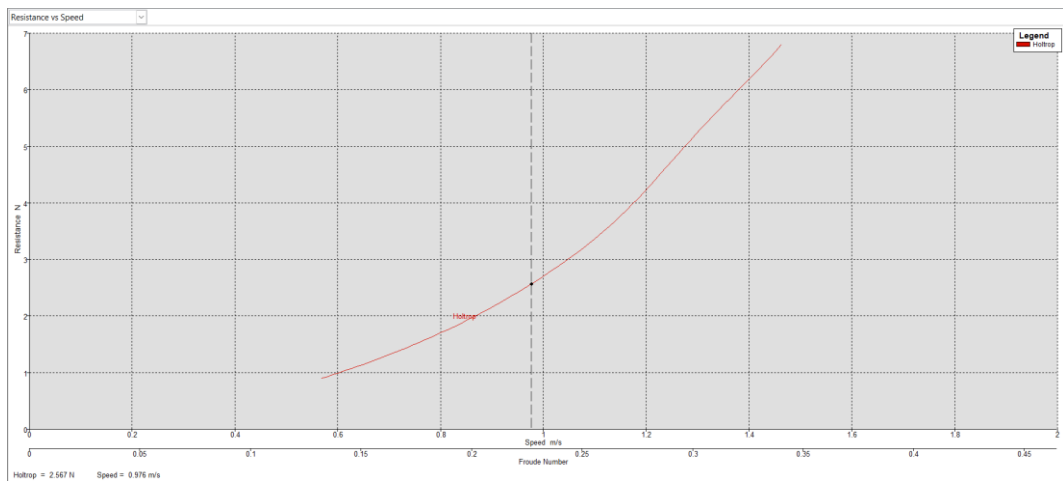
a. Kecepatan 0,813 m/s



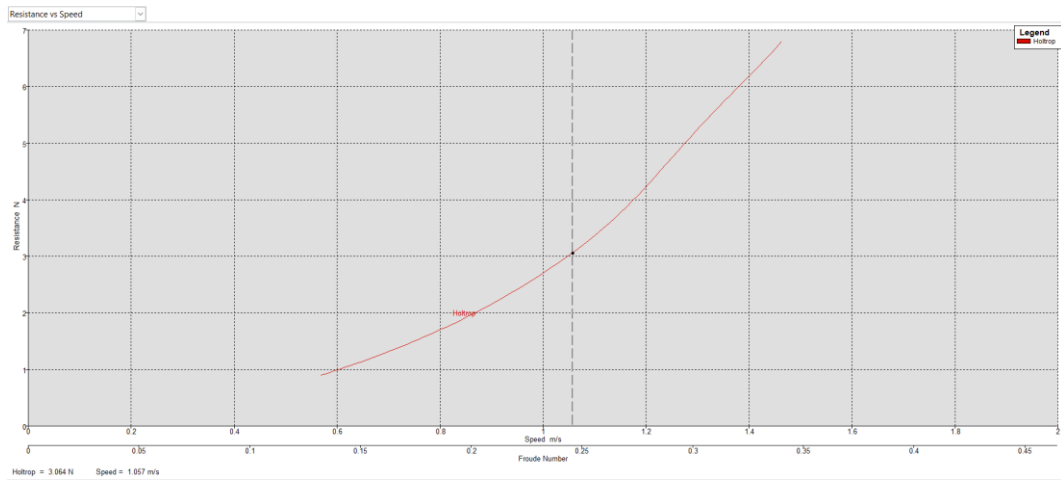
b. Kecepatan 0,895 m/s



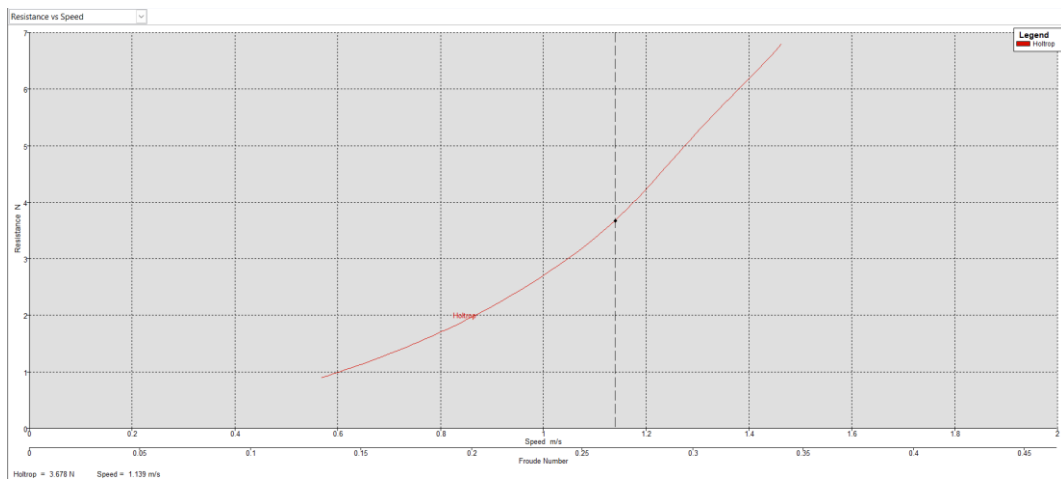
c. Kecepatan 0,976 m/s



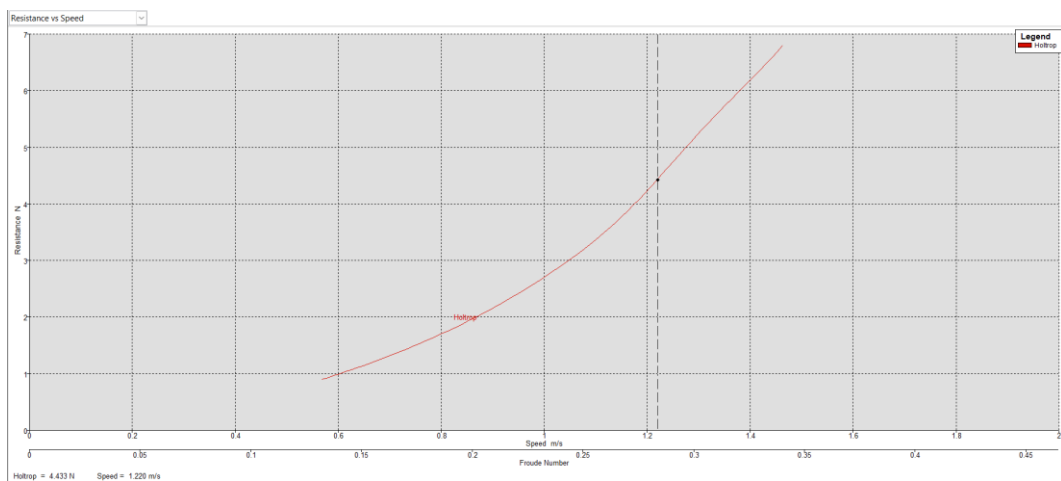
d. Kecepatan 1,057 m/s



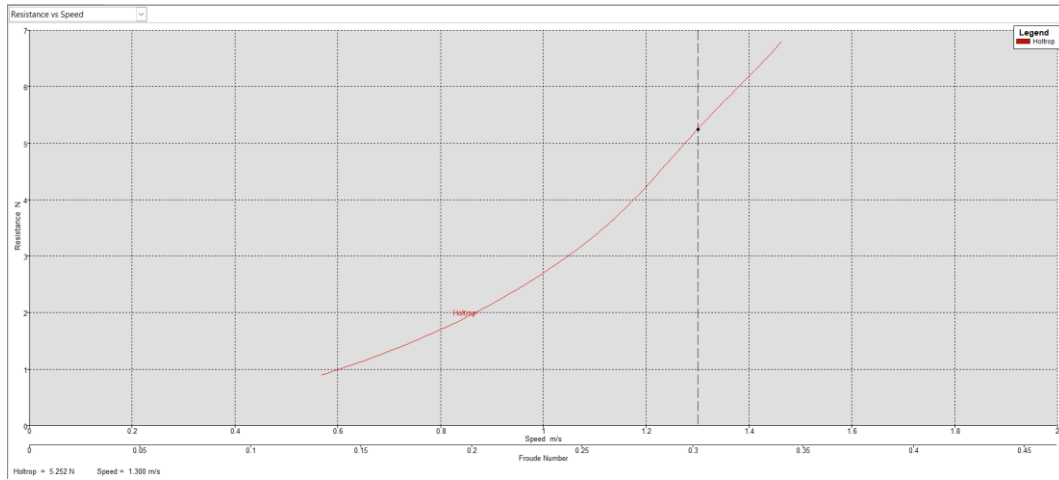
e. Kecepatan 1,139 m/s



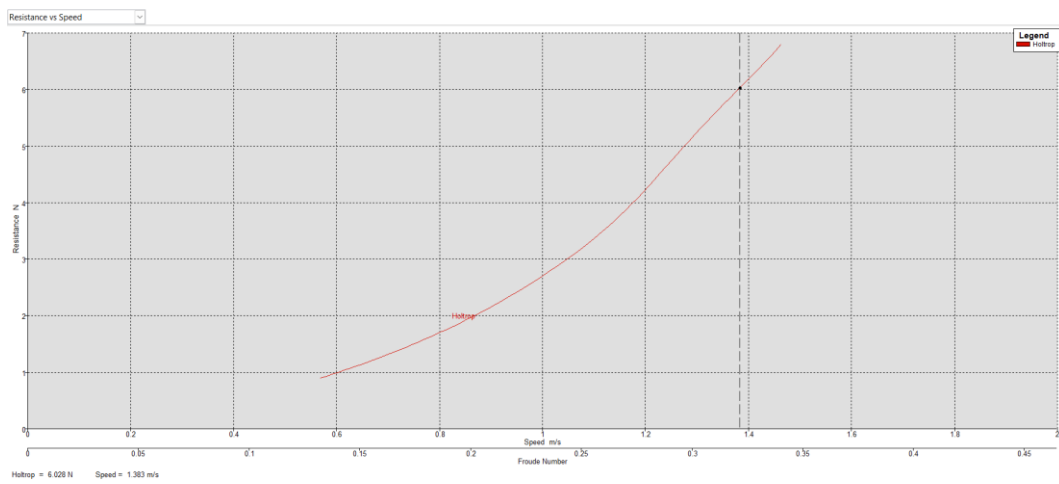
f. Kecepatan 1,220 m/s



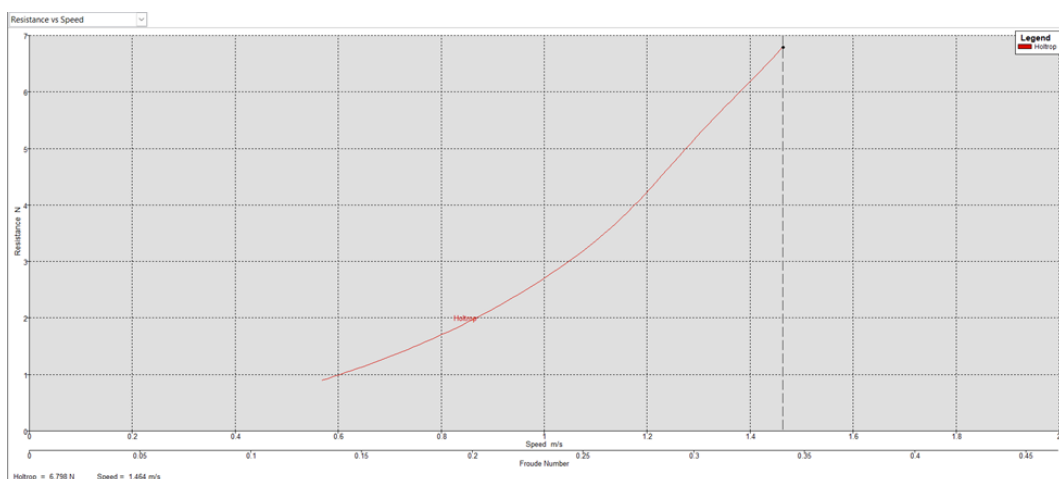
g. Kecepatan 1,300 m/s



h. Kecepatan 1,383 m/s



i. Kecepatan 1,464 m/s



Lampiran 7 Hasil nilai perhitungan *wall calculator* tahanan model kapal di setiap variasi kecepatan diubah menjadi tahanan kapal sesungguhnya

a. Kecepatan 10 knot

$$\begin{aligned}R_{TS} &= R_{TM} * \lambda^3 \\ &= 1,563 \times 40^3 \\ &= 1,563 \times 64000 \\ &= 100032 \text{ N} \\ &= 100,032 \text{ KN}\end{aligned}$$

b. Kecepatan 11 knot

$$\begin{aligned}R_{TS} &= R_{TM} * \lambda^3 \\ &= 1,803 \times 40^3 \\ &= 1,803 \times 64000 \\ &= 115392 \text{ N} \\ &= 115,392 \text{ KN}\end{aligned}$$

c. Kecepatan 12 knot

$$\begin{aligned}R_{TS} &= R_{TM} * \lambda^3 \\ &= 2,081 \times 40^3 \\ &= 2,081 \times 64000 \\ &= 133184 \text{ N} \\ &= 133,184 \text{ KN}\end{aligned}$$

d. Kecepatan 13 knot

$$\begin{aligned}R_{TS} &= R_{TM} * \lambda^3 \\ &= 2,453 \times 40^3 \\ &= 2,453 \times 64000 \\ &= 156992 \text{ N}\end{aligned}$$

$$= 156,992 \text{ KN}$$

e. Kecepatan 14 knot

$$R_{TS} = R_{TM} * \lambda^3$$

$$= 2,811 \times 40^3$$

$$= 2,811 \times 64000$$

$$= 179904 \text{ N}$$

$$= 179,904 \text{ KN}$$

f. Kecepatan 15 knot

$$R_{TS} = R_{TM} * \lambda^3$$

$$= 3,177 \times 40^3$$

$$= 3,713 \times 64000$$

$$= 203328 \text{ N}$$

$$= 203,328 \text{ KN}$$

g. Kecepatan 16 knot

$$R_{TS} = R_{TM} * \lambda^3$$

$$= 3,797 \times 40^3$$

$$= 3,797 \times 64000$$

$$= 243008 \text{ N}$$

$$= 243,008 \text{ KN}$$

h. Kecepatan 17 knot

$$R_{TS} = R_{TM} * \lambda^3$$

$$= 4,484 \times 40^3$$

$$= 4,484 \times 64000$$

$$= 286976 \text{ N}$$

$$= 286,976 \text{ KN}$$

i. Kecepatan 18 knot

$$R_{TS} = R_{TM} * \lambda^3$$

$$= 5,248 \times 40^3$$

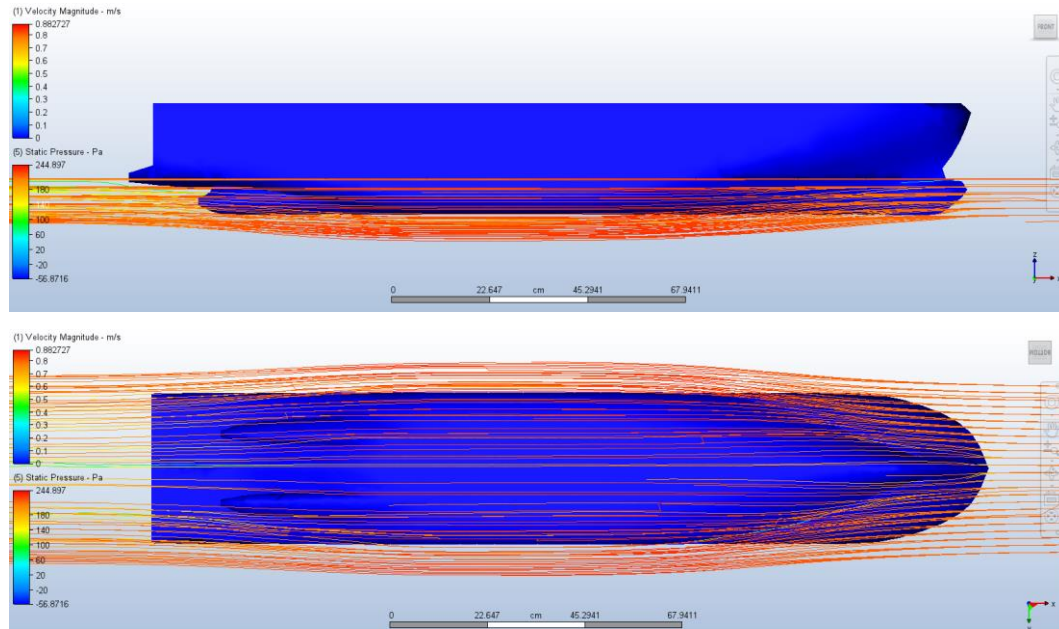
$$= 5,248 \times 64000$$

$$= 335872 \text{ N}$$

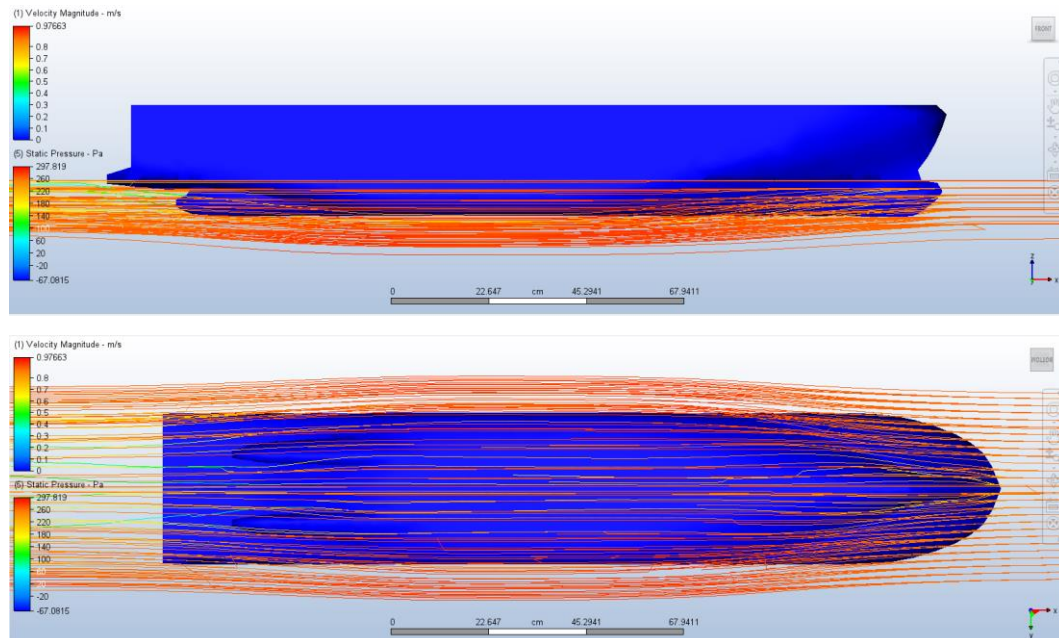
$$= 335,872 \text{ KN}$$

Lampiran 8 Visualisasi pola aliran fluida pada setiap variasi kecepatan menggunakan *software* CFD (*Computational Fluid Dynamic*)

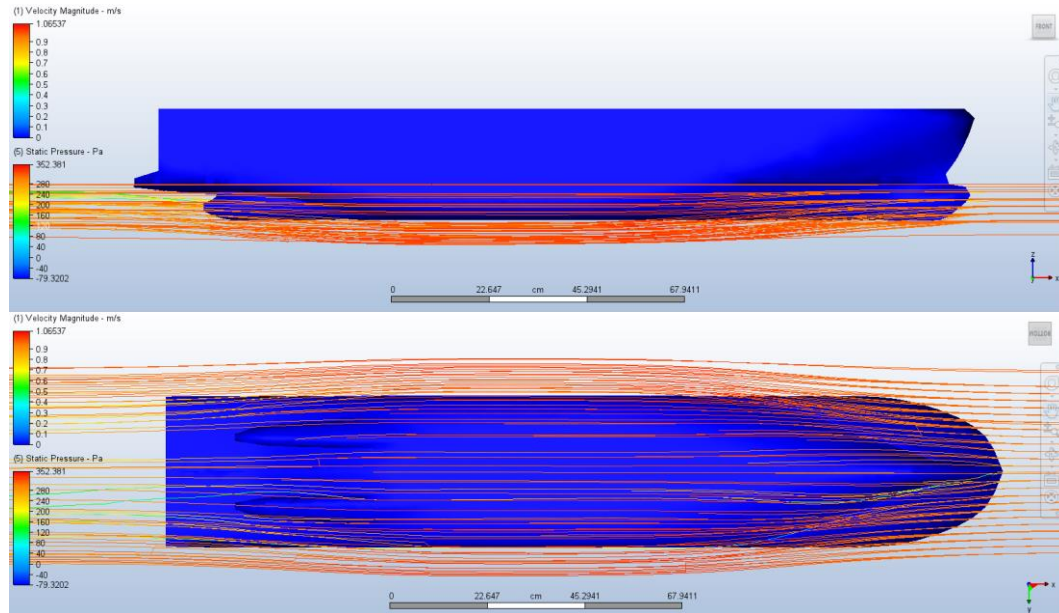
a. Kecepatan 0,813 m/s



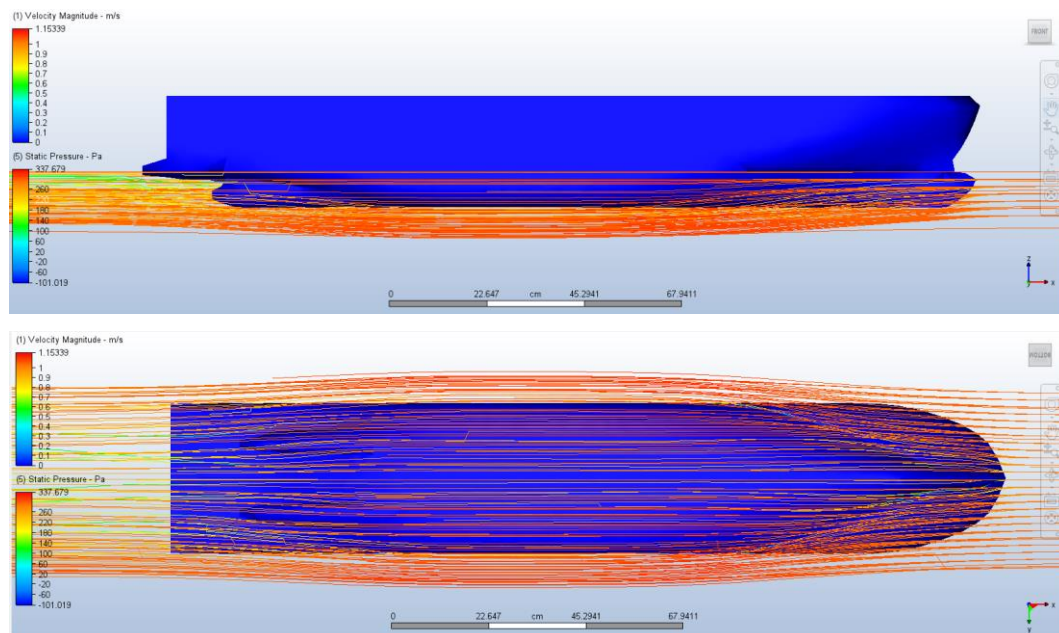
b. Kecepatan 0,895 m/s



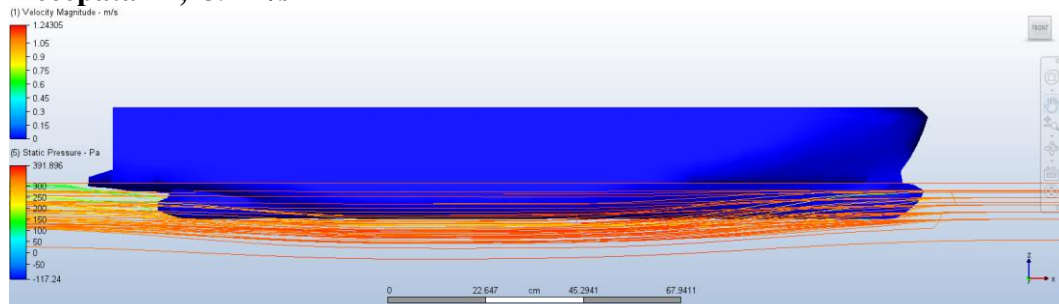
c. Kecepatan 0,976 m/s

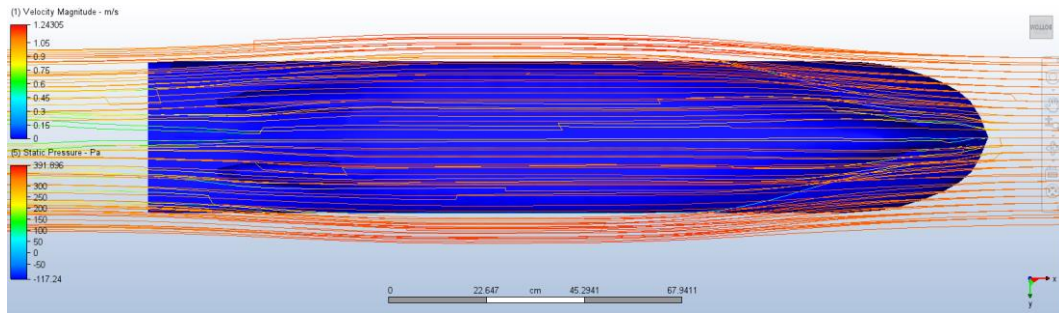


d. Kecepatan 1,057 m/s

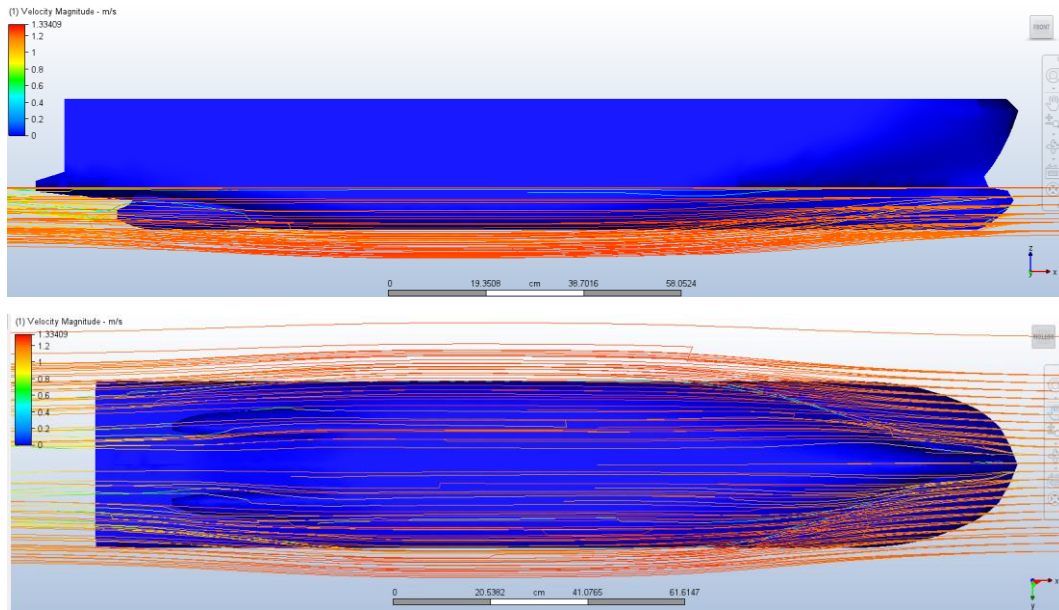


e. Kecepatan 1,139 m/s

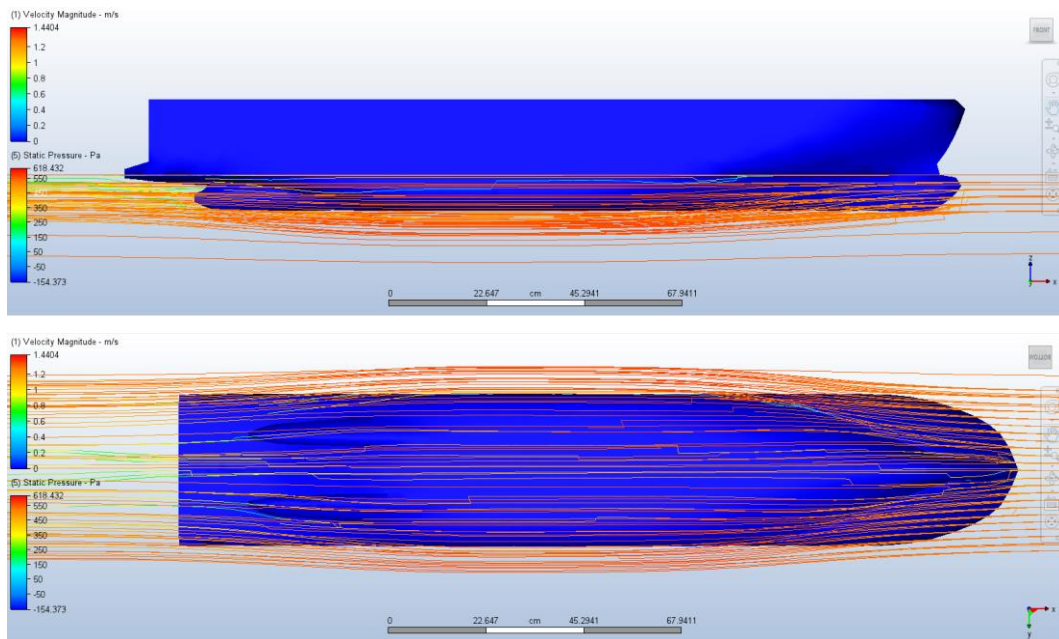




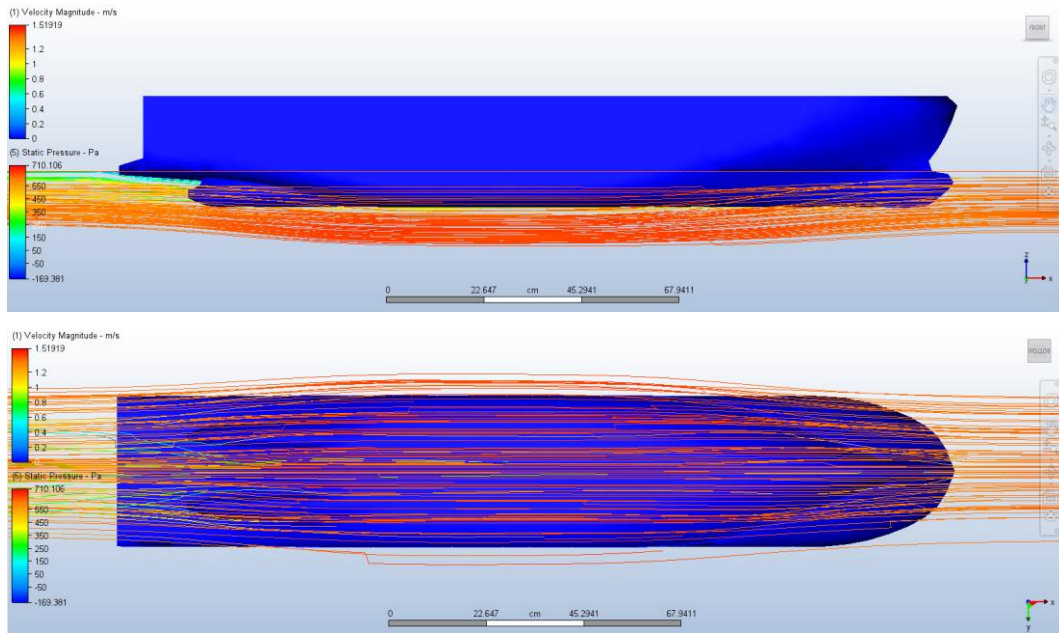
f. Kecepatan 1,220 m/s



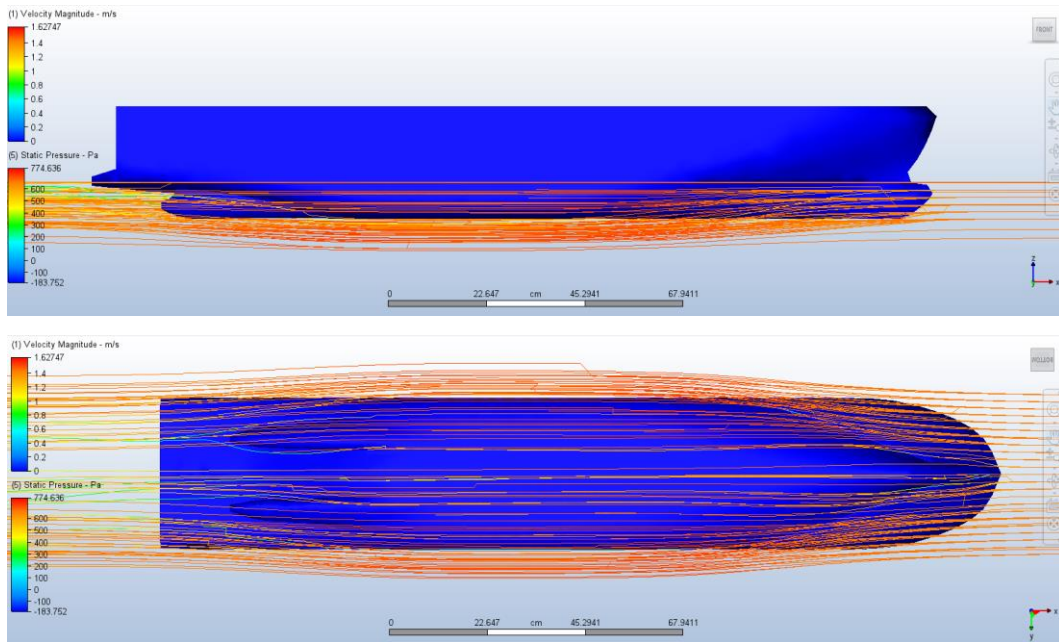
g. Kecepatan 1,301 m/s



h. Kecepatan 1,383 m/s



i. Kecepatan 1,464 m/s



Lampiran 9 Data Ukuran Utama Kapal ferry Roro Lintas Lembar Padang-Bai

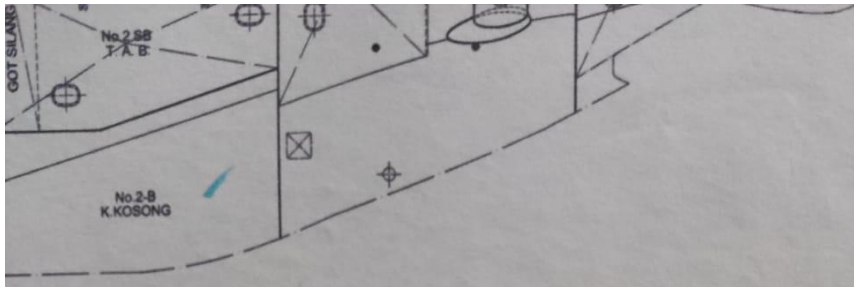


Diagram showing deck layout with labels: No. 2.8B Y-A-B, No. 2-8 K.KOSONG, and GUY SILANG.

VCG dari BL (m)	FSM (Lm)
453	4.106
453	4.106
263	18.662
964	26.874

BIRO KLASIFIKASI INDONESIA

SEEN
DIKETAHUI

Number Nomor **2001150011**

JAKARTA, 03 JUN 2021

UKURAN UTAMA :

PANJANG SELURUHNYA (Loa) =	77.72 m
PANJANG A.G.T. (Lpp) =	72.60 m
LEBAR (B) =	14.00 m
TINGGI (H) =	4.60 m
SARAT (T) =	3.30 m
SARAT KONSTRUKSI (T _k) =	3.30 m
KECEPATAN PERCOBAAN (v _t) =	16.00 Knot
KECEPATAN DINAS (v _d) =	15.00 Knot
MESIN INDUK =	2 x 1350 kW minimum RPM Max 1100, dry circulation

KLAS : + A 100 I (P) KAPAL PENYEBERANGAN G.L.D. TERTUTUP
(RO RO PASSENGER FERRY CLOSED DECK TYPE)
+ SM

VCG dari BL (m)	FSM (Lm)
0.441	1.073
0.441	1.073
0.441	3.146
0.441	3.146
0.441	8.438

VCG dari BL (m)	FSM (Lm)
0.465	6.385
0.465	6.385
0.465	12.770

R.02				
R.01				
REVISI	KETERANGAN	OLSH	TAMBAH	

PT. ASDP INDONESIA FERRY (PERSERO)

**KAPAL PENYEBERANGAN
LINTAS LEMBAR - PADANG BAI**

RENCANA KAPASITAS TANGKI


Director
J. Ahmad Adhwal Yan
Kor 01 A
Jakarta 10560
Telpom 021-5900546
Fax 021-5900145
Email

www.asdp.co.id

PEMBANGUN IKI SHIPYARD <small>PT. INDUSTRI KAPAL INDONESIA (Persero)</small> <small>www.ikihipyard.co.id email: pib@ikihipyard.co.id</small>	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td>SKALA</td> <td>1 : 100</td> <td>LEMBAR</td> <td>1/1</td> </tr> <tr> <td>UKURAN</td> <td>A1</td> <td>REVISI</td> <td>00</td> </tr> <tr> <td>NO. GAMBAR PEMILIK</td> <td colspan="3">R98-0820111</td> </tr> <tr> <td>KELAS & No. KONTRAK</td> <td colspan="3">BNI-2001150011</td> </tr> <tr> <td>PELETAKAN LUNAS</td> <td colspan="3">30 SEPTEMBER 2020</td> </tr> </table>	SKALA	1 : 100	LEMBAR	1/1	UKURAN	A1	REVISI	00	NO. GAMBAR PEMILIK	R98-0820111			KELAS & No. KONTRAK	BNI-2001150011			PELETAKAN LUNAS	30 SEPTEMBER 2020		
SKALA	1 : 100	LEMBAR	1/1																		
UKURAN	A1	REVISI	00																		
NO. GAMBAR PEMILIK	R98-0820111																				
KELAS & No. KONTRAK	BNI-2001150011																				
PELETAKAN LUNAS	30 SEPTEMBER 2020																				

www.ikihipyard.co.id

<small>PEMERINTAH RI KEMENTERIAN PERKAPALAN DAN PERBURUHAN DIREKTORAT JENDERAL PERKAPALAN DAN PERBURUHAN DIREKTORAT PERENCANAAN DAN KONTROL KAPAL</small>	<p>NAMA PROYEK : PEMBANGUNAN 1 (SATU) LAYAR KAPAL PENYEBERANGAN DI LINTAS LEMBAR PADANG BAI</p>
---	--

<p>NO. LAMBUANG : 18B 186</p> <p>NO. GAMBAR : B-12-093</p>	<p>PENGAWAS : PT BKI BBU MARINE & OFFSHORE MIGAS</p> <p>PERENCANA : R98a.iki@gmail.com </p>
--	--

Sumber: PT. Industri Kapal Indonesia

Lampiran 10 Data hasil perhitungan nilai tahanan kapal yang dilakukan Laboratorium Hidrodinamika Indonesia (LHI)



Tabel 8. Hasil ekstrapolasi hambatan kapal sarat 3.30 m

RESULTS OF RESISTANCE EXTRAPOLATION

RESISTANCE TEST KAPAL FERRY RORO 1500 GT DRAUGHT FWD 3.30 m
SHIP MODEL NO. LHI-0258 DRAUGHT AFT 3.30 m

VS	VM	RM	CTM	CFM	CRES	CFS	CTS	FD	RS	PE	CE
KNOTS	M/S	N	5	5	5	5	5	N	KN	KW	
			*10	*10	*10	*10	*10				
10	1.23	14.88	492	326	56	169	339	4.63	57	292	430
11	1.35	18.19	497	320	68	167	349	5.43	71	400	418
12	1.47	21.84	501	315	79	165	357	6.29	86	532	408
13	1.60	26.19	512	311	96	163	372	7.19	105	704	392
14	1.72	32.42	547	307	136	162	410	8.14	135	969	356
15	1.84	41.34	607	303	201	160	473	9.14	178	1377	308
16	1.97	51.16	661	300	259	159	529	10.18	227	1869	275
17	2.09	60.06	687	296	290	158	558	11.27	270	2364	261
18	2.210	68.33	697	294	304	157	571	12.40	310	2869	255

NOTES: - FOR EXPLANATION OF ABBREVIATIONS SEE LIST OF SYMBOLS
 - THE RESULTS ABOVE WERE OBTAINED BY MEANS OF THE ITTC-1957 FORMULA
 WITH A FORM FACTOR OF $1+K=1.340$
 AND A MODEL-SHIP CORRELATION ALLOWANCE OF $CA=.00057$
 FOR A WETTED AREA OF $S=4.012\text{ M}^2$ (SHIP VALUE= 1235.7 M^2)
 AND A LENGTH ON THE WATERLINE $LWL=4.365\text{ M}$
 (SHIP $L=76.60\text{ M}$)
 FOR A TANK WATER TEMPERATURE OF 27.3 DEGREES C
 $\frac{2}{3} \quad 3$
 - $CE=0.7477 \cdot DISV \cdot VS / PE$ IN UNITS AS ABOVE AND $DISV=2179.2\text{ M}^3$
 - THE RESULTS ARE FOR TRIAL CONDITIONS, IMPLYING UNRESTRICTED DEEP WATER OF 30 DEGREES C . AND A MASS DENSITY OF 1025.0 KG/M^3 , A CLEAN HULL

Sumber: Laboratorium Hidrodinamika Indonesia