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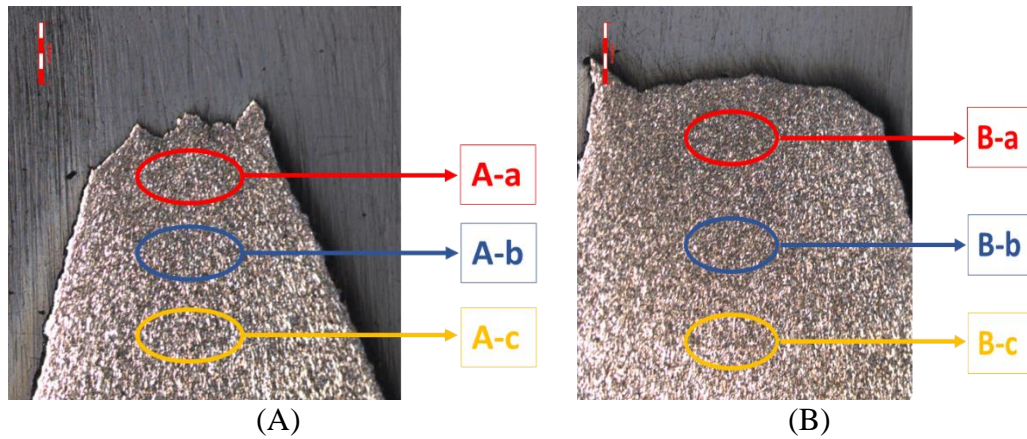
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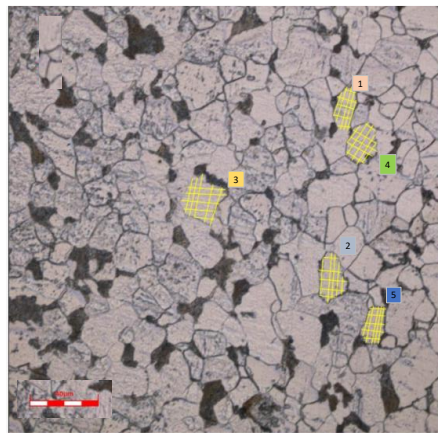
LAMPIRAN

Lampiran A Titik Lokasi Pengamatan Struktur Mikro dan Pengukuran Grain Rasio

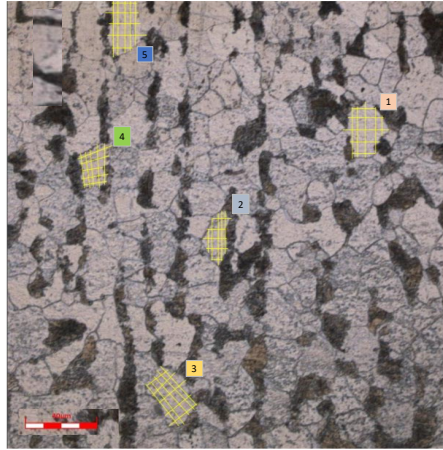
Lampiran A.1 Titik Lokasi Pengamatan Struktur Mikro dan Pengukuran Grain Rasio spesimen raw



Bentuk patahan dan titik pengamatan struktur mikro pada spesimen setelah mengalami creep rupture, (A) merupakan bagian tebal axial, (B) bagian sisi diameter luar dari superheater tube



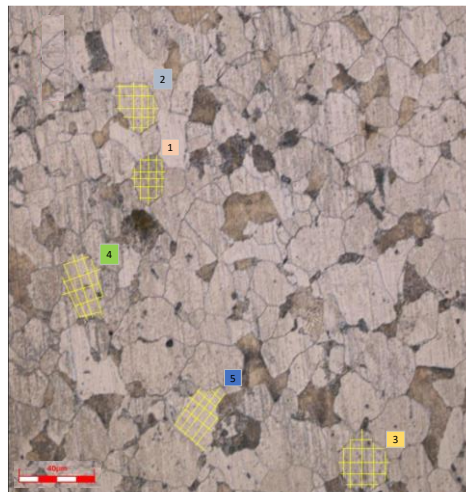
Titik lokasi pengamatan mikro struktur material raw bagian A-atas



Titik lokasi pengamatan mikro struktur material raw bagian A-tengah



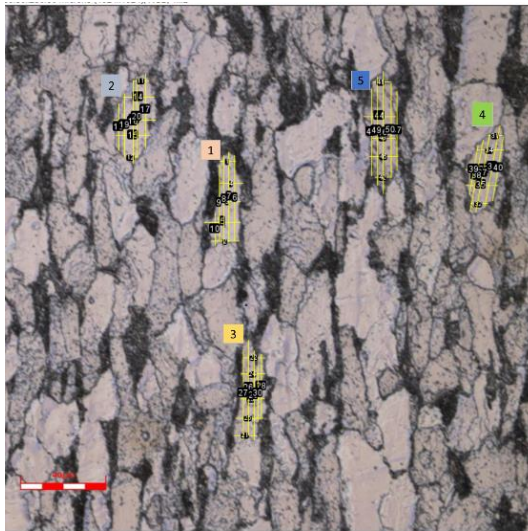
Titik lokasi pengamatan mikro struktur material raw bagian A-bawah



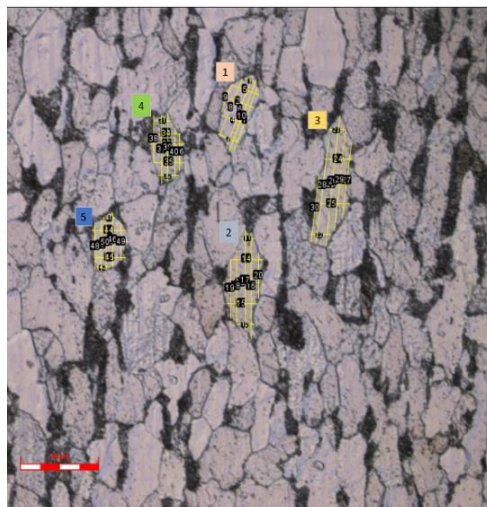
Titik lokasi pengamatan mikro struktur material raw bagian B



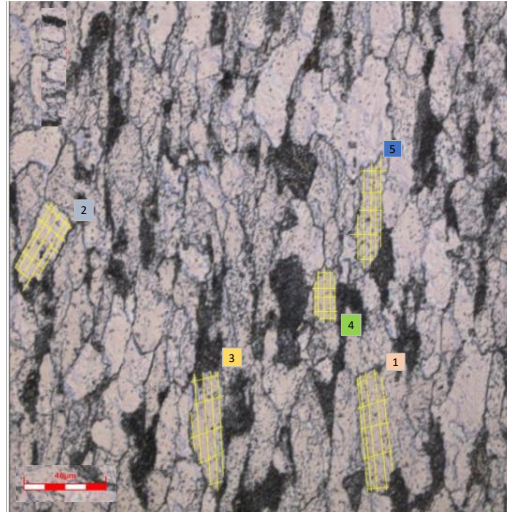
Struktur mikro material raw bagian A-a setelah mengalami creep



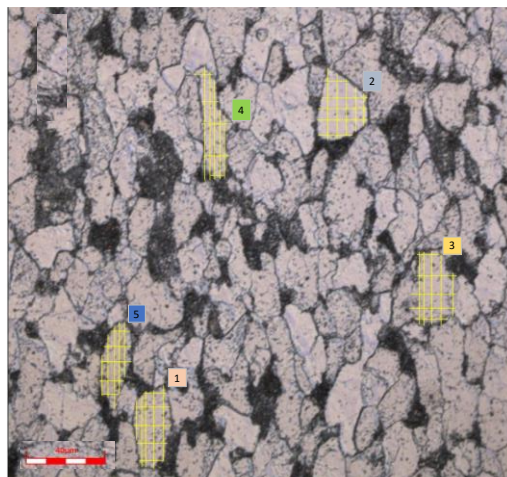
Struktur mikro material raw bagian A-b setelah mengalami creep



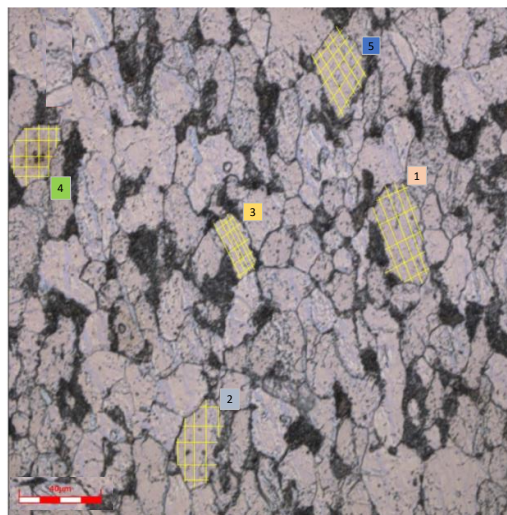
Struktur mikro material raw bagian A-c setelah mengalami creep



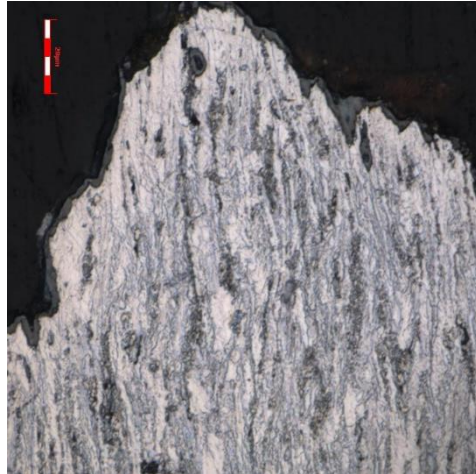
Struktur mikro material raw bagian B-a setelah mengalami *creep*



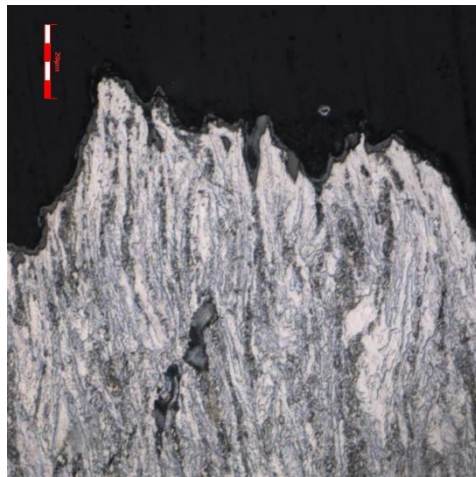
Struktur mikro material raw bagian B-b setelah mengalami *creep*



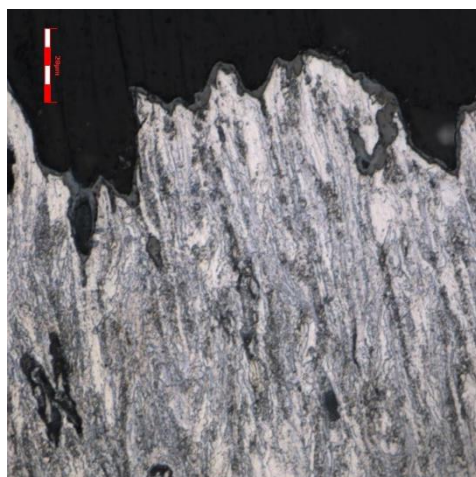
Struktur mikro material raw bagian B-c setelah mengalami *creep*



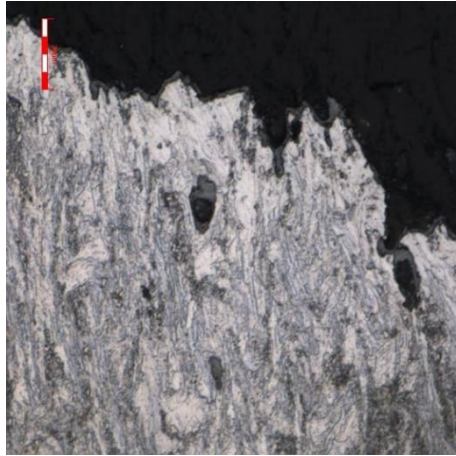
Struktur mikro jenis patahan yang terjadi pada material raw setelah pengujian tensile bagian A-1



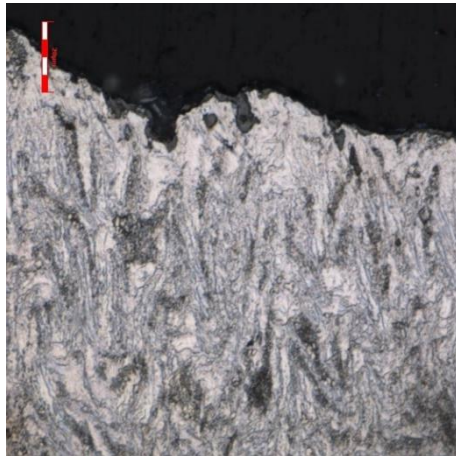
Struktur mikro jenis patahan yang terjadi bagian A-2 material raw setelah pengujian tensile



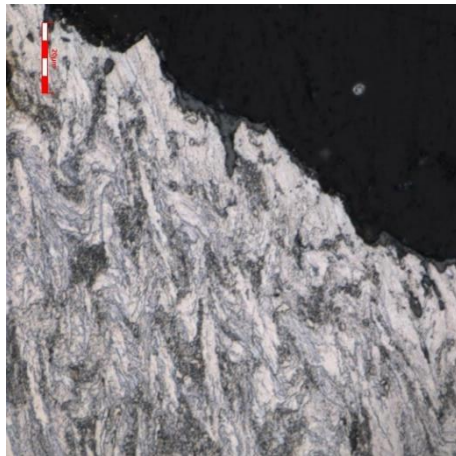
Struktur mikro jenis patahan yang terjadi bagian A-3 material raw setelah pengujian tensile



Struktur mikro jenis patahan yang terjadi bagian B-1 material raw setelah pengujian tensile

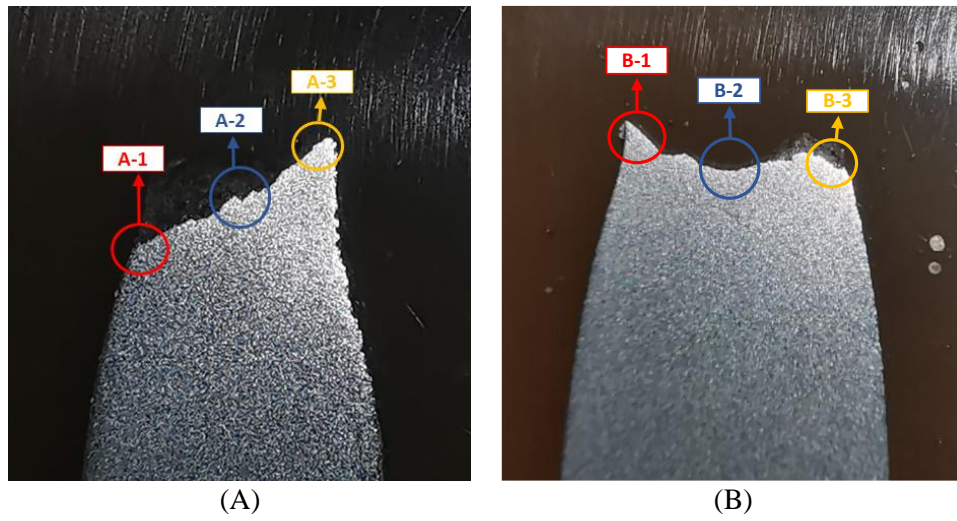


Struktur mikro jenis patahan yang terjadi bagian B-2 material raw setelah pengujian tensile

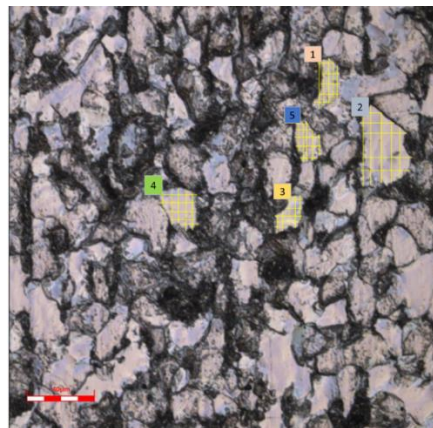


Struktur mikro jenis patahan yang terjadi bagian B-3 material raw setelah setelah pengujian tensile

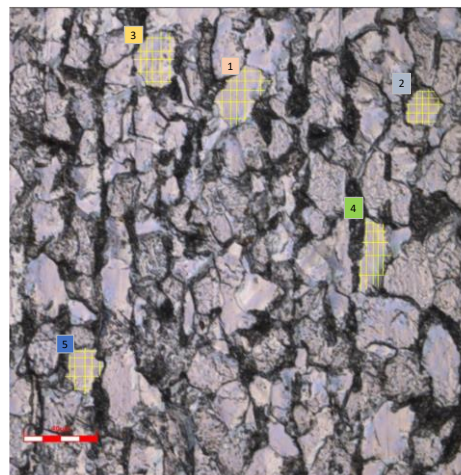
Lampiran A.2 Titik Lokasi Pengamatan Struktur Mikro dan Pengukuran Grain Rasio Spesimen 4 mm



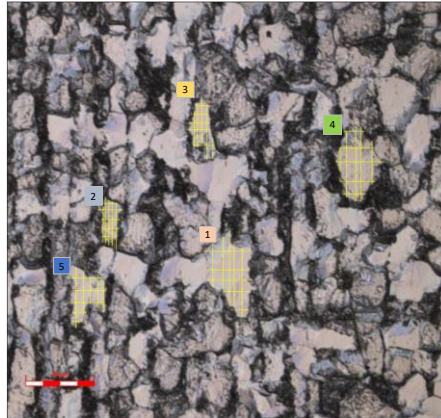
Bentuk patahan dan titik pengamatan struktur mikro pada spesimen 4 mm, (A) merupakan bagian tebal axial, (B) bagian sisi diameter luar dari *superheater* tube



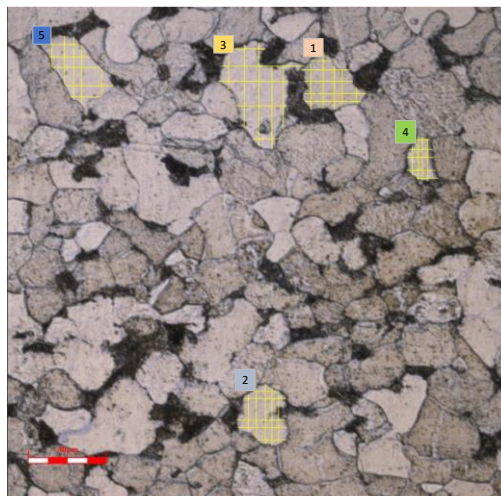
Struktur mikro spesimen 1 bagian A-atas setelah mengalami *creep displacement* 4mm



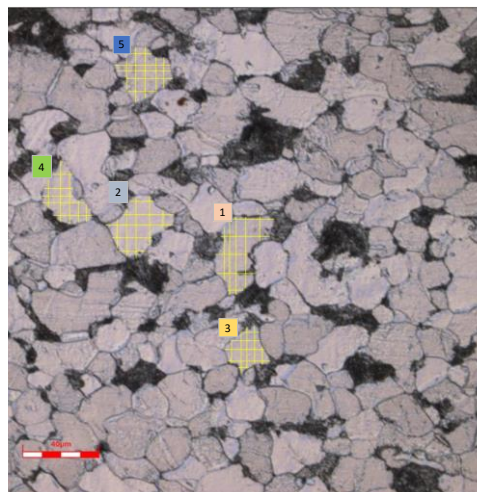
Struktur mikro spesimen 1 bagian A-tengah setelah mengalami *creep displacement* 4mm



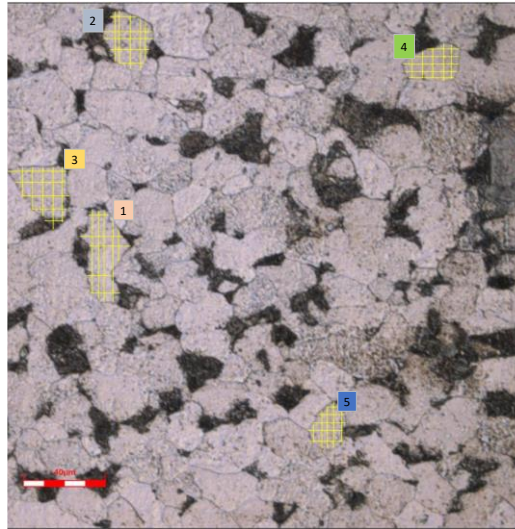
Struktur mikro spesimen 1 bagian A-bawah setelah mengalami *creep displacement* 4mm



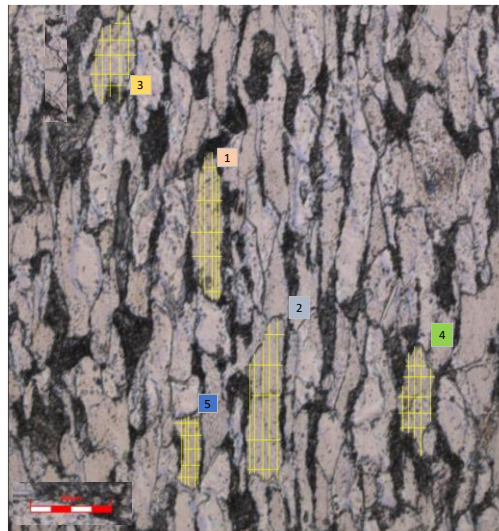
Struktur mikro spesimen 1 bagian B1 setelah mengalami *creep displacement* 4mm



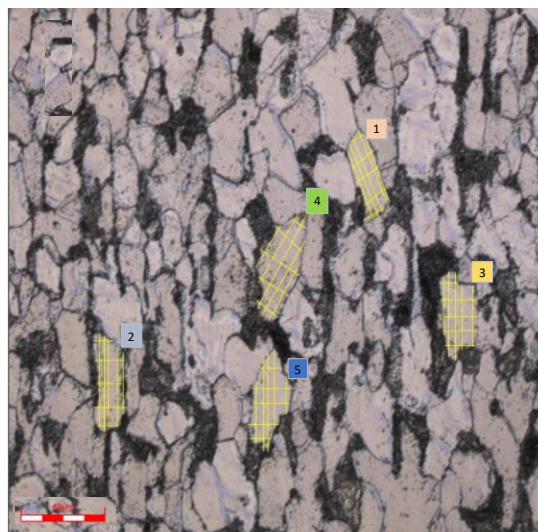
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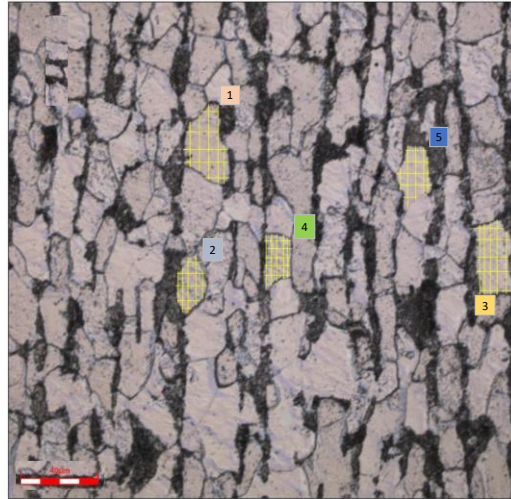
Struktur mikro spesimen 1 bagian B3 setelah mengalami *creep displacement* 4mm



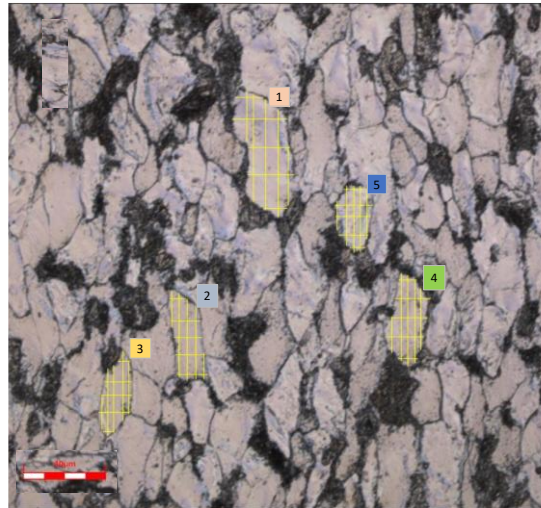
Struktur mikro spesimen 1 bagian A-a setelah setelah pengujian tensile



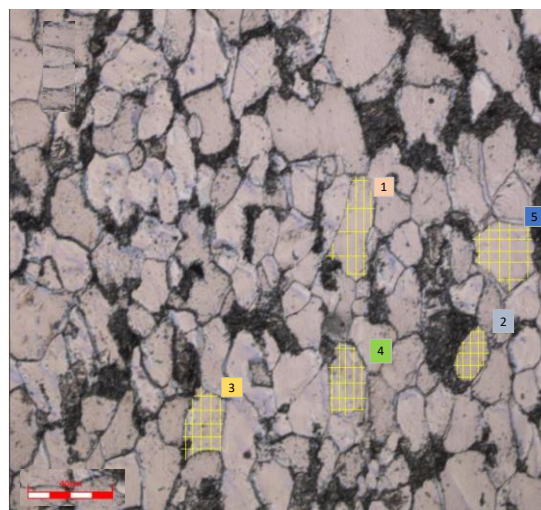
Struktur mikro spesimen 1 bagian A-b setelah pengujian tensile



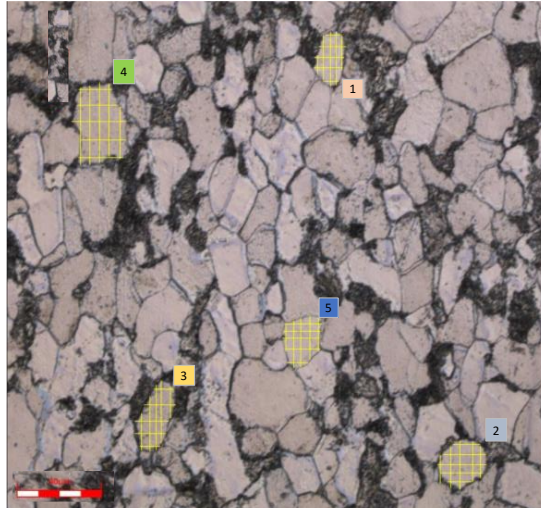
Struktur mikro spesimen 1 bagian A-c setelah setelah pengujian tensile



Struktur mikro spesimen 1 bagian B-a setelah setelah pengujian tensile



Struktur mikro spesimen 1 bagian B-b setelah pengujian tensile



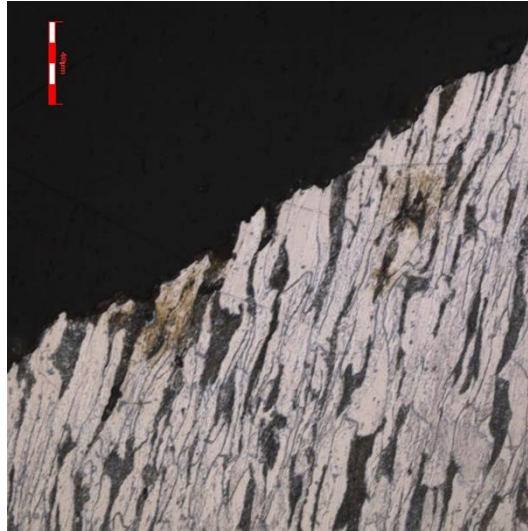
Struktur mikro spesimen 1 bagian B-c setelah setelah pengujian tensile



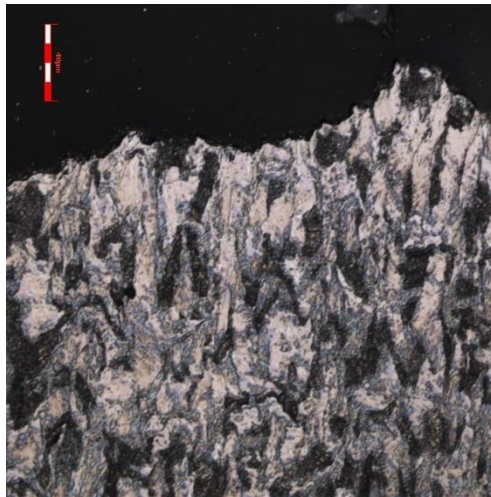
Struktur mikro spesimen 4 mm bagian A-1 setelah setelah pengujian tensile



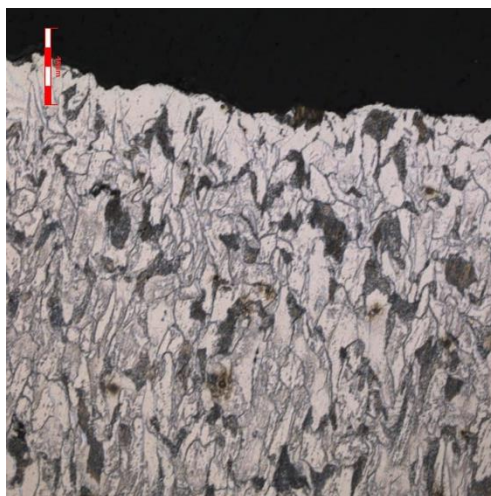
Struktur mikro spesimen 4 mm bagian A-2 setelah pengujian tensile



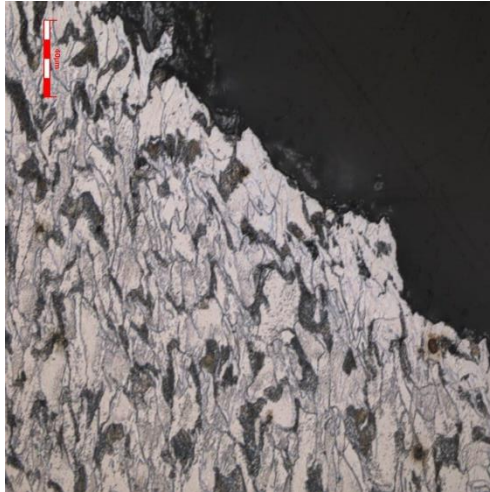
Struktur mikro spesimen 4 mm bagian A-3 setelah setelah pengujian tensile



Struktur mikro bentuk patahan spesimen 4 mm bagian B-1 setelah setelah pengujian tensile

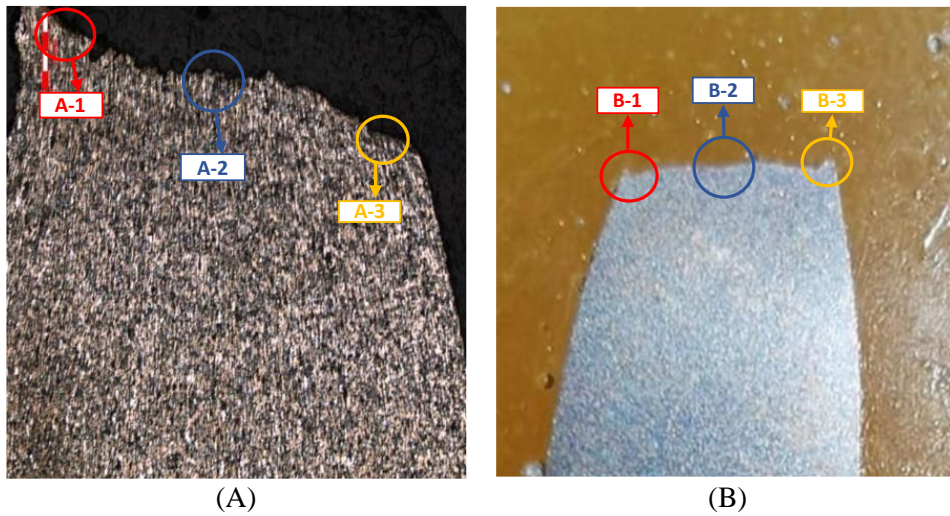


Struktur mikro bentuk patahan spesimen 4 mm bagian B-2 setelah pengujian tensile

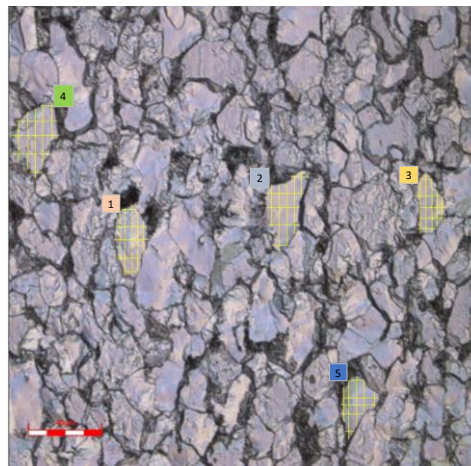


Struktur mikro bentuk patahan spesimen 4 mm bagian B-3 setelah setelah pengujian tensile

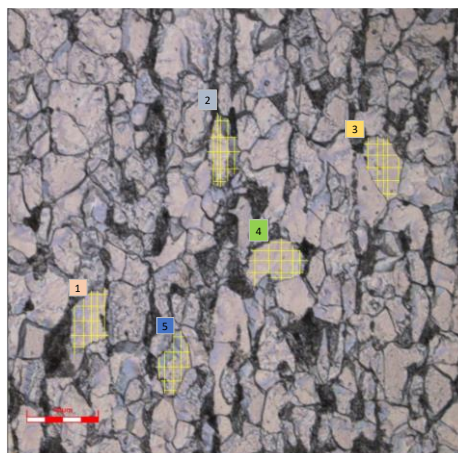
Lampiran A.3 Titik Lokasi Pengamatan Struktur Mikro dan Pengukuran Grain Rasio Spesimen 6 mm



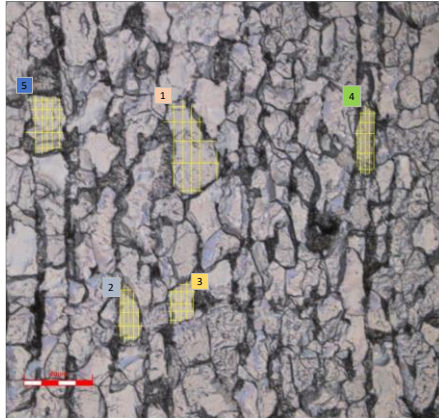
Bentuk patahan dan titik pengamatan struktur mikro pada spesimen 6 mm, (A) merupakan bagian tebal axial, (B) bagian sisi diameter luar dari *superheater* tube



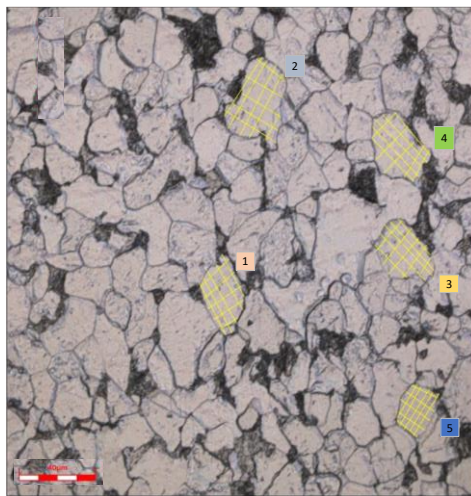
Struktur mikro spesimen 6 mm bagian A-atas setelah mengalami *creep*



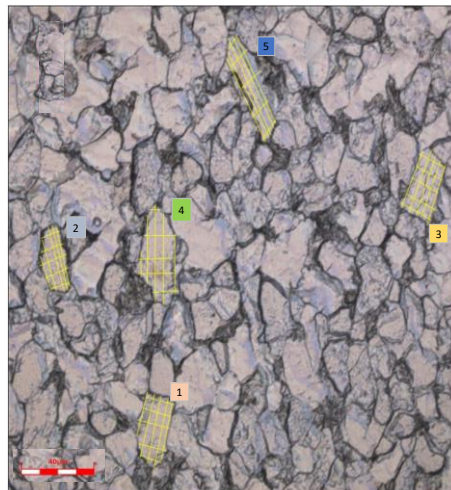
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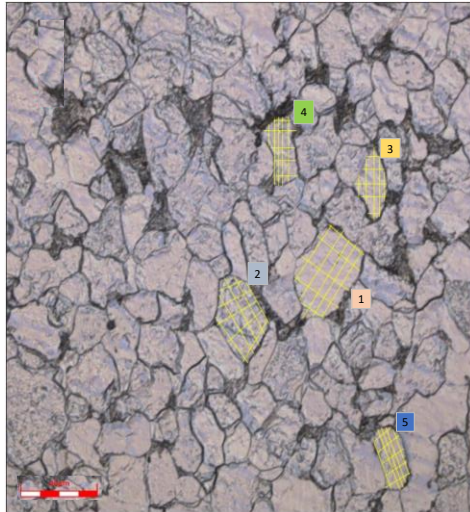
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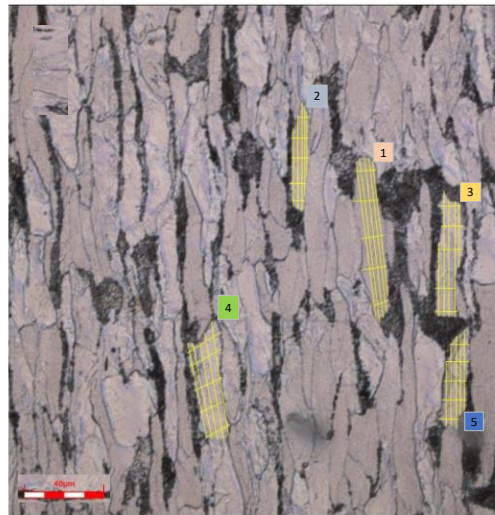
Struktur mikro spesimen 6 mm bagian B1 setelah mengalami



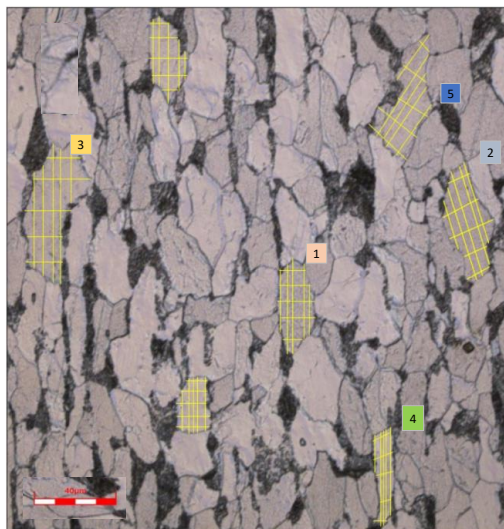
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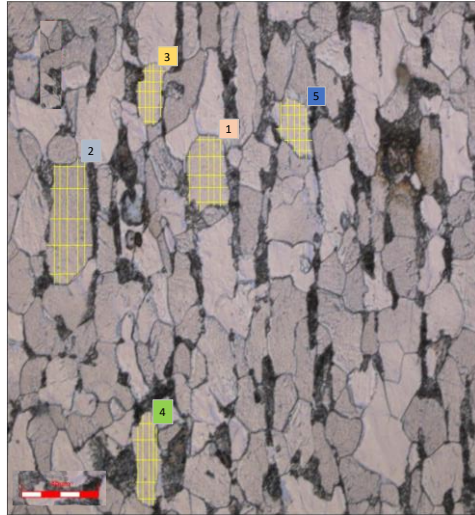
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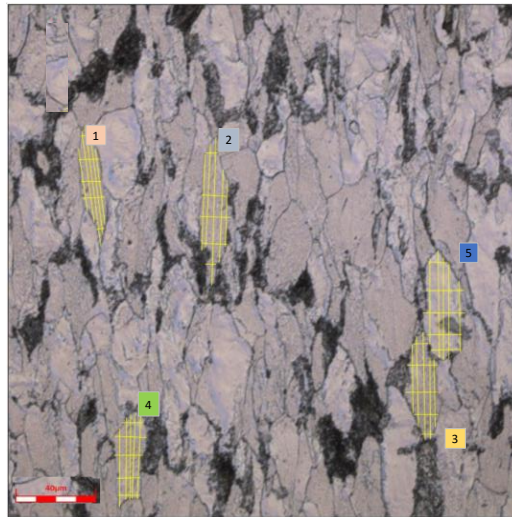
Struktur mikro spesimen 6 mm bagian A-a setelah setelah pengujian tensile



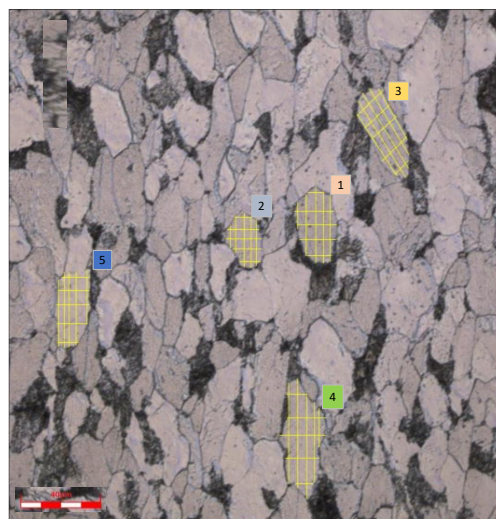
Struktur mikro spesimen 6 mm bagian A-b setelah pengujian tensile



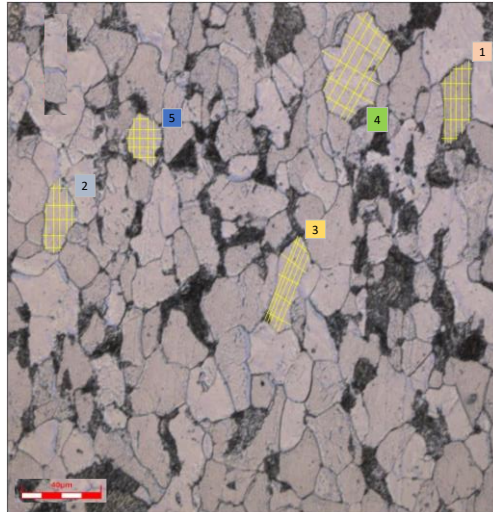
Struktur mikro spesimen 6 mm bagian A-c setelah setelah pengujian tensile



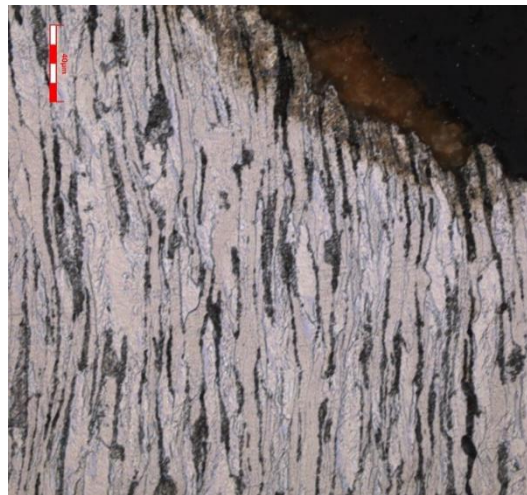
Struktur mikro spesimen 6 mm bagian B-a setelah setelah pengujian tensile



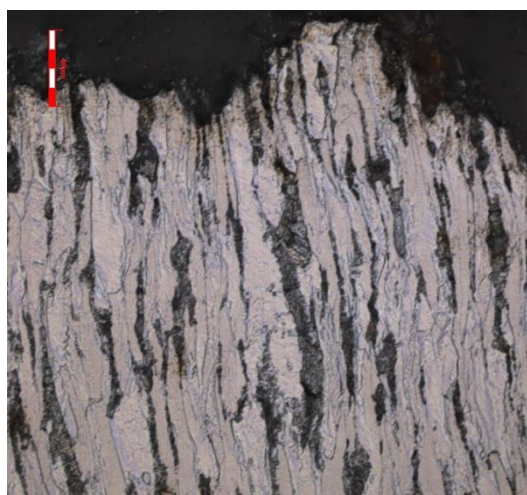
Struktur mikro spesimen 6 mm bagian B-b setelah pengujian tensile



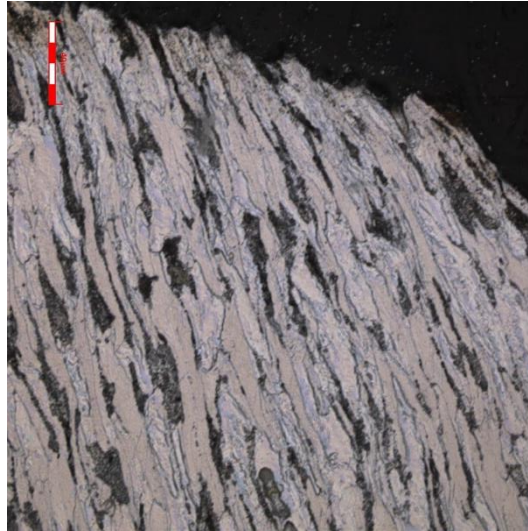
Struktur mikro spesimen 6 mm bagian B-c setelah setelah pengujian tensile



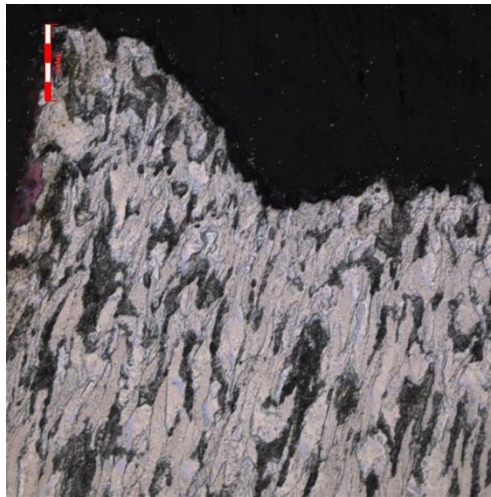
Struktur mikro spesimen 6 mm bagian A-1 setelah setelah pengujian tensile



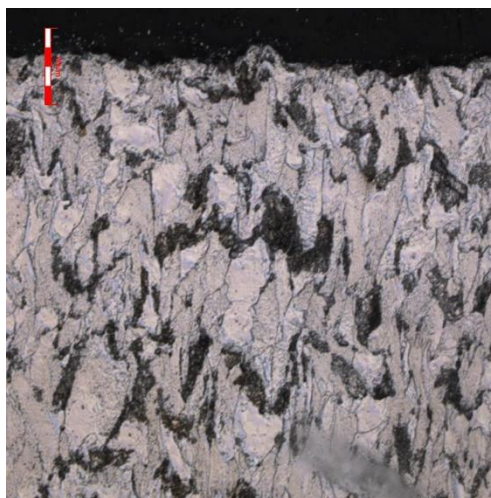
Struktur mikro spesimen 6 mm bagian A-2 setelah pengujian tensile



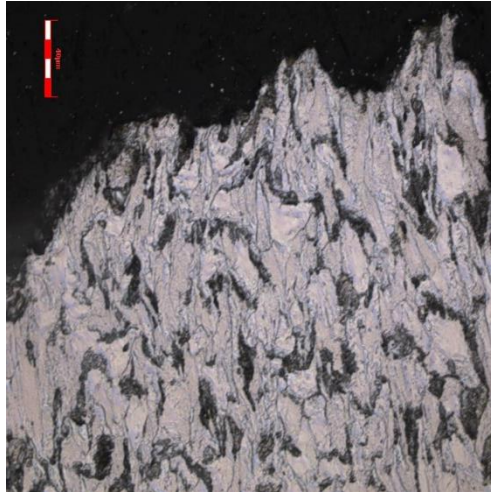
Struktur mikro spesimen 6 mm bagian A-3 setelah setelah pengujian tensile



Struktur mikro bentuk patahan spesimen 6 mm bagian B-1 setelah setelah pengujian tensile

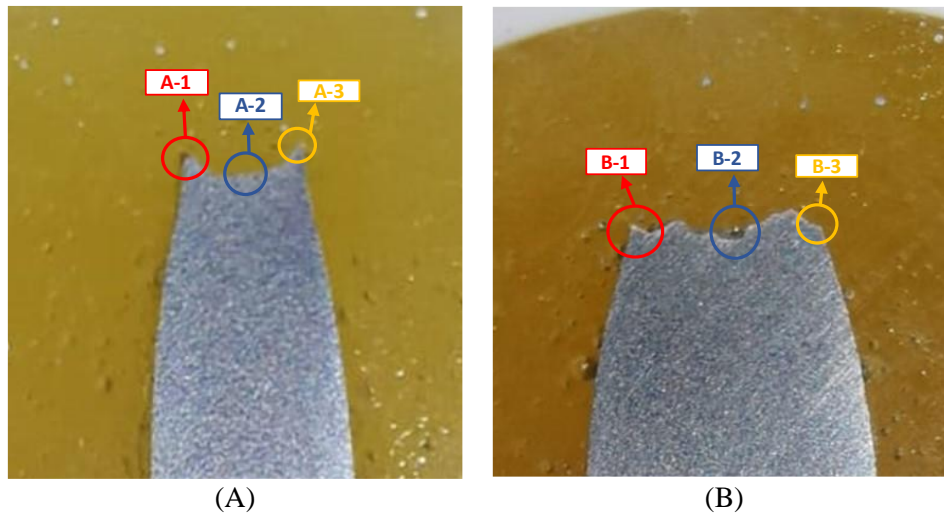


Struktur mikro bentuk patahan spesimen 6 mm bagian B-2 setelah pengujian tensile

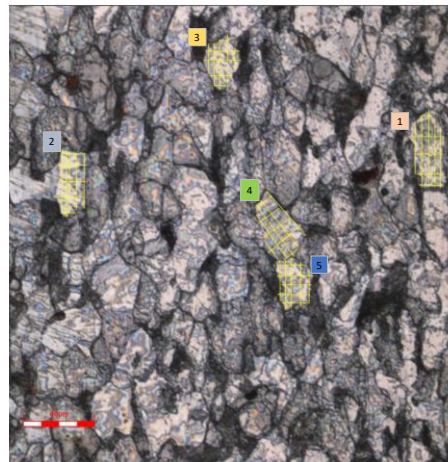


Struktur mikro bentuk patahan spesimen 6 mm bagian B-3 setelah setelah pengujian tensile

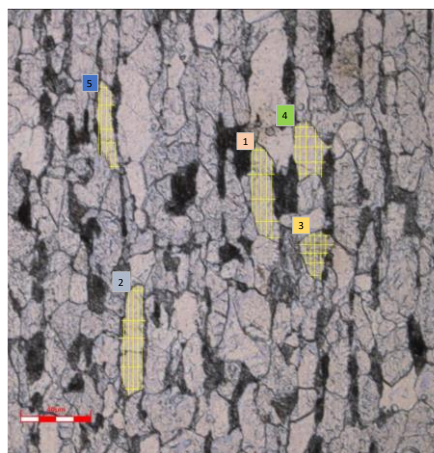
Lampiran A.4 Titik Lokasi Pengamatan Struktur Mikro dan Pengukuran Grain Rasio Spesimen 8 mm



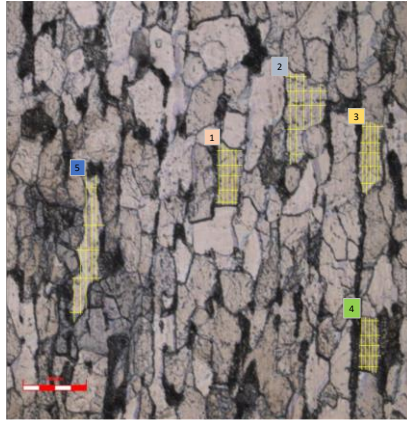
Bentuk patahan dan titik pengamatan struktur mikro pada spesimen 8 mm, (A) merupakan bagian tebal axial, (B) bagian sisi diameter luar dari *superheater* tube



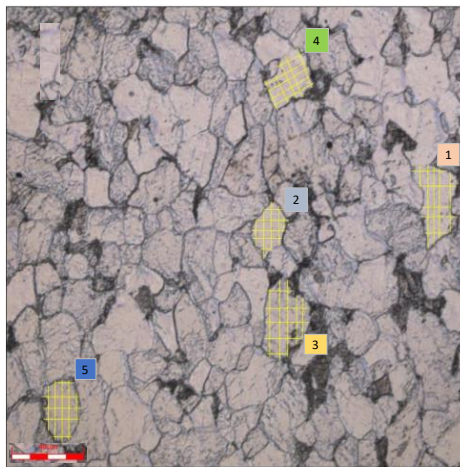
Struktur mikro spesimen 3 bagian A-atas setelah mengalami *creep displacement* 8 mm



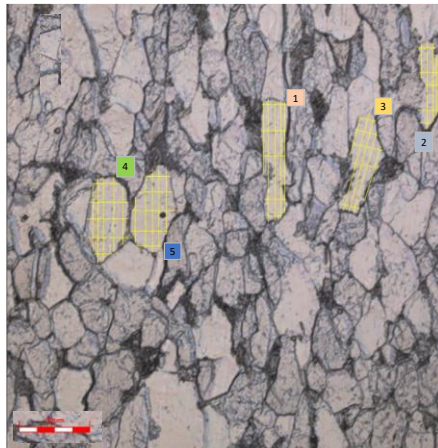
Struktur mikro spesimen 3 bagian A-tengah setelah mengalami *creep displacement* 8 mm



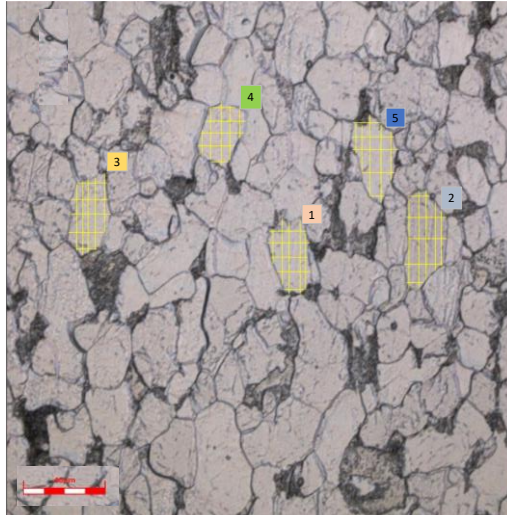
Struktur mikro spesimen 3 bagian A-bawah setelah mengalami *creep displacement* 8 mm



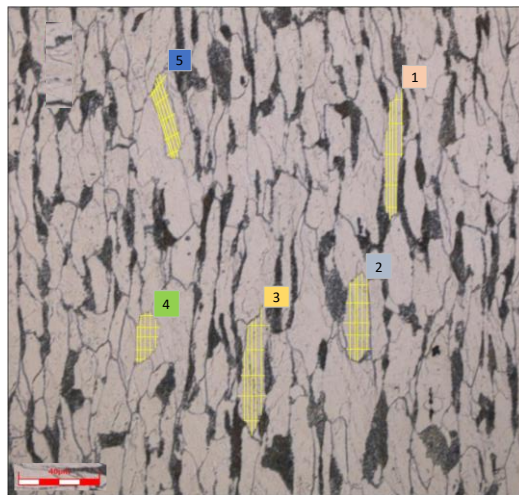
Struktur mikro spesimen 8 mm bagian B1 setelah mengalami *creep*



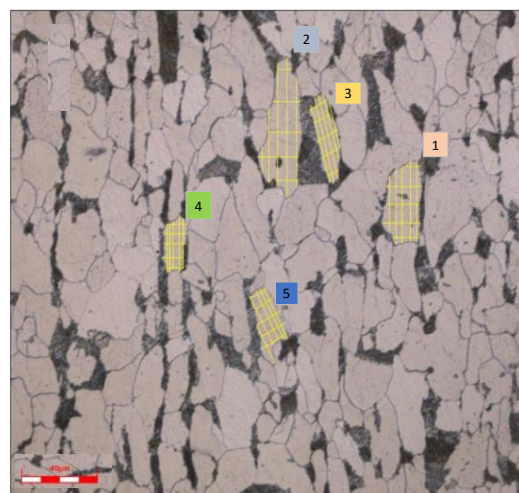
Struktur mikro spesimen 8 mm bagian B2 setelah mengalami *creep*



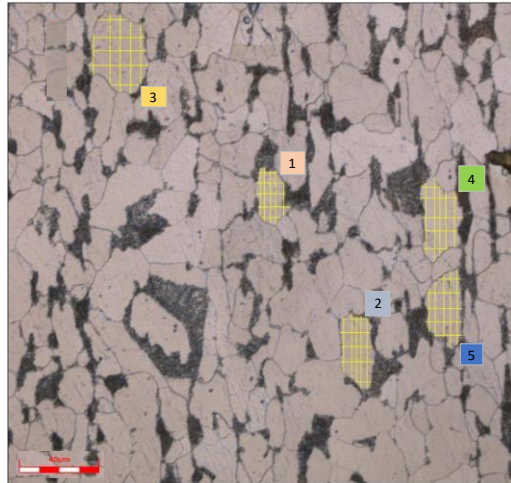
Struktur mikro spesimen 8 mm bagian B3 setelah mengalami *creep*



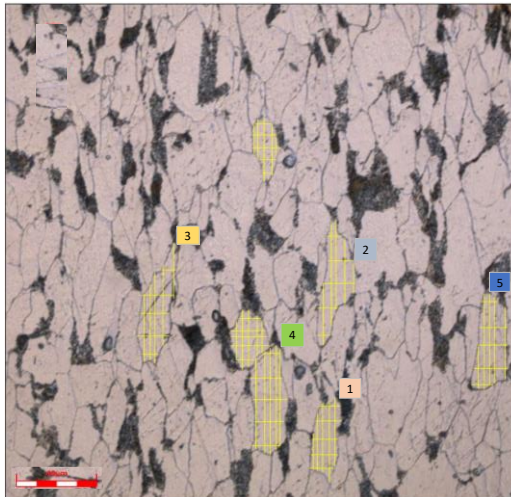
Struktur mikro spesimen 8 mm bagian A-a setelah setelah pengujian tensile



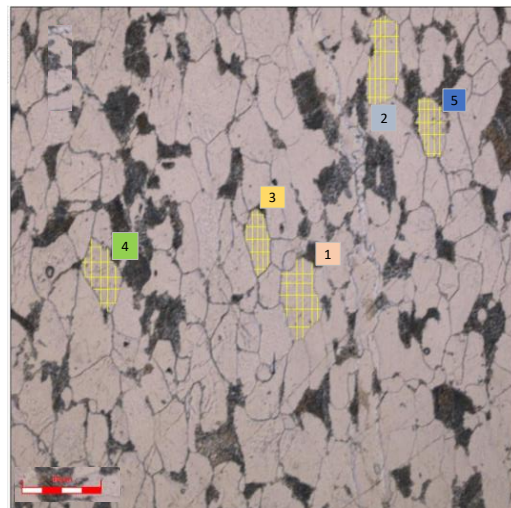
Struktur mikro spesimen 8 mm bagian A-b setelah pengujian tensile



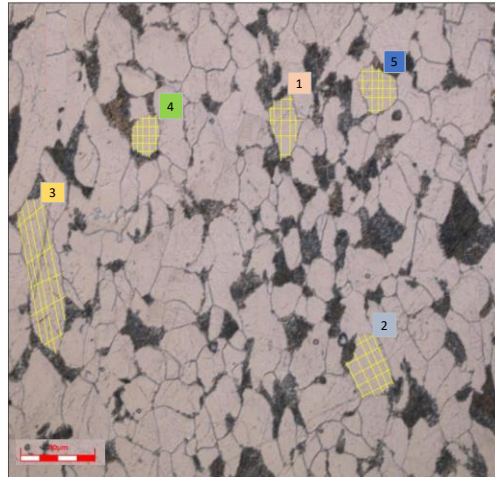
Struktur mikro spesimen 8 mm bagian A-c setelah setelah pengujian tensile



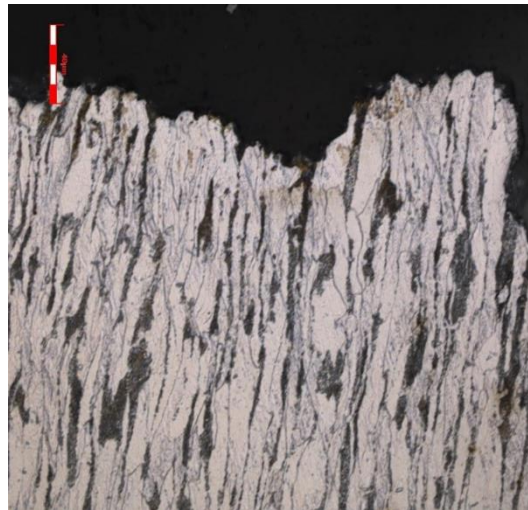
Struktur mikro spesimen 8 mm bagian B-a setelah setelah pengujian tensile



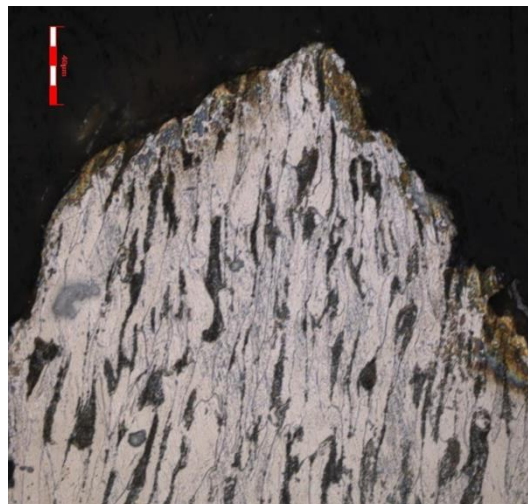
Struktur mikro spesimen 8 mm bagian B-b setelah pengujian tensile



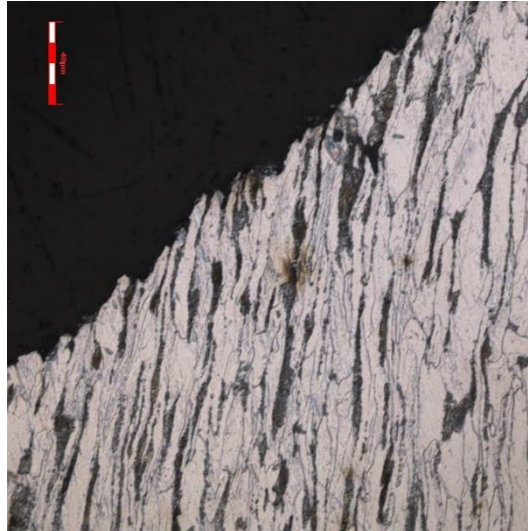
Struktur mikro spesimen 8 mm bagian B-c setelah setelah pengujian tensile



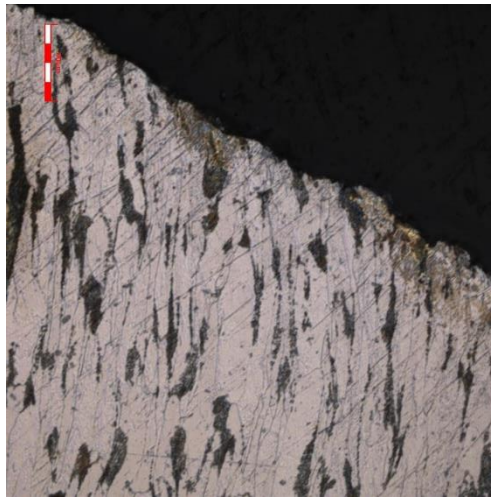
Struktur mikro spesimen 8 mm bagian A-1 setelah setelah pengujian tensile



Struktur mikro spesimen 8 mm bagian A-2 setelah pengujian tensile



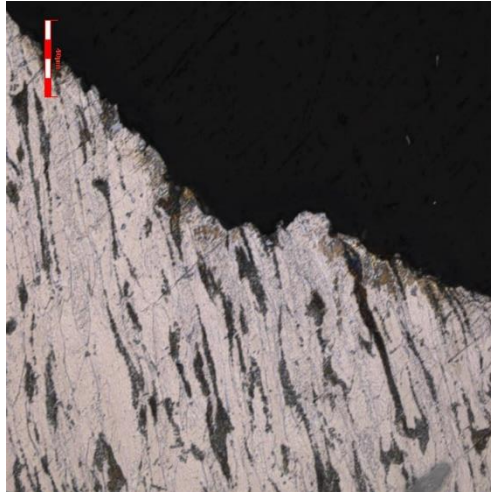
Struktur mikro spesimen 8 mm bagian A-3 setelah setelah pengujian tensile



Struktur mikro bentuk patahan spesimen 8 mm bagian B-1 setelah setelah pengujian tensile



Struktur mikro bentuk patahan spesimen 8 mm bagian B-2 setelah pengujian tensile



Struktur mikro bentuk patahan spesimen 8 mm bagian B-3 setelah setelah pengujian tensile

Lampiran B Data Pengujian *Grain Ratio*

Lampiran B.1 Data Pengukuran *Grain Ratio* Spesimen Raw

<i>Section A-atas</i>			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	9,389	21,165	0,443
2	12,413	21,636	0,573
3	20,120	23,090	0,871
4	13,986	18,814	0,743
5	10,974	20,608	0,532
<i>Grain Ratio Average</i>			0,664

<i>Section A-tengah</i>			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	18,257	24,778	0,737
2	10,633	23,323	0,456
3	18,488	29,970	0,617
4	15,823	21,360	0,741
5	17,154	29,342	0,585
<i>Grain Ratio Average</i>			0,684

<i>Section A-Bawah</i>			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	11,994	18,960	0,633
2	14,940	19,135	0,781
3	8,860	22,805	0,389
4	12,358	26,826	0,461
5	14,970	22,556	0,664
<i>Grain Ratio Average</i>			0,585

Section B1			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	14,545	18,909	0,769
2	17,990	19,686	0,914
3	20,965	21,542	0,973
4	17,354	28,662	0,605
5	16,392	26,065	0,629
<i>Grain Ratio Average</i>			0,843

Section B2			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	22.721	26.433	0,859
2	16.802	20.865	0,805
3	20.514	18.608	1,102
4	29.091	32.351	0,899
5	25.379	15.147	1,675
<i>Grain Ratio Average</i>			1,068

Section B3			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	20,336	17,247	1,179
2	17,990	16,772	1,073
3	20,965	17,542	1,195
4	17,354	18,662	0,930
5	20,344	16,690	1,219
<i>Grain Ratio Average</i>			1,125

Lampiran B.2 Data Pengukuran Grain Ratio Spesimen 4 mm

Section A-atas			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	10,8012	25,3734	0,425
2	22,467	39,3744	0,570
3	11,3134	14,564	0,776
4	17,2598	19,498	0,885
5	11,5402	19,0866	0,604
<i>Grain Ratio Average</i>			0,652

Section A-tengah			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	18,671	22,240	0,839
2	15,505	14,547	1,066
3	18,393	26,054	0,706
4	11,641	30,623	0,380
5	14,917	16,983	0,878
<i>Grain Ratio Average</i>			0,773

Section A-Bawah			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	20,543	37,401	0,549
2	10,498	27,129	0,387
3	10,852	24,883	0,436
4	18,473	34,776	0,531
5	14,940	24,227	0,617
<i>Grain Ratio Average</i>			0,504

Section B1			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	24,202	20,467	1,182
2	19,583	26,461	0,740
3	26,574	37,796	0,703
4	11,540	18,543	0,622
5	21,232	23,243	0,913
<i>Grain Ratio Average</i>			0,832

Section B2			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	18,214	31,547	0,577
2	21,585	21,786	0,991
3	14,373	16,889	0,851
4	16,805	19,069	0,881
5	21,585	21,032	1,026
<i>Grain Ratio Average</i>			0,865

Section B3			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	15,275	36,794	0,415
2	18,469	24,131	0,765
3	20,508	23,372	0,877
4	22,875	14,888	1,536
5	13,498	17,390	0,776
<i>Grain Ratio Average</i>			0,874

Section A-a			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	12,050	62,012	0,194
2	15,094	65,207	0,231
3	17,409	34,088	0,511
4	14,742	36,176	0,408
5	10,516	31,966	0,329
<i>Grain Ratio Average</i>			0,335

Section A-b			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	11,636	36,558	0,318
2	11,943	40,542	0,295
3	14,539	34,318	0,424
4	15,756	37,011	0,426
5	14,211	35,024	0,406
<i>Grain Ratio Average</i>			0,373

Section A-c			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	16,151	30,390	0,531
2	10,792	21,635	0,499
3	16,755	36,277	0,462
4	12,780	24,478	0,522
5	12,226	22,792	0,536
<i>Grain Ratio Average</i>			0,510

Section B-a			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	17,799	44,377	0,401
2	12,293	30,692	0,401
3	10,398	29,585	0,351
4	13,468	36,344	0,371
5	13,107	27,434	0,478
<i>Grain Ratio Average</i>			0,400

Section B-b			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	13,283	33,258	0,399
2	11,270	18,818	0,599
3	16,855	27,270	0,618
4	15,396	30,088	0,512
5	23,396	25,593	0,914
<i>Grain Ratio Average</i>			0,608

Section B-c			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	10,843	20,174	0,537
2	17,449	18,746	0,931
3	12,800	24,592	0,520
4	20,645	35,544	0,581
5	15,622	19,653	0,795
<i>Grain Ratio Average</i>			0,673

Lampiran B.3 Data Pengukuran Grain Ratio Spesimen 6 mm

<i>Section A-atas</i>			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	12,632	30,303	0,417
2	14,589	28,069	0,520
3	11,523	25,121	0,459
4	16,579	29,010	0,572
5	12,473	20,662	0,604
<i>Grain Ratio Average</i>			0,514

<i>Section A-tengah</i>			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	14,370	28,790	0,499
2	12,794	34,349	0,372
3	15,639	25,773	0,607
4	23,093	18,554	1,245
5	11,470	23,244	0,493
<i>Grain Ratio Average</i>			0,643

<i>Section A-Bawah</i>			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	20,076	46,132	0,435
2	10,549	29,451	0,358
3	11,659	21,224	0,549
4	9,590	36,593	0,262
5	19,129	33,817	0,566
<i>Grain Ratio Average</i>			0,434

Section B1			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	19,162	29,844	0,642
2	25,834	35,191	0,734
3	20,525	31,559	0,650
4	21,219	34,030	0,624
5	17,083	24,167	0,707
<i>Grain Ratio Average</i>			0,671

Section B2			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	16,008	32,579	0,491
2	13,213	29,924	0,442
3	17,820	33,343	0,534
4	15,829	36,170	0,438
5	12,188	52,228	0,233
<i>Grain Ratio Average</i>			0,427

Section B3			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	25,661	41,812	0,614
2	21,481	32,193	0,667
3	11,339	23,055	0,492
4	12,876	29,103	0,442
5	13,763	28,944	0,475
<i>Grain Ratio Average</i>			0,838

Section A-a			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	11,056	78,138	0,141
2	7,223	43,574	0,166
3	11,036	50,016	0,221
4	15,951	52,339	0,305
5	10,684	40,365	0,265
<i>Grain Ratio Average</i>			0,219

Section A-b			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	15,095	36,378	0,415
2	16,247	43,551	0,373
3	14,566	25,509	0,571
4	13,736	28,579	0,481
5	21,182	53,157	0,398
<i>Grain Ratio Average</i>			0,447

Section A-c			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	18,888	33,607	0,562
2	19,692	57,972	0,340
3	12,257	26,625	0,460
4	11,102	39,686	0,280
5	14,267	23,761	0,600
<i>Grain Ratio Average</i>			0,448

Section B-a			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	8,211	45,634	0,180
2	10,107	50,583	0,200
3	11,151	41,156	0,271
4	12,655	41,361	0,306
5	16,253	45,902	0,354
<i>Grain Ratio Average</i>			0,262

Section B-b			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	16,050	30,122	0,533
2	14,004	21,082	0,664
3	16,152	39,069	0,413
4	16,075	43,446	0,370
5	14,625	34,466	0,424
<i>Grain Ratio Average</i>			0,481

Section B-c			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	12,182	34,361	0,355
2	12,006	26,022	0,461
3	12,572	44,392	0,283
4	25,804	47,726	0,541
5	14,116	19,843	0,711
<i>Grain Ratio Average</i>			0,470

Lampiran B.4 Data Pengukuran Grain Ratio Spesimen 8 mm

<i>Section A-atas</i>			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	13,994	37,016	0,378
2	13,693	34,006	0,403
3	12,865	22,771	0,565
4	15,419	29,188	0,528
5	17,405	24,501	0,710
<i>Grain Ratio Average</i>			0,516

<i>Section A-tengah</i>			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	11,641	46,151	0,252
2	11,767	55,710	0,211
3	12,951	21,258	0,609
4	15,546	26,583	0,585
5	7,156	35,880	0,199
<i>Grain Ratio Average</i>			0,371

<i>Section A-Bawah</i>			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	14,312	34,718	0,412
2	16,739	37,846	0,442
3	12,674	39,144	0,324
4	12,464	32,034	0,389
5	12,170	55,433	0,220
<i>Grain Ratio Average</i>			0,357

Section B1			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	17,783	35,064	0,507
2	13,564	19,692	0,689
3	19,257	34,780	0,554
4	20,889	23,634	0,884
5	16,528	29,070	0,569
<i>Grain Ratio Average</i>			0,640

Section B2			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	12,835	61,564	0,208
2	10,650	36,144	0,295
3	14,019	43,135	0,325
4	19,290	41,896	0,460
5	19,391	39,385	0,492
<i>Grain Ratio Average</i>			0,356

Section B3			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	17,006	29,585	0,575
2	15,245	38,818	0,393
3	16,327	33,560	0,486
4	16,034	22,004	0,729
5	16,453	27,874	0,590
<i>Grain Ratio Average</i>			0,554

Section A-a			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	6,440	52,679	0,122
2	11,572	42,113	0,275
3	10,767	52,855	0,204
4	9,081	38,466	0,236
5	6,289	77,339	0,081
<i>Grain Ratio Average</i>			0,183

Section A-b			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	14,819	39,158	0,378
2	13,915	49,884	0,279
3	9,931	38,752	0,256
4	10,399	26,926	0,386
5	12,939	27,814	0,465
<i>Grain Ratio Average</i>			0,353

Section A-c			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	12,880	25,845	0,498
2	13,711	34,968	0,392
3	22,516	34,264	0,657
4	15,472	36,377	0,425
5	15,472	33,333	0,464
<i>Grain Ratio Average</i>			0,487

Section B-a			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	12,245	32,252	0,380
2	10,482	36,031	0,291
3	12,170	38,375	0,317
4	14,110	51,956	0,272
5	12,724	40,290	0,316
<i>Grain Ratio Average</i>			0,315

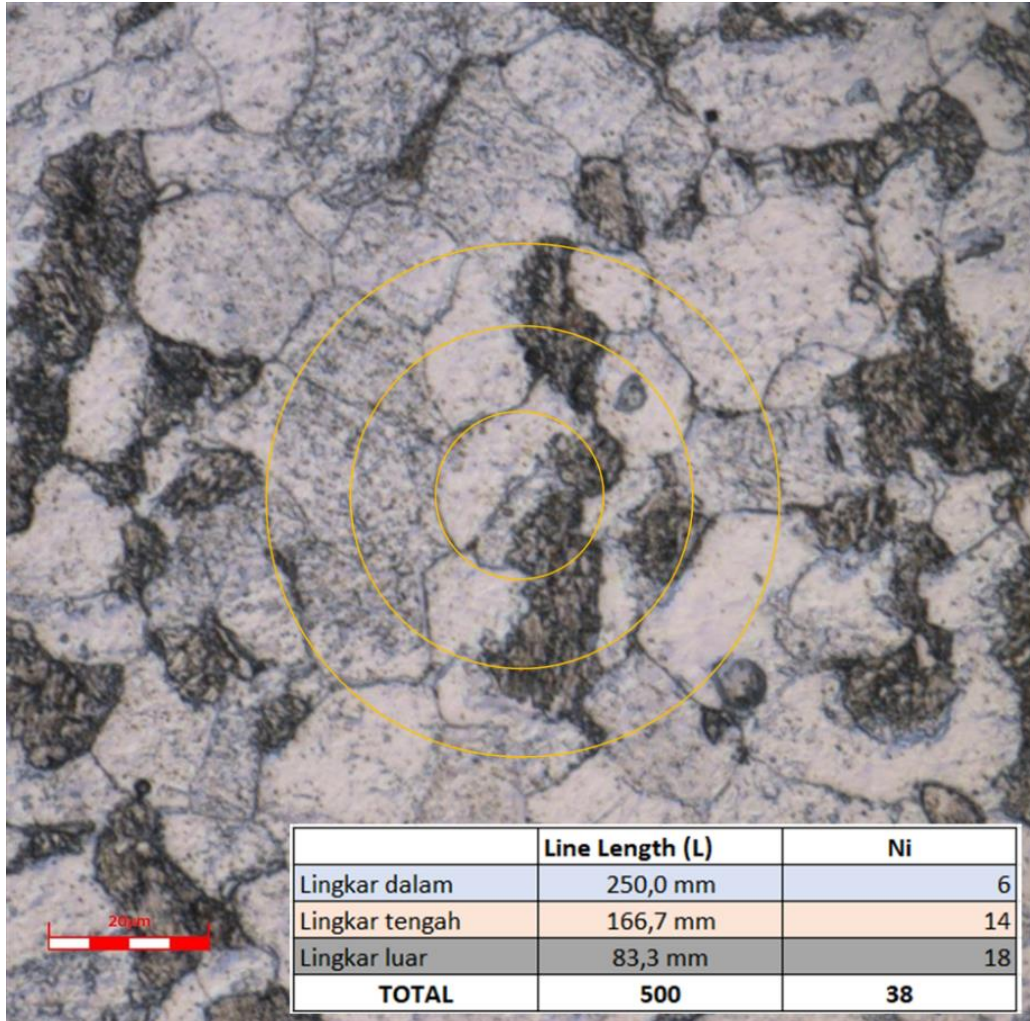
Section B-b			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	16,387	29,697	0,552
2	13,639	36,882	0,370
3	8,975	22,815	0,393
4	12,403	22,941	0,541
5	11,118	25,361	0,438
<i>Grain Ratio Average</i>			0,458

Section B-c			
<i>Grain</i>	<i>Horizontal line Average</i>	<i>Vertical line Average</i>	<i>Ratio</i>
1	10,918	22,088	0,494
2	18,272	28,656	0,638
3	17,592	75,828	0,232
4	11,698	18,667	0,627
5	14,826	20,596	0,720
<i>Grain Ratio Average</i>			0,542

Lampiran C Data Pengukuran Besar Butir Rata-Rata

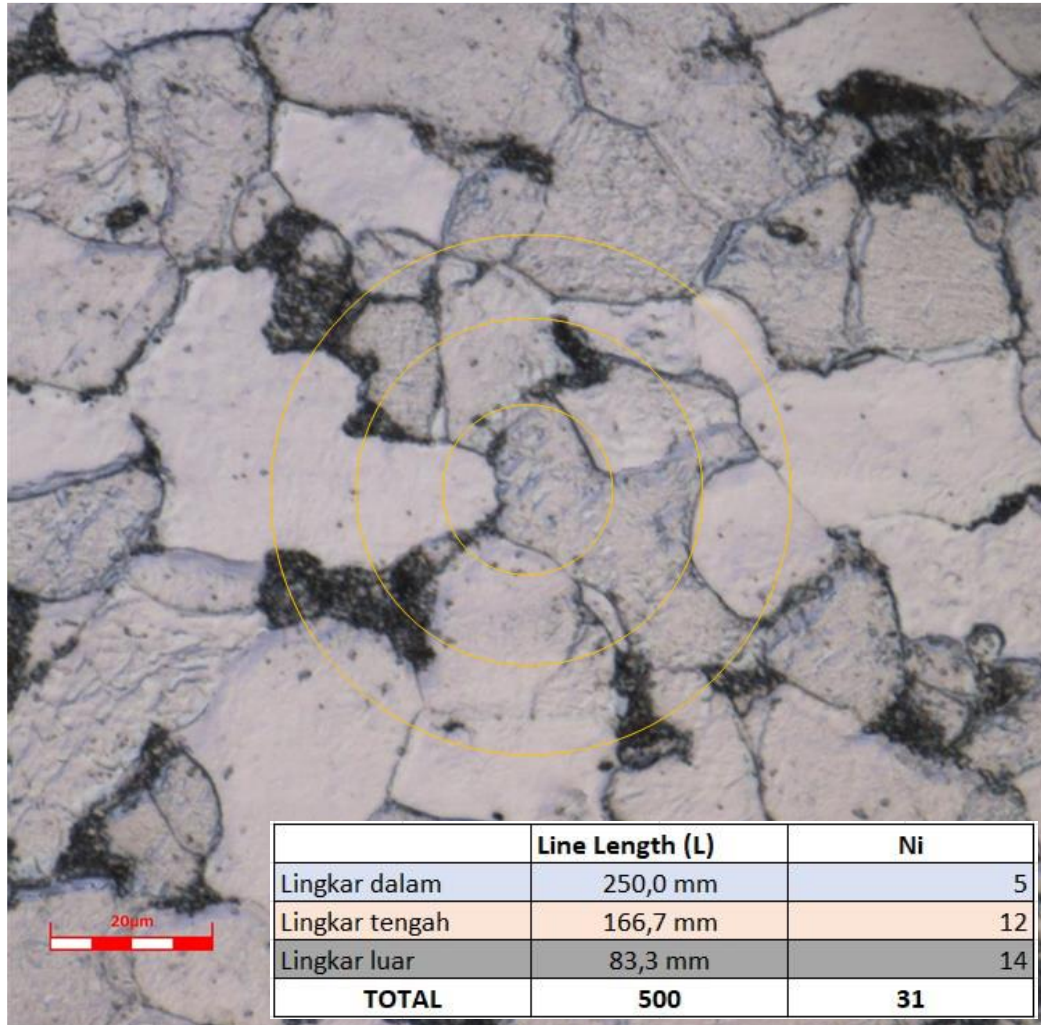
Lampiran C.1 Data perhitungan ASTM grain size Spesimen raw

N_i	L	M	$\bar{N}_L = \frac{N_i}{L/M}$	$\bar{\ell} = \frac{1}{\bar{N}_L}$	$G = (-6,643856 \log_{10} \bar{\ell}) - 3,288$
38	500	100	7,600	0,13158	2,564



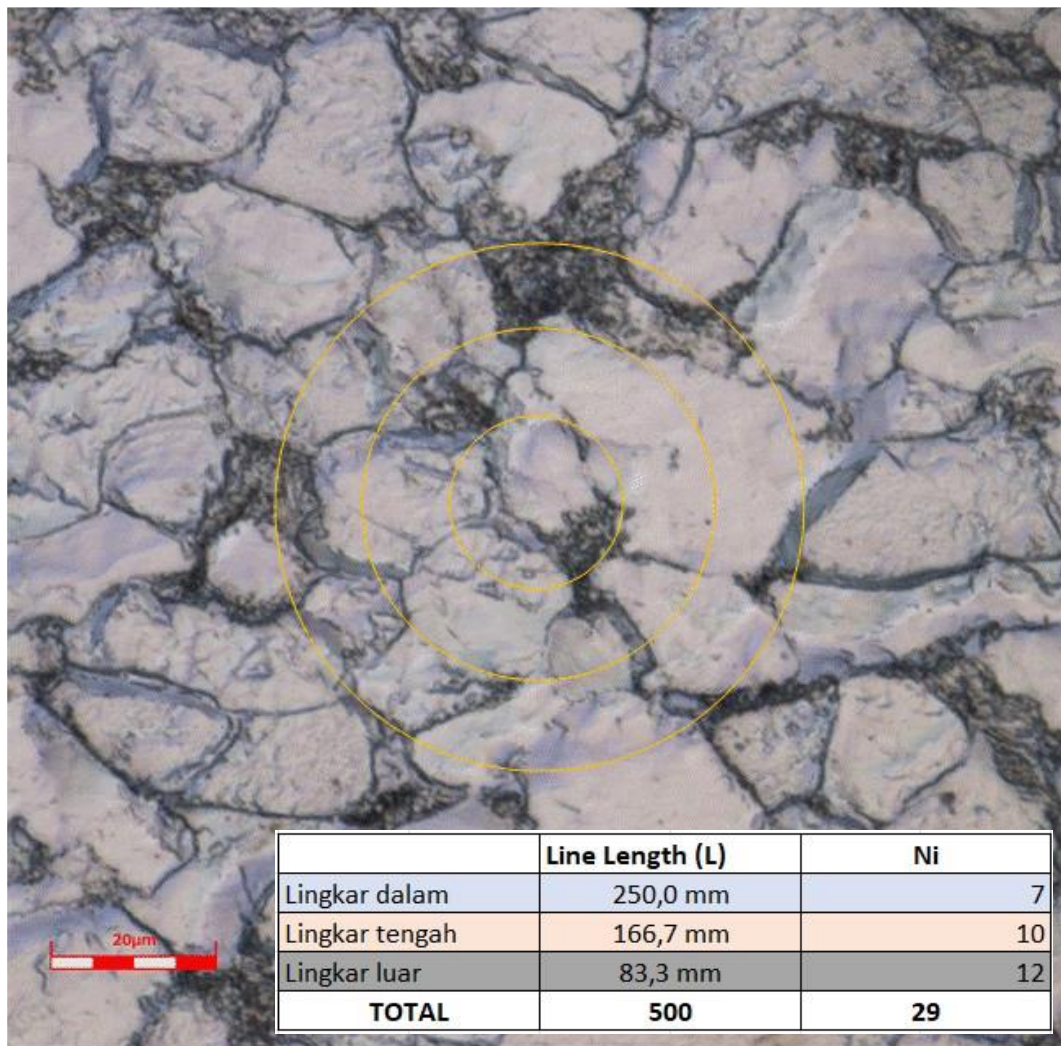
Lampiran C.2 Data perhitungan ASTM grain size Spesimen 4 mm

N_i	L	M	$\bar{N}_L = \frac{N_i}{L/M}$	$\bar{\ell} = \frac{1}{\bar{N}_L}$	$G = (-6,643856 \log_{10} \bar{\ell}) - 3,288$
31	500	100	6,200	0,16129	1,977



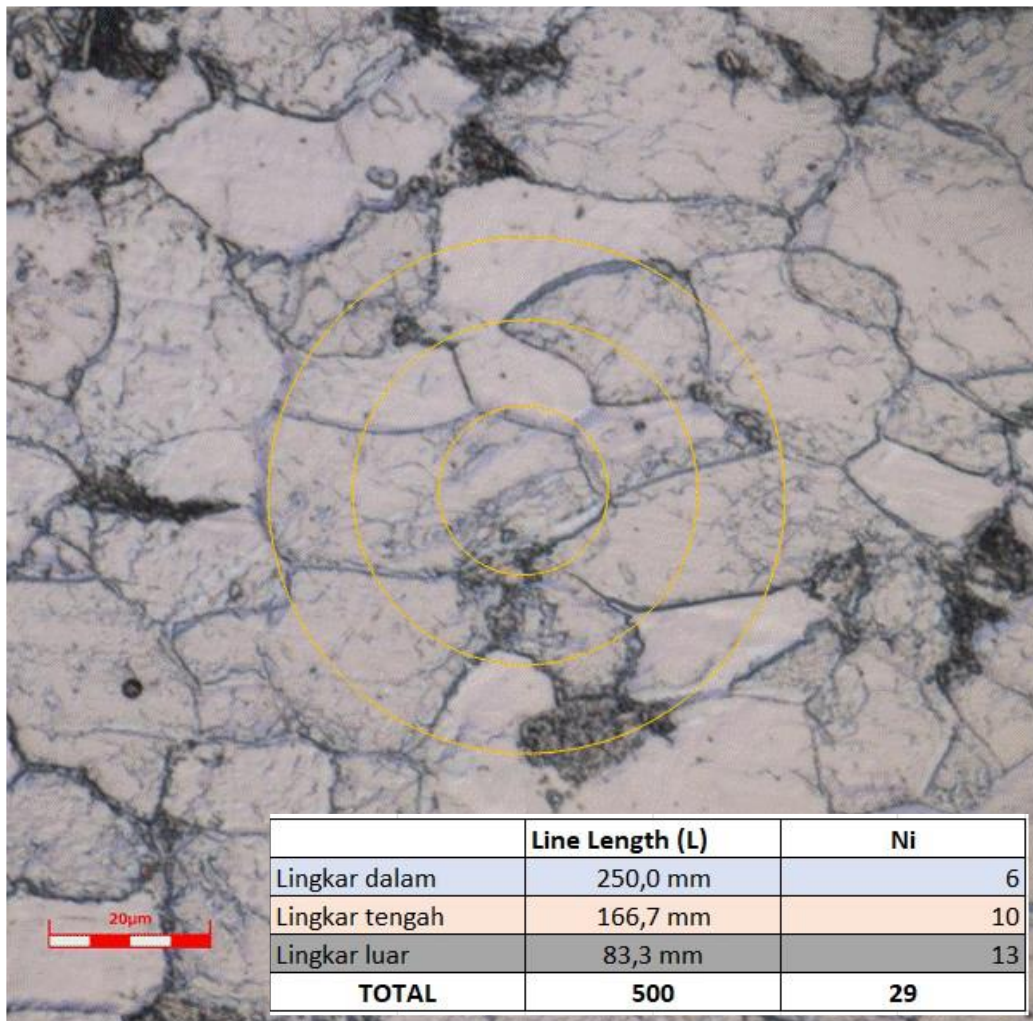
Lampiran C.3 Data perhitungan ASTM grain size Spesimen 6 mm

N_i	L	M	$\bar{N}_L = \frac{N_i}{L/M}$	$\bar{\ell} = \frac{1}{\bar{N}_L}$	$G = (-6,643856 \log_{10} \bar{\ell}) - 3,288$
29	500	100	5,800	0,17241	1,784



Lampiran C.4 Data perhitungan ASTM grain size Spesimen 8 mm

N_i	L	M	\bar{N}_L $= \frac{N_i}{L/M}$	$\bar{\ell} = \frac{1}{\bar{N}_L}$	$G = (-6,643856 \log_{10} \bar{\ell}) - 3,288$
29	500	100	5,800	0,17241	1,784



Lampiran D Data Pengujian Kekerasan

Lampiran D.1 Data pengujian kekerasan Spesimen raw

	B1			Average	B2			Average	B3			Average	Total Average
HV	156,4	154,2	158	156,2	158,9	151,2	159,4	156,5	153,4	158,1	156,6	156,0333333	156,2
HRB	81,8	81,1	82,3	81,733		80,1	82,7	81,4	80,8	82,3	81,9	81,667	81,6

Lampiran D.2 Data pengujian kekerasan Spesimen 4 mm

	B1			Average	B2			Average	B3			Average	Total Average
HV	114,7	115,4	116,6	115,6	122,0	119,6	116,9	119,5	114,0	112,5	110,1	112,2	115,8
HRB	63,8	64,2	64,9	64,3	68,0	66,4	65,0	66,5	63,3	62,3	61,4	62,3	64,4

Lampiran D.3 Data pengujian kekerasan Spesimen 6 mm

	B1			Average	B2			Average	B3			Average	Total Average
HV	117,2	112,4	114,4	114,7	120,2	122,6	119,0	120,6	115,5	117,0	114,4	115,6	117,0
HRB	65,2	62,2	63,2	63,5	66,7	68,3	66,0	67,0	64,3	65,1	63,5	64,3	64,9

Lampiran D. 4 Data pengujian kekerasan Spesimen 8 mm

	B1			Average	B2			Average	B3			Average	Total Average
HV	117,2	112,4	114,4	114,7	120,2	122,6	119,0	120,6	115,5	117,0	114,4	115,6	117,0
HRB	65,2	62,2	63,2	63,5	66,7	68,3	66,0	67,0	64,3	65,1	63,5	64,3	64,9

Lampiran E Dimensi Spesimen

Lampiran E.1 Dimensi spesimen 4 mm

SEBELUM CREEP									
W1		W2		W3		W4		W5	
A	6,49	A	6,2	A	6,13	A	6,06	A	6,37
B	6,53	B	6,22	B	6,16	B	6,16	B	6,42
C	6,24	C	5,95	C	5,89	C	5,97	C	6,25
W ave	6,42		6,123333		6,06		6,063333		6,346667
T1		T2		T3		T4		T5	
A	4,65	A	4,67	A	4,72	A	4,71	A	4,7
B	4,63	B	4,62	B	4,71	B	4,68	B	4,68
T average	4,64		4,645		4,715		4,695		4,69
		A1	A2	A3	A4	A5			
		29,7888	28,44288	28,5729	28,46735	29,76587			

SETELAH CREEP									
W1		W2		W3		W4		W5	
A		A		A		A		A	
B		B		B		B		B	
C		C		C		C		C	
W ave									
T1		T2		T3		T4		T5	
A		A		A		A		A	
B		B		B		B		B	
T average									
		A1	A2	A3	A4	A5			

SEBELUM TENSILE									
W1		W2		W3		W4		W5	
W1		W2		W3		W4		W5	
A	6,3	A	5,88	A	5,78	A	5,79	A	6,09
B	6,4	B	5,86	B	5,81	B	5,86	B	6,13
C	6,01	C	5,55	C	5,7	C	5,73	C	5,97
T1		T2		T3		T4		T5	
A	4,19	A	4,09	A	3,9	A	4,07	A	4,25
B	4,18	B	4,01	B	3,91	B	3,94	B	4,19
T average	4,185		4,05		3,905		4,005		4,22
		A1	A2	A3	A4	A5			
		25,82145	23,166	21,2432	22,04085	24,79953333			

Lampiran E.2 Dimensi spesimen 6 mm

SEBELUM CREEP									
W1		W2		W3		W4		W5	
A	6,34	A	6,08	A	5,92	A	5,9	A	6,04
B	6,41	B	6,21	B	6,04	B	6,05	B	6,14
C	6,4	C	6,24	C	6,05	C	6,03	C	6,09
W ave	6,383		6,177		6,003		5,993		6,090
T1		T2		T3		T4		T5	
A	4,35	A	4,38	A	4,38	A	4,41	A	5,54
B	4,34	B	4,39	B	4,38	B	4,43	B	4,51
T average	4,345		4,385		4,38		4,42		5,025
		A1	A2	A3	A4	A5			
		27,735	27,084	26,294	26,490	30,602			

SETELAH CREEP									
W1		W2		W3		W4		W5	
A	6,07	A	5,64	A	5,37	A	5,44	A	5,79
B	6,22	B	5,72	B	5,45	B	5,5	B	5,94
C	6,22	C	5,8	C	5,5	C	5,57	C	5,9
W ave	6,170		5,720		5,440		5,503		5,877
T1		T2		T3		T4		T5	
A	4,19	A	4,09	A	3,9	A	4,07	A	4,25
B	4,18	B	4,01	B	3,91	B	3,94	B	4,19
T average	4,185		4,05		3,905		4,005		4,22
		A1	A2	A3	A4	A5			
		25,821	23,166	21,243	22,040	24,799			

SEBELUM TENSILE									
W1		W2		W3		W4		W5	
A	6,12	A	5,6	A	5,21	A	5,3	A	5,68
B	6,14	B	5,66	B	5,38	B	5,46	B	5,83
C	6,07	C	5,66	C	5,36	C	5,46	C	5,94
W ave	6,11		5,64		5,316		5,406		5,816
T1		T2		T3		T4		T5	
A	4,06	A	3,86	A	3,72	A	3,88	A	4,07
B	4,01	B	3,88	B	3,78	B	3,9	B	4,02
T average	4,035		3,87		3,75		3,89		4,045
		A1	A2	A3	A4	A5			
		24,653	21,826	19,937	21,031	23,528			

Lampiran E. 3 Dimensi spesimen 8 mm

SEBELUM CREEP									
W1		W2		W3		W4		W5	
A	6,29	A	6,07	A	5,97	A	6,05	A	6,28
B	6,33	B	6,06	B	6,03	B	6,09	B	5,34
C	6,19	C	5,83	C	5,79	C	5,87	C	6,24
W ave	6,270		5,987		5,930		6,003		5,953
T1		T2		T3		T4		T5	
A	4,63	A	4,59	A	4,64	A	4,63	A	4,69
B	4,58	B	4,57	B	4,59	B	4,52	B	4,62
T average	4,605		4,58		4,615		4,575		4,655
		A1	A2	A3	A4	A5			
		28,873	27,419	27,367	27,465	27,713			

SETELAH CREEP									
W1		W2		W3		W4		W5	
A	5,87	A	5,26	A	5,1	A	5,52	A	5,84
B	5,88	B	5,27	B	5,16	B	5,55	B	6,06
C	5,87	C	5,02	C	4,95	C	5,49	C	5,56
W ave	5,873		5,183		5,070		5,520		5,820
T1		T2		T3		T4		T5	
A	4,24	A	3,85	A	3,88	A	3,94	A	4,94
B	4,19	B	3,87	B	3,76	B	4,11	B	4,28
T average	4,215		3,86		3,82		4,025		4,61
		A1	A2	A3	A4	A5			
		24,756	20,008	19,367	22,218	26,830			

SEBELUM TENSILE									
W1		W2		W3		W4		W5	
A	5,81	A	5,09	A	5,09	A	5,25	A	8,86
B	5,85	B	5,08	B	5,18	B	5,39	B	5,9
C	5,83	C	4,91	C	4,94	C	5,12	C	5,55
W ave	5,830		5,027		5,070		5,253		6,770
T1		T2		T3		T4		T5	
A	4,1	A	3,9	A	3,88	A	3,94	A	4,26
B	4,12	B	3,79	B	3,91	B	3,99	B	4,22
T average	4,11		3,845		3,895		3,965		4,24
		A1	A2	A3	A4	A5			
		23,961	19,328	19,748	20,829	28,705			

Lampiran F Perhitungan Laju Creep

Lampiran F. 1 Perhitungan laju creep rupture

section	displacement awal	displacement akhir	Total $d\varepsilon$	Waktu awal	Waktu akhir	Total dt	Creep rate $d\varepsilon/dt$
1	4,954	5,165	0,211	455	710	255	0,0008
2	5,175	5,415	0,240	715	970	255	0,0009
3	5,419	5,708	0,289	975	1230	255	0,0011
4	5,713	6,050	0,337	1235	1490	255	0,0013
5	6,062	6,429	0,367	195	450	255	0,0014

Lampiran G Data Curva Creep

Lampiran G.1 Data curva creep rupture

CREEP-RUPTURE DATA													
MATERIAL		GB 5310 20G			SPECIMEN		4		THICKNESS			Minimum (mm)	4,74
TEMPERATURE		550°C			LOAD/MASS		75,1 kg					Average (mm)	4,75
No.	Date	Time			Duration (hour)	Length /l (mm)	No.	Date	Time			Duration (hour)	Length /l (mm)
		Hour	Min.	Sec.					Hour	Min.	Sec.		
1	7/09/2022 Start Load	10	00	00	--	1,98	58	--	14	45	00	--	4,06
2		10	05	00	--	2,04	59	--	14	50	00	--	4,08
3	--	10	10	00	--	2,092	60	--	14	55	00	--	4,106
4	--	10	15	00	--	2,14	61	--	15	00	00	--	4,13
5	--	10	20	00	--	2,20	62	--	15	05	00	--	4,15
6	--	10	25	00	--	2,248	63	--	15	10	00	--	4,17
7	--	10	30	00	--	2,30	64	--	15	15	00	--	4,189
8	--	10	35	00	--	2,35	65	--	15	20	00	--	4,21
9	--	10	40	00	--	2,40	66	--	15	25	00	--	4,23
10	--	10	45	00	--	2,445	67	--	15	30	00	--	4,248
11	--	10	50	00	--	2,49	68	--	15	35	00	--	4,267
12	--	10	55	00	--	2,54	69	--	15	40	00	--	4,29
13	--	11	00	00	--	2,58	70	--	15	45	00	--	4,30
14	--	11	05	00	--	2,630	71	--	15	50	00	--	4,32
15	--	11	10	00	--	2,675	72	--	15	55	00	--	4,339
16	--	11	15	00	--	2,719	73	--	16	00	00	--	4,36
17	--	11	20	00	--	2,76	74	--	16	05	00	--	4,37
18	--	11	25	00	--	2,805	75	--	16	10	00	--	4,39
19	--	11	30	00	--	2,85	76	--	16	15	00	--	4,406
20	--	11	35	00	--	2,889	77	--	16	20	00	--	4,42
21	--	11	40	00	--	2,93	78	--	16	25	00	--	4,44
22	--	11	45	00	--	2,97	79	--	16	30	00	--	4,45
23	--	11	50	00	--	3,009	80	--	16	35	00	--	4,468
24	--	11	55	00	--	3,048	81	--	16	40	00	--	4,48
25	--	12	00	00	--	3,087	82	--	16	45	00	--	4,50
26	--	12	05	00	--	3,12	83	--	16	50	00	--	4,51
27	--	12	10	00	--	3,16	84	--	16	55	00	--	4,53
28	--	12	15	00	--	3,20	85	--	17	00	00	--	4,540
29	--	12	20	00	--	3,23	86	--	17	05	00	--	4,55
30	--	12	25	00	--	3,270	87	--	17	10	00	--	4,56
31	--	12	30	00	--	3,30	88	--	17	15	00	--	4,57
32	--	12	35	00	--	3,34	89	--	17	20	00	--	4,575
33	--	12	40	00	--	3,37	90	--	17	25	00	--	4,583

34	--	12	45	00	--	3,407	91	--	17	30	00	--	4,59
35	--	12	50	00	--	3,439	92	--	17	35	00	--	4,597
36	--	12	55	00	--	3,47	93	--	17	40	00	--	4,608
37	--	13	00	00	--	3,50	94	--	17	45	00	--	4,612
38	--	13	05	00	--	3,53	95	--	17	50	00	--	4,624
39	--	13	10	00	--	3,57	96	--	17	55	00	--	4,628
40	--	13	15	00	--	3,60	97	--	18	00	00	--	4,638
41	--	13	20	00	--	3,63	98	--	18	05	00	--	4,644
42	--	13	25	00	--	3,65	99	--	18	10	00	--	4,647
43	--	13	30	00	--	3,684	100	--	18	15	00	--	4,65
44	--	13	35	00	--	3,712	101	--	18	20	00	--	4,658
45	--	13	40	00	--	3,740	102	--	18	25	00	--	4,668
46	--	13	45	00	--	3,77	103	--	18	30	00	--	4,67
47	--	13	50	00	--	3,79	104	--	18	35	00	--	4,68
48	--	13	55	00	--	3,82	105	--	18	40	00	--	4,69
49	--	14	00	00	--	3,847	106	--	18	45	00	--	4,705
50	--	14	05	00	--	3,87	107	--	18	50	00	--	4,708
51	--	14	10	00	--	3,90	108	--	18	55	00	--	4,71
52	--	14	15	00	--	3,92	109	--	19	00	00	--	4,715
53	--	14	20	00	--	3,95	110	--	19	05	00	--	4,718
54	--	14	25	00	--	3,97	111	--	19	10	00	--	4,723
55	--	14	30	00	--	3,994	112	--	19	15	00	--	4,728
56	--	14	35	00	--	4,02	113	--	19	20	00	--	4,73
57	--	14	40	00	--	4,04	114	--	19	25	00	--	4,739
115	--	19	30	00	--	4,749	172	--	00	15	00	--	5,022
116	--	19	35	00	--	4,75	173	--	00	20	00	--	5,022
117	--	19	40	00	--	4,759	174	--	00	25	00	--	5,03
118	--	19	45	00	--	4,765	175	--	00	30	00	--	5,034
119	--	19	50	00	--	4,77	176	--	00	35	00	--	5,043
120	--	19	55	00	--	4,774	177	--	00	40	00	--	5,045
121	--	20	00	00	--	4,783	178	--	00	45	00	--	5,05
122	--	20	05	00	--	4,786	179	--	00	50	00	--	5,054
123	--	20	10	00	--	4,795	180	--	00	55	00	--	5,06
124	--	20	15	00	--	4,798	181	--	01	00	00	--	5,065
125	--	20	20	00	--	4,8	182	--	01	05	00	--	5,068
126	--	20	25	00	--	4,804	183	--	01	10	00	--	5,073
127	--	20	30	00	--	4,809	184	--	01	15	00	--	5,078
128	--	20	35	00	--	4,813	185	--	01	20	00	--	5,085
129	--	20	40	00	--	4,815	186	--	01	25	00	--	5,09
130	--	20	45	00	--	4,819	187	--	01	30	00	--	5,095
131	--	20	50	00	--	4,822	188	--	01	35	00	--	5,097

132	--	20	55	00	--	4,83	189	--	01	40	00	--	5,1
133	--	21	00	00	--	4,835	190	--	01	45	00	--	5,105
134	--	21	05	00	--	4,835	191	--	01	50	00	--	5,11
135	--	21	10	00	--	4,842	192	--	01	55	00	--	5,115
136	--	21	15	00	--	4,85	193	--	02	00	00	--	5,12
137	--	21	20	00	--	4,855	194	--	02	05	00	--	5,124
138	--	21	25	00	--	4,868	195	--	02	10	00	--	5,126
139	--	21	30	00	--	4,868	196	--	02	15	00	--	5,13
140	--	21	35	00	--	4,869	197	--	02	20	00	--	5,133
141	--	21	40	00	--	4,875	198	--	02	25	00	--	5,136
142	--	21	45	00	--	4,897	199	--	02	30	00	--	5,14
143	--	21	50	00	--	4,889	200	--	02	35	00	--	5,144
144	--	21	55	00	--	4,89	201	--	02	40	00	--	5,146
145	--	22	00	00	--	4,895	202	--	02	45	00	--	5,148
146	--	22	05	00	--	4,9	203	--	02	50	00	--	5,15
147	--	22	10	00	--	4,9	204	--	02	55	00	--	5,155
148	--	22	15	00	--	4,905	205	--	03	00	00	--	5,157
149	--	22	20	00	--	4,913	206	--	03	05	00	--	5,16
150	--	22	25	00	--	4,92	207	--	03	10	00	--	5,165
151	--	22	30	00	--	4,92	208	--	03	15	00	--	5,175
152	--	22	35	00	--	4,927	209	--	03	20	00	--	5,176
153	--	22	40	00	--	4,932	210	--	03	25	00	--	5,18
154	--	22	45	00	--	4,933	211	--	03	30	00	--	5,182
155	--	22	50	00	--	4,952	212	--	03	35	00	--	5,188
156	--	22	55	00	--	4,945	213	--	03	40	00	--	5,193
157	--	23	00	00	--	4,95	214	--	03	45	00	--	5,197
158	--	23	05	00	--	4,956	215	--	03	50	00	--	5,2
159	--	23	10	00	--	4,963	216	--	03	55	00	--	5,205
160	--	23	15	00	--	4,967	217	--	04	00	00	--	5,21
161	--	23	20	00	--	4,97	218	--	04	05	00	--	5,216
162	--	23	25	00	--	4,974	219	--	04	10	00	--	5,218
163	--	23	30	00	--	4,98	220	--	04	15	00	--	5,22
164	--	23	35	00	--	4,984	221	--	04	20	00	--	5,226
165	--	23	40	00	--	4,992	222	--	04	25	00	--	5,228
166	--	23	45	00	--	4,994	223	--	04	30	00	--	5,234
167	--	23	50	00	--	4,999	224	--	04	35	00	--	5,24
168	--	23	55	00	--	5,006	225	--	04	40	00	--	5,242
169	08/09/2022	00	00	00	--	5,01	226	--	04	45	00	--	5,247
170	--	00	05	00	--	5,01	227	--	04	50	00	--	5,252
171	--	00	10	00	--	5,018	228	--	04	55	00	--	5,26
229	--	05	00	00	--	5,266	286	--	09	45	00	--	5,557

230	--	05	05	00	--	5,27	287	--	09	50	00	--	5,564
231	--	05	10	00	--	5,27	288	--	09	55	00	--	5,57
232	--	05	15	00	--	5,28	289	--	10	00	00	--	5,58
233	--	05	20	00	--	5,288	290	--	10	05	00	--	5,585
234	--	05	25	00	--	5,29	291	--	10	10	00	--	5,59
235	--	05	30	00	--	5,294	292	--	10	15	00	--	5,596
236	--	05	35	00	--	5,3	293	--	10	20	00	--	5,6
237	--	05	40	00	--	5,302	294	--	10	25	00	--	5,608
238	--	05	45	00	--	5,308	295	--	10	30	00	--	5,612
239	--	05	50	00	--	5,313	296	--	10	35	00	--	5,62
240	--	05	55	00	--	5,318	297	--	10	40	00	--	5,626
241	--	06	00	00	--	5,322	298	--	10	45	00	--	5,63
242	--	06	05	00	--	5,328	299	--	10	50	00	--	5,638
243	--	06	10	00	--	5,331	300	--	10	55	00	--	5,64
244	--	06	15	00	--	5,339	301	--	11	00	00	--	5,648
245	--	06	20	00	--	5,349	302	--	11	05	00	--	5,65
246	--	06	25	00	--	5,35	303	--	11	10	00	--	5,657
247	--	06	30	00	--	5,359	304	--	11	15	00	--	5,66
248	--	06	35	00	--	5,359	305	--	11	20	00	--	5,67
249	--	06	40	00	--	5,36	306	--	11	25	00	--	5,676
250	--	06	45	00	--	5,365	307	--	11	30	00	--	5,682
251	--	06	50	00	--	5,37	308	--	11	35	00	--	5,69
252	--	06	55	00	--	5,375	309	--	11	40	00	--	5,698
253	--	07	00	00	--	5,381	310	--	11	45	00	--	5,702
254	--	07	05	00	--	5,389	311	--	11	50	00	--	5,708
255	--	07	10	00	--	5,399	312	--	11	55	00	--	5,713
256	--	07	15	00	--	5,4	313	--	12	00	00	--	5,718
257	--	07	20	00	--	5,405	314	--	12	05	00	--	5,723
258	--	07	25	00	--	5,41	315	--	12	10	00	--	5,73
259	--	07	30	00	--	5,415	316	--	12	15	00	--	5,734
260	--	07	35	00	--	5,419	317	--	12	20	00	--	5,74
261	--	07	40	00	--	5,425	318	--	12	25	00	--	5,748
262	--	07	45	00	--	5,43	319	--	12	30	00	--	5,753
263	--	07	50	00	--	5,439	320	--	12	35	00	--	5,758
264	--	07	55	00	--	5,445	321	--	12	40	00	--	5,763
265	--	08	00	00	--	5,45	322	--	12	45	00	--	5,77
266	--	08	05	00	--	5,455	323	--	12	50	00	--	5,775
267	--	08	10	00	--	5,46	324	--	12	55	00	--	5,78
268	--	08	15	00	--	5,462	325	--	13	00	00	--	5,79
269	--	08	20	00	--	5,467	326	--	13	05	00	--	5,792
270	--	08	25	00	--	5,471	327	--	13	10	00	--	5,795

271	--	08	30	00	--	5,475	328	--	13	15	00	--	5,802
272	--	08	35	00	--	5,48	329	--	13	20	00	--	5,807
273	--	08	40	00	--	5,485	330	--	13	25	00	--	5,812
274	--	08	45	00	--	5,49	331	--	13	30	00	--	5,818
275	--	08	50	00	--	5,495	332	--	13	35	00	--	5,823
276	--	08	55	00	--	5,502	333	--	13	40	00	--	5,83
277	--	09	00	00	--	5,51	334	--	13	45	00	--	5,839
278	--	09	05	00	--	5,511	335	--	13	50	00	--	5,845
279	--	09	10	00	--	5,52	336	--	13	55	00	--	5,85
280	--	09	15	00	--	5,53	337	--	14	00	00	--	5,858
281	--	09	20	00	--	5,534	338	--	14	05	00	--	5,87
282	--	09	25	00	--	5,538	339	--	14	10	00	--	5,876
283	--	09	30	00	--	5,54	340	--	14	15	00	--	5,882
284	--	09	35	00	--	5,548	341	--	14	20	00	--	5,888
285	--	09	40	00	--	5,55	342	--	14	25	00	--	5,894
343	--	14	30	00	--	5,9	400	--	19	15	00	--	6,31
344	--	14	35	00	--	5,908	401	--	19	20	00	--	6,318
345	--	14	40	00	--	5,913	402	--	19	25	00	--	6,322
346	--	14	45	00	--	5,92	403	--	19	30	00	--	6,33
347	--	14	50	00	--	5,934	404	--	19	35	00	--	6,34
348	--	14	55	00	--	5,94	405	--	19	40	00	--	6,355
349	--	15	00	00	--	5,95	406	--	19	45	00	--	6,36
350	--	15	05	00	--	5,958	407	--	19	50	00	--	6,367
351	--	15	10	00	--	5,963	408	--	19	55	00	--	6,375
352	--	15	15	00	--	5,97	409	--	20	00	00	--	6,383
353	--	15	20	00	--	5,974	410	--	20	05	00	--	6,39
354	--	15	25	00	--	5,98	411	--	20	10	00	--	6,396
355	--	15	30	00	--	5,99	412	--	20	15	00	--	6,4
356	--	15	35	00	--	5,997	413	--	20	20	00	--	6,412
357	--	15	40	00	--	6,003	414	--	20	25	00	--	6,42
358	--	15	45	00	--	6,01	415	--	20	30	00	--	6,429
359	--	15	50	00	--	6,022	416	--	20	35	00	--	6,438
360	--	15	55	00	--	6,03	417	--	20	40	00	--	6,45
361	--	16	00	00	--	6,04	418	--	20	45	00	--	6,463
362	--	16	05	00	--	6,045	419	--	20	50	00	--	6,472
363	--	16	10	00	--	6,05	420	--	20	55	00	--	6,48
364	--	16	15	00	--	6,062	421	--	21	00	00	--	6,5
365	--	16	20	00	--	6,068	422	--	21	05	00	--	6,5
366	--	16	25	00	--	6,074	423	--	21	10	00	--	6,502
367	--	16	30	00	--	6,082	424	--	21	15	00	--	6,512
368	--	16	35	00	--	6,093	425	--	21	20	00	--	6,528

369	--	16	40	00	--	6,1	426	--	21	25	00	--	6,54
370	--	16	45	00	--	6,107	427	--	21	30	00	--	6,548
371	--	16	50	00	--	6,12	428	--	21	35	00	--	6,56
372	--	16	55	00	--	6,13	429	--	21	40	00	--	6,568
373	--	17	00	00	--	6,136	430	--	21	45	00	--	6,575
374	--	17	05	00	--	6,14	431	--	21	50	00	--	6,583
375	--	17	10	00	--	6,149	432	--	21	55	00	--	6,59
376	--	17	15	00	--	6,15	433	--	22	00	00	--	6,605
377	--	17	20	00	--	6,16	434	--	22	05	00	--	6,613
378	--	17	25	00	--	6,17	435	--	22	10	00	--	6,623
379	--	17	30	00	--	6,176	436	--	22	15	00	--	6,63
380	--	17	35	00	--	6,188	437	--	22	20	00	--	6,643
381	--	17	40	00	--	6,2	438	--	22	25	00	--	6,65
382	--	17	45	00	--	6,21	439	--	22	30	00	--	6,658
383	--	17	50	00	--	6,215	440	--	22	35	00	--	6,668
384	--	17	55	00	--	6,223	441	--	22	40	00	--	6,68
385	--	18	00	00	--	6,23	442	--	22	45	00	--	6,692
386	--	18	05	00	--	6,235	443	--	22	50	00	--	6,7
387	--	18	10	00	--	6,239	444	--	22	55	00	--	6,718
388	--	18	15	00	--	6,239	445	--	23	00	00	--	6,72
389	--	18	20	00	--	6,245	446	--	23	05	00	--	6,73
390	--	18	25	00	--	6,25	447	--	23	10	00	--	6,742
391	--	18	30	00	--	6,257	448	--	23	15	00	--	6,75
392	--	18	35	00	--	6,27	449	--	23	20	00	--	6,763
393	--	18	40	00	--	6,275	450	--	23	25	00	--	6,775
394	--	18	45	00	--	6,283	451	--	23	30	00	--	6,784
395	--	18	50	00	--	6,293	452	--	23	35	00	--	6,798
396	--	18	55	00	--	6,305	453	--	23	40	00	--	6,805
397	--	19	00	00	--	6,306	454	--	23	45	00	--	6,817
398	--	19	05	00	--	6,308	455	--	23	50	00	--	6,821
399	--	19	10	00	--	6,31	456	--	23	55	00	--	6,834
457	09/09/2022	00	00	00	--	6,848	514	--	04	45	00	--	7,613
458	--	00	05	00	--	6,856	515	--	04	50	00	--	7,628
459	--	00	10	00	--	6,87	516	--	04	55	00	--	7,64
460	--	00	15	00	--	6,883	517	--	05	00	00	--	7,652
461	--	00	20	00	--	6,89	518	--	05	05	00	--	7,667
462	--	00	25	00	--	6,903	519	--	05	10	00	--	7,69
463	--	00	30	00	--	6,916	520	--	05	15	00	--	7,703
464	--	00	35	00	--	6,928	521	--	05	20	00	--	7,72
465	--	00	40	00	--	6,942	522	--	05	25	00	--	7,732
466	--	00	45	00	--	6,954	523	--	05	30	00	--	7,754

467	--	00	50	00	--	6,965	524	--	05	35	00	--	7,775
468	--	00	55	00	--	6,972	525	--	05	40	00	--	7,793
469	--	01	00	00	--	6,984	526	--	05	45	00	--	7,808
470	--	01	05	00	--	6,995	527	--	05	50	00	--	7,825
471	--	01	10	00	--	7,018	528	--	05	55	00	--	7,842
472	--	01	15	00	--	7,02	529	--	06	00	00	--	7,86
473	--	01	20	00	--	7,033	530	--	06	05	00	--	7,88
474	--	01	25	00	--	7,045	531	--	06	10	00	--	7,895
475	--	01	30	00	--	7,055	532	--	06	15	00	--	7,912
476	--	01	35	00	--	7,07	533	--	06	20	00	--	7,933
477	--	01	40	00	--	7,08	534	--	06	25	00	--	7,95
478	--	01	45	00	--	7,092	535	--	06	30	00	--	7,967
479	--	01	50	00	--	7,107	536	--	06	35	00	--	7,985
480	--	01	55	00	--	7,12	537	--	06	40	00	--	8,005
481	--	02	00	00	--	7,145	538	--	06	45	00	--	8,024
482	--	02	05	00	--	7,147	539	--	06	50	00	--	8,048
483	--	02	10	00	--	7,158	540	--	06	55	00	--	8,062
484	--	02	15	00	--	7,173	541	--	07	00	00	--	8,078
485	--	02	20	00	--	7,186	542	--	07	05	00	--	8,1
486	--	02	25	00	--	7,2	543	--	07	10	00	--	8,127
487	--	02	30	00	--	7,213	544	--	07	15	00	--	8,143
488	--	02	35	00	--	7,224	545	--	07	20	00	--	8,163
489	--	02	40	00	--	7,238	546	--	07	25	00	--	8,185
490	--	02	45	00	--	7,25	547	--	07	30	00	--	8,21
491	--	02	50	00	--	7,27	548	--	07	35	00	--	8,225
492	--	02	55	00	--	7,282	549	--	07	40	00	--	8,244
493	--	03	00	00	--	7,296	550	--	07	45	00	--	8,26
494	--	03	05	00	--	7,308	551	--	07	50	00	--	8,28
495	--	03	10	00	--	7,32	552	--	07	55	00	--	8,302
496	--	03	15	00	--	7,336	553	--	08	00	00	--	8,32
497	--	03	20	00	--	7,35	554	--	08	05	00	--	8,343
498	--	03	25	00	--	7,367	555	--	08	10	00	--	8,366
499	--	03	30	00	--	7,378	556	--	08	15	00	--	8,385
500	--	03	35	00	--	7,392	557	--	08	20	00	--	8,402
501	--	03	40	00	--	7,403	558	--	08	25	00	--	8,428
502	--	03	45	00	--	7,419	559	--	08	30	00	--	8,45
503	--	03	50	00	--	7,433	560	--	08	35	00	--	8,472
504	--	03	55	00	--	7,452	561	--	08	40	00	--	8,494
505	--	04	00	00	--	7,467	562	--	08	45	00	--	8,52
506	--	04	05	00	--	7,482	563	--	08	50	00	--	8,546
507	--	04	10	00	--	7,498	564	--	08	55	00	--	8,56

508	--	04	15	00	--	7,513	565	--	09	00	00	--	8,582
509	--	04	20	00	--	7,542	566	--	09	05	00	--	8,606
510	--	04	25	00	--	7,55	567	--	09	10	00	--	8,633
511	--	04	30	00	--	7,563	568	--	09	15	00	--	8,65
512	--	04	35	00	--	7,58	569	--	09	20	00	--	8,68
513	--	04	40	00	--	7,594	570	--	09	25	00	--	8,7
571	--	09	30	00	--	8,723	628	--	14	15	00	--	10,542
572	--	09	35	00	--	8,75	629	--	14	20	00	--	10,583
573	--	09	40	00	--	8,775	630	--	14	25	00	--	10,63
574	--	09	45	00	--	8,8	631	--	14	30	00		10,678
575	--	09	50	00	--	8,82	632	--	14	35	00		10,718
576	--	09	55	00	--	8,85	633	--	14	40	00		10,76
577	--	10	00	00	--	8,872	634	--	14	45	00		10,808
578	--	10	05	00	--	8,9	635	--	14	50	00		10,865
579	--	10	10	00	--	8,92	636	--	14	55	00		10,9
580	--	10	15	00	--	8,945	637	--	15	00	00		10,954
581	--	10	20	00	--	8,974	638	--	15	05	00		11
582	--	10	25	00	--	9,002	639	--	15	10	00		11,055
583	--	10	30	00	--	9,03	640	--	15	15	00		11,1
584	--	10	35	00	--	9,056	641	--	15	20	00		11,16
585	--	10	40	00	--	9,08	642	--	15	25	00		11,21
586	--	10	45	00	--	9,11	643	--	15	30	00		11,26
587	--	10	50	00	--	9,14	644	--	15	35	00		11,32
588	--	10	55	00	--	9,16	645	--	15	40	00		11,38
589	--	11	00	00	--	9,194	646	--	15	45	00		11,438
590	--	11	05	00	--	9,218	647	--	15	50	00		11,5
591	--	11	10	00	--	9,248	648	--	15	55	00		11,565
592	--	11	15	00	--	9,278	649	--	16	00	00		11,63
593	--	11	20	00	--	9,31	650	--	16	05	00		11,69
594	--	11	25	00	--	9,36	651	--	16	10	00		11,75
595	--	11	30	00	--	9,37	652	--	16	15	00		11,823
596	--	11	35	00	--	9,395	653	--	16	20	00		11,895
597	--	11	40	00	--	9,43	654	--	16	25	00		11,975
598	--	11	45	00	--	9,46	655	--	16	30	00		12,047
599	--	11	50	00	--	9,484	656	--	16	35	00		12,114
600	--	11	55	00	--	9,517	657	--	16	40	00		12,184
601	--	12	00	00	--	9,55	658	--	16	45	00		12,264
602	--	12	05	00	--	9,58	659	--	16	50	00		12,345
603	--	12	10	00	--	9,61	660	--	16	55	00		12,427
604	--	12	15	00	--	9,648	661	--	17	00	00		12,515
605	--	12	20	00	--	9,678	662	--	17	05	00		12,6

606	--	12	25	00	--	9,713	663	--	17	10	00		12,69
607	--	12	30	00	--	9,74	664	--	17	15	00		12,786
608	--	12	35	00	--	9,78	665	--	17	20	00		12,886
609	--	12	40	00	--	9,813	666	--	17	25	00		12,987
610	--	12	45	00	--	9,842	667	--	17	30	00		13,09
611	--	12	50	00	--	9,88	668	--	17	35	00		13,21
612	--	12	55	00	--	9,91	669	--	17	40	00		13,32
613	--	13	00	00	--	9,952	670	--	17	45	00		13,453
614	--	13	05	00	--	9,982	671	--	17	50	00		13,58
615	--	13	10	00	--	10,028	672	--	17	55	00		13,717
616	--	13	15	00	--	10,064	673	--	18	00	00		13,87
617	--	13	20	00	--	10,1	674	--	18	05	00		14,027
618	--	13	25	00	--	10,135	675	--	18	10	00		14,21
619	--	13	30	00	--	10,172	676	--	18	15	00		14,4
620	--	13	35	00	--	10,21	677	--	18	20	00	--	14,62
621	--	13	40	00	--	10,252	678	--	18	25	00	--	14,86
622	--	13	45	00	--	10,295	679	--	18	30	00	--	15,09
623	--	13	50	00	--	10,335	680	--	18	35	00	--	15,48
624	--	13	55	00	--	10,374	681	--	18	40	00	--	15,918
625	--	14	00	00	--	10,417	682	Fracture	18	45	00	--	16,637
626	--	14	05	00	--	10,456	683	--					
627	--	14	10	00	--	10,49	684	--					

Lampiran H Sertifikat Material

常州盛德无缝钢管有限公司 产品质量证明书
INSPECTION CERTIFICATE

SD-WF-JZ-24
江苏省常州市西郊邹区镇 邮编: 213144
Zouqū Town, West Suburbs of Changzhou City,
Jiangsu Province, China. Post Code: 213144.
Tel: 0519-883832158 Fax: 0519-83632723
http://www.shengdechina.com



合同号 C201603899

CONTACT 收货单位
PURCHASER 东方电气集团东方锅炉股份有限公司
产品名称 高压锅炉用无缝钢管

产品标准
PRODUCT STANDARD GB1898-2015-GB5310-2008

工艺性能
SUPPLIER OF BILLETS/ZHONGTIAN

制造方法
MANUFACTURE METHOD COLD DRAWN

生产许可证号
LICENSE NO. TS270020-2020

质保书编号
SHEET NO. 162649

序号	炉号 Heat No.	批号 Lot No.	规格 Size				重量 Weight	支数 Pieces	捆数 Bundles	工艺性能 Technological Properties			超声波 UT/5774.2	表面尺寸 Surface & Dimensions	非金属夹杂物 NON-METALLIC INCLUSIONS			硬度 Hardness	冲击功 Impact J	力学性能 Mechanical Properties			金相 Metallography									
			外径/mm Outer Diameter	壁厚/mm Wall Thickness	长度/mm Length	重量/kg Weight				扩口 Flaring	弯曲 Bending	水压 Hydro			拉伸强度 Yield Strength (MPa)	抗拉强度 Tensile Strength (MPa)	延伸率 Elongation (%)			布氏硬度 HB	夏比冲击 Charpy	屈服强度 Yield Strength (MPa)		抗拉强度 Tensile Strength (MPa)	断面收缩率 Reduction of Area (%)	晶粒度 Grain Size						
1	YN-168	0125-0200	38.1	4.75	1860±6	3822	90	2		合格 (OK)	合格 (OK)	合格 (OK)	合格 (OK)	合格 (OK)	合格 (OK)	0.5	1	0	1	0	0	1	0	1	0	0	1	0	0			
合计 Total			3822				90	2																								
序号	炉号 Heat No.	批号 Lot No.	化学成分(%) Chemical Composition										力学性能 Mechanical Properties			金相 Metallography																
			C	Si	Mn	P	S	Cr	Ni	Cu	Al	Mo	Ti	V	屈服强度 Yield Strength (MPa)		抗拉强度 Tensile Strength (MPa)	延伸率 Elongation (%)	布氏硬度 HB	冲击功 Impact J	晶粒度 Grain Size											
1	YN-168	IA	0.17	0.17	0.35	≤0.025	≤0.015	≤0.035	0.25	0.05	≤0.035	≤0.01	≤0.005	0.07	0.06	0.01	0.11				317	38.5		75.75	0.0	0.07	0.07	FP	FP	FP	4-10	
2		IB	0.19	0.20	0.51	≤0.025	≤0.015	≤0.035	0.05	0.06	0.05	0.10									330	38.0		75.75	0.0	0.00	0.00	FP	FP	FP	8.0-8.5	
3																																
4																																
注释		1. 酸洗表面已钝化。 THE BLIND ZONES FOR ET/OT HAVE BEEN ELIMINATED. 2. 交货状态: 正火 (NORMALIZATION): 900°C 保温 20 分钟。 3. 交货状态: 正火 (NORMALIZATION): 900°C 保温 20 分钟。 4. LA: 化学成分分析 (For chemical composition, LA stands for Ludde analysis, PA stands for product analysis) 5. 本钢管未经修焊和补焊 (NO REPAIRS BY WELDING, HAVE BEEN PERFORMED) 6. 材料管坯质保书 (THE BULLET CERTIFICATE IS APPLIED) (最高炉温度 460°C)																														
备注		本证明本报告产品, 均按标准与合同规定的测量和检验, 并符合标准和合同要求。 WE HEREBY CERTIFY THAT THE MATERIAL HEREIN DESCRIBED WAS MANUFACTURED, SAMPLED, TESTED IN ACCORDANCE WITH ABOVE STAND AND SPECIFICATION SATISFIED THE REQUIREMENTS.																														



质量保证书
MUST CERTIFY SEAL

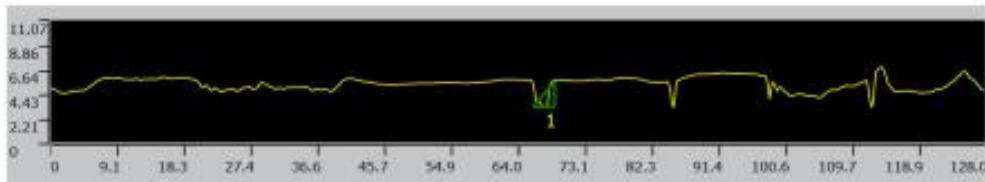
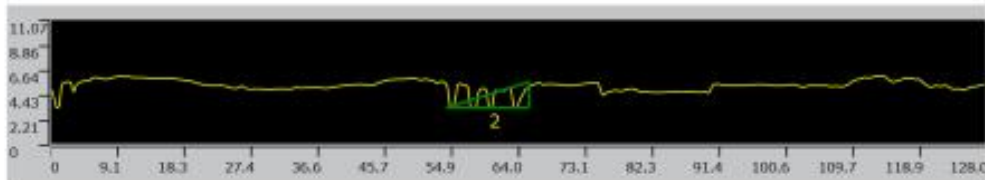
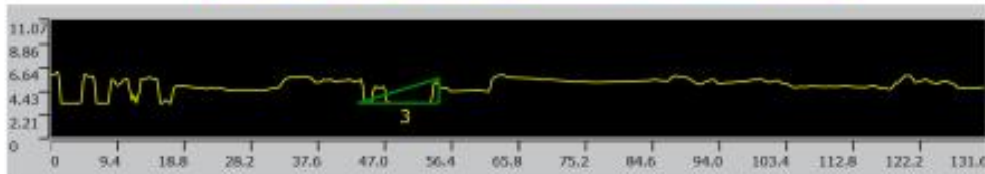
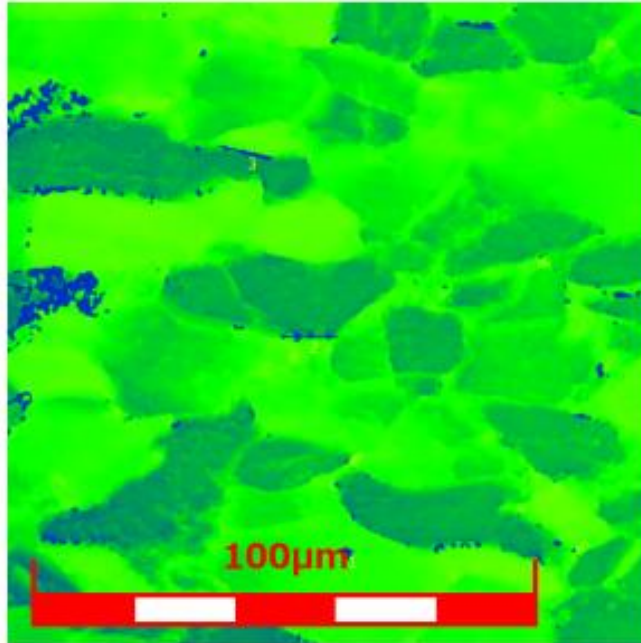
发货人 蒋雪英
ISSUED BY 蒋雪英 2016.9.23

收货人 范磊
RECEIVED BY 范磊 2016.9.23

发货日期
ISSUED DATE 2016年9月17日

Lampiran I Data Pengukuran Void Dan Micro Crack

LEXT



No.	Result	Width[µm]	Height[µm]	Length[µm]	Angle[°]	File name	
<input checked="" type="checkbox"/>	1		2.993	2.341	38.028	spec B(7) bag B2-1000x	
<input checked="" type="checkbox"/>	2		11.333	2.341	11.573	11.670	spec B(7) bag B2-1000x
<input checked="" type="checkbox"/>	3		11.483	2.341	11.719	11.522	spec B(7) bag B2-1000x

Lampiran J Dokumentasi Proses Pengambilan Data



