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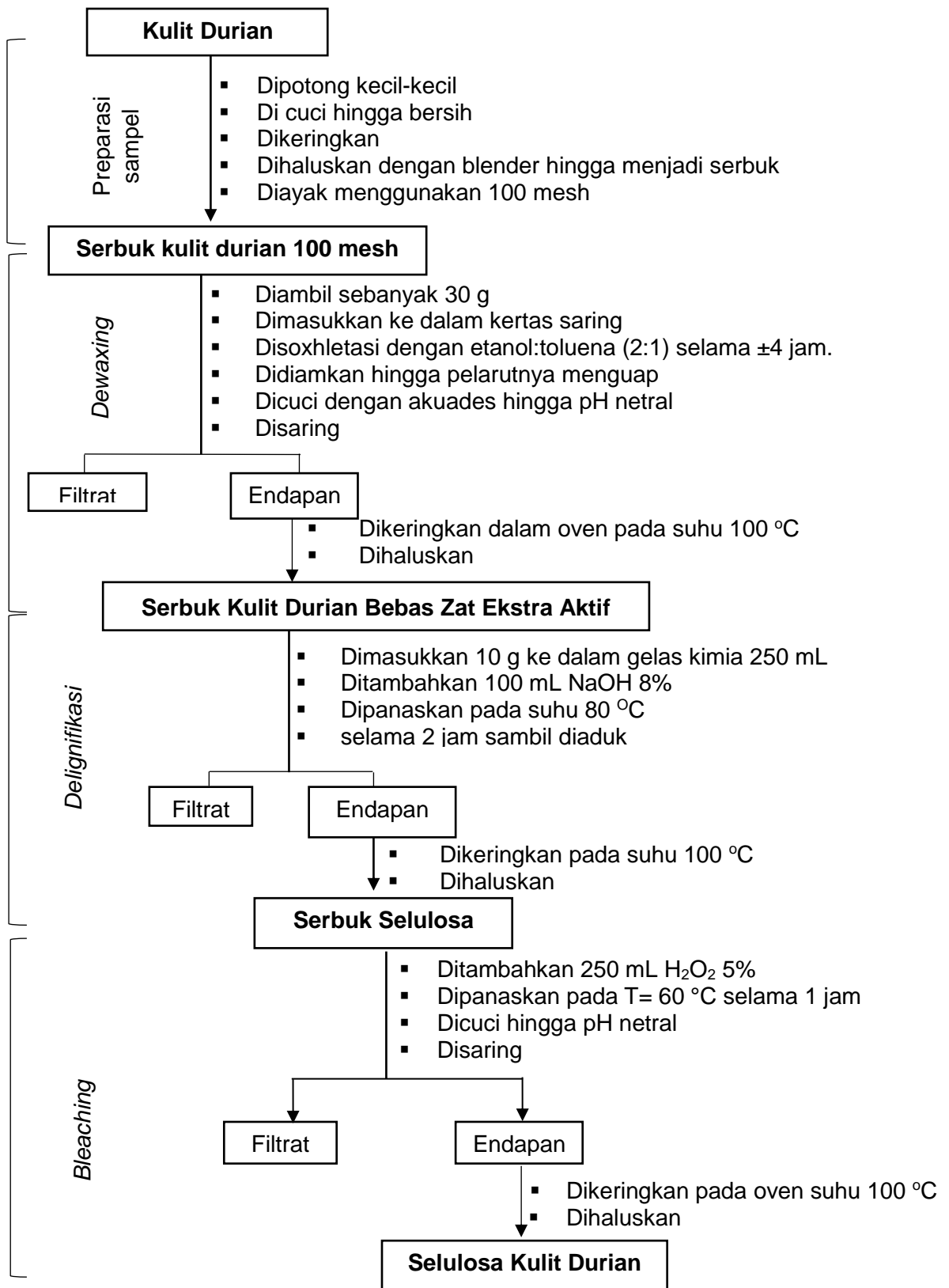
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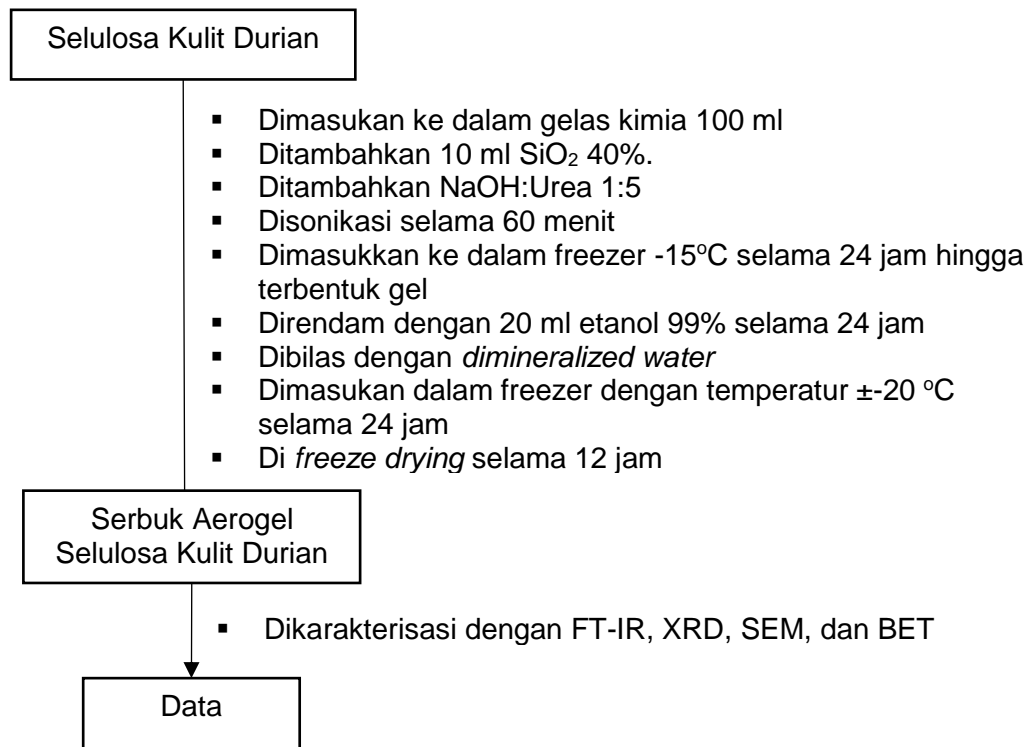
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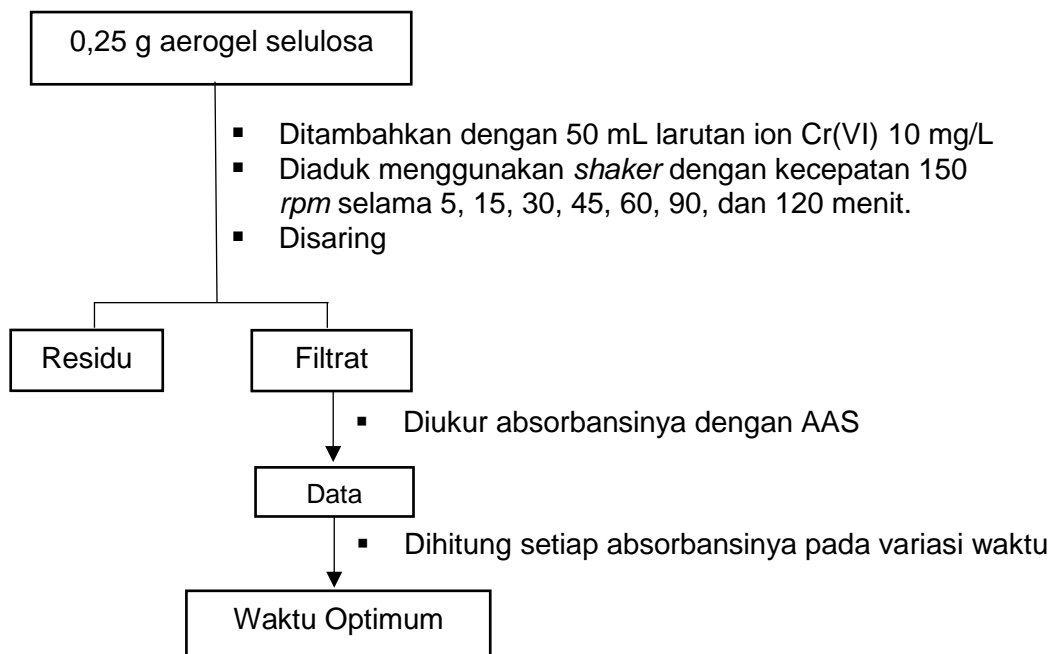
Lampiran 1. Skema Preparasi sampel, *Dewaxing*, *Delignifikasi*, dan *Bleaching*

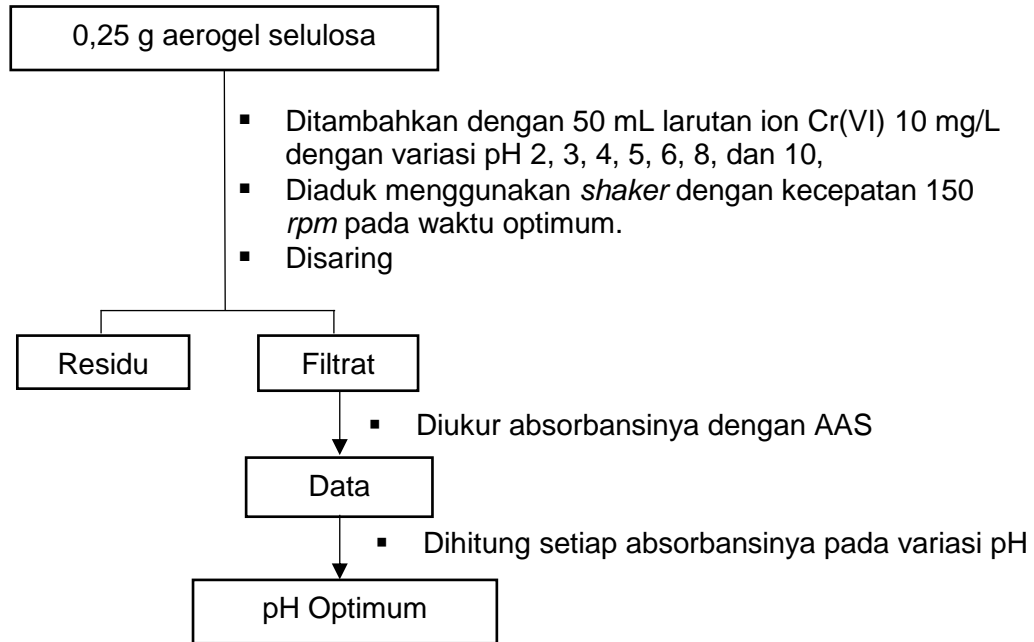
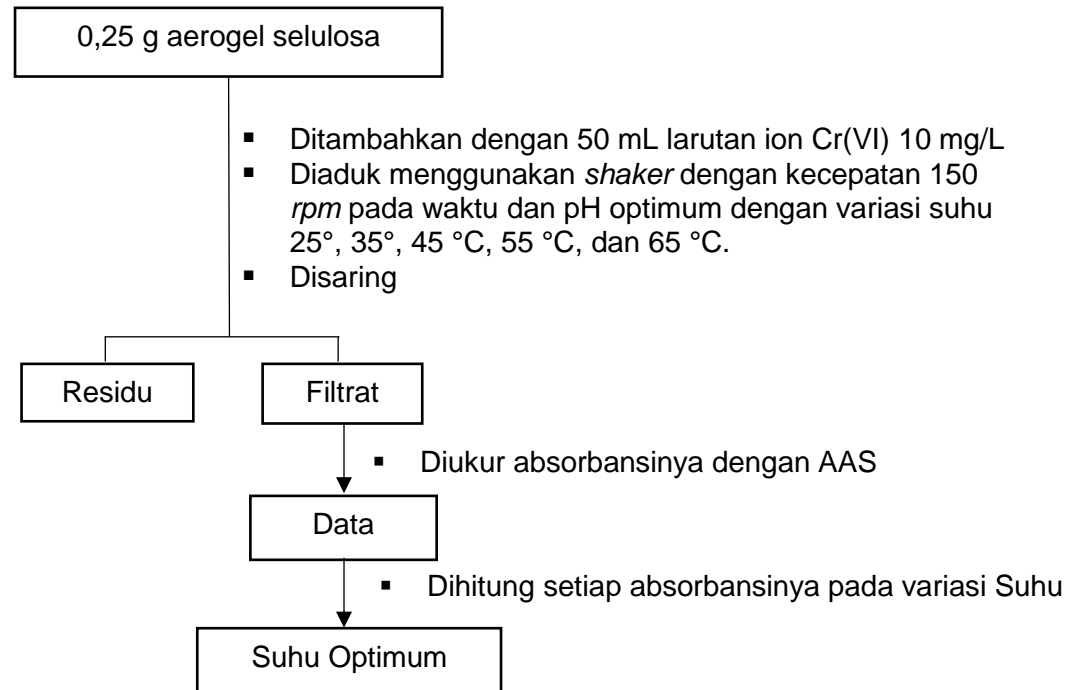


Lampiran 2. Skema Pembuatan Aerogel Selulosa

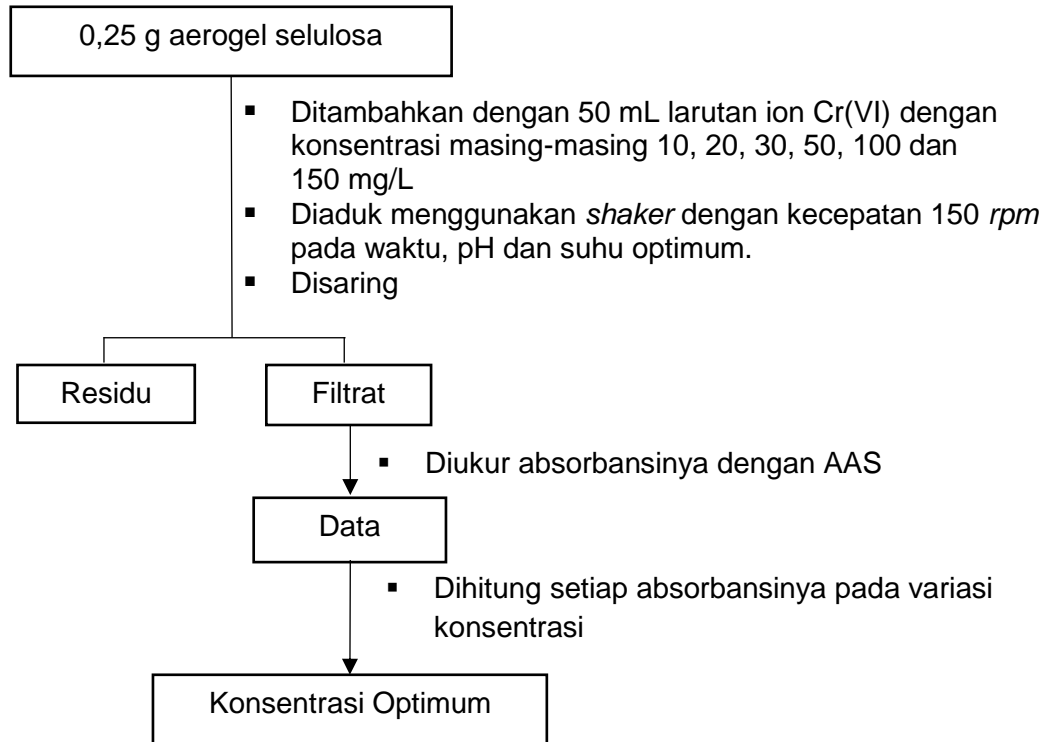


Lampiran 3. Penentuan Waktu Optimum pada Adsorpsi Ion Logam Cr(VI)



Lampiran 4. Penentuan pH Optimum pada Adsorpsi Ion Logam Cr(VI)**Lampiran 5. Penentuan Suhu Optimum pada Adsorpsi Ion Logam Cr(VI)**

Lampiran 6. Penentuan Konsentrasi Optimum pada Proses Adsorpsi Ion Logam Cr(VI)



Lampiran 7. Dokumentasi Penelitian

1. Proses Ekstraksi Selulosa dari Kulit Durian

a) Preparasi sampel



Kulit Durian



Proses pengeringan
Sampel



Serbuk Kulit Durian
setelah diblender

b) *Dewaxing*



Preparasi sampel untuk
di soxhlet



Proses Soxhlet



Sampel kulit durian
setelah di soxhlet

c) Delignifikasi



Proses delignifikasi
menggunakan NaOH
8%



Proses Pencucian dan
Penyaringan



Setelah dikeringkan
dalam oven

d) *Bleaching*

Proses *bleaching* menggunakan H_2O_2 5%



Proses Pencucian dan Penyaringan Selulosa



Selulosa Kulit Durian

2. Proses Sintesis Aerogel Selulosa



Campuran selulosa+NaOH+Urea+SiO₂



Proses Sonikasi selama 60 menit



Setelah proses sonikasi



Campuran *difreezer* pada suhu -15 °C selama 1x24 jam



Perendaman dengan etanol 99% selama 24 jam



Aerogel setelah dibilas dengan *demineralized water*



Setelah difreezer suhu ± 20 °C selama 24 jam



Aerogel selulosa di freeze drying



Aerogel Selulosa

3. Studi Adsorpsi



Larutan Cr(VI) 50 ppm



Proses penyaringan



Filtrat hasil penyaringan



Proses pengenceran



Larutan yang akan diukur absorbansinya menggunakan Spektrofotometer AAS

Lampiran 8. Perhitungan Rendemen (%) Selulosa Kulit Durian

Rendemen selulosa kulit durian dapat dihitung menggunakan persamaan berikut:

$$\text{Rendemen (\%)} = \frac{\text{Bobot ekstrak yang diperoleh (g)}}{\text{Bobot Sampel Awal}} \times 100\%$$

Maka, persentase rendemen selulosa pada proses ekstraksi dari kulit durian yaitu:

- *Dewaxing*

$$\begin{aligned} \text{Rendemen (\%)} &= \frac{22,755 \text{ g}}{30,117 \text{ g}} \times 100\% \\ &= 77,55 \% \end{aligned}$$

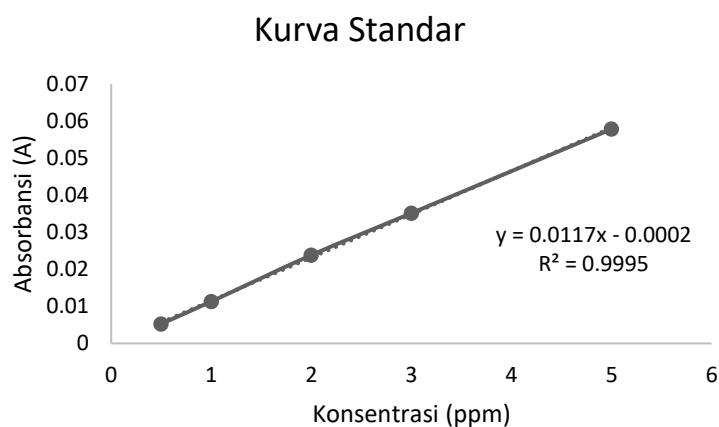
- *Delignifikasi*

$$\begin{aligned} \text{Rendemen (\%)} &= \frac{14,023 \text{ g}}{22,755 \text{ g}} \times 100\% \\ &= 61,63 \% \end{aligned}$$

- *Bleaching*

$$\begin{aligned} \text{Rendemen (\%)} &= \frac{12,250 \text{ g}}{14,023 \text{ g}} \times 100\% \\ &= 87,36 \% \end{aligned}$$

Lampiran 9. Kurva Kalibrasi Ion Logam Cr(VI)



Gambar 28. Kurva Kalibrasi Logam Cr(VI)

Lampiran 10. Data Pengaruh Waktu terhadap adsorpsi Ion Logam Cr(VI)

Berdasarkan persamaan garis linear pada kurva kalibrasi Cr(VI), maka nilai C_e dapat dihitung menggunakan persamaan $y = 0,0117x - 0,0002$.

Contohnya:

Untuk waktu kontak 5 menit dengan absorbansi 0,02145 dan faktor pengenceran (FP) 5 kali.

Diketahui:

$$\begin{aligned} t &= 5 \text{ menit} \\ y &= 0,02145 \\ C_0 &= 10,043 \text{ mg.L}^{-1} \\ m &= 0,2501 \text{ g} \\ V &= 0,05 \text{ L} \end{aligned}$$

Berdasarkan persamaan garis linear pada kurva standar, diperoleh:

$$\begin{aligned} y &= 0,0117x - 0,0002 \\ 0,0215 &= 0,0117x - 0,0002 \\ 0,0117x &= 0,0215 + 0,0002 \\ x &= 1,850 \text{ mg.L}^{-1} \end{aligned}$$

Sehingga,

$$\begin{aligned} C_e &= (\text{nilai } x) \times \text{Faktor Pengenceran} \\ &= 1,850 \times 5 \\ &= 9,252 \text{ mg.L}^{-1} \end{aligned}$$

Selanjutnya, jumlah ion logam Cr(VI) yang teradsorpsi untuk $t = 5$ menit dapat dihitung menggunakan persamaan:

$$\begin{aligned} q_t &= \frac{(C_0 - C_e)}{m} \times V \\ &= \frac{(10,043 - 9,252) \text{ mg.L}^{-1}}{0,2501 \text{ g}} \times 0,05 \text{ L} \\ &= 0,1581 \text{ mg.g}^{-1} \end{aligned}$$

Jadi, jumlah ion logam Cr(VI) yang teradsorpsi oleh aerogel selulosa pada waktu kontak 5 menit adalah sebesar $0,1518 \text{ mg.g}^{-1}$

Dengan menggunakan perhitungan yang sama, maka jumlah ion logam Cr(VI) yang teradsorpsi untuk setiap variasi waktu kontak dapat diketahui. Berikut data hasil perhitungan untuk penentuan waktu kontak optimum ion logam Cr(VI) dapat dilihat pada Tabel 10.

Tabel 10. Data penentuan waktu optimum ion logam Cr(VI) oleh Aerogel Selulosa

| t (m) | m (g) | C _o (mg.L ⁻¹) | C _e (mg.L ⁻¹) | V (L) | q _t (mg.g ⁻¹) |
|-------|--------|--------------------------------------|--------------------------------------|-------|--------------------------------------|
| 5 | 0,2501 | 10,043 | 9,252 | 0,05 | 0,158 |
| 15 | 0,2501 | 10,043 | 8,846 | 0,05 | 0,239 |
| 30 | 0,2501 | 10,043 | 8,675 | 0,05 | 0,273 |
| 45 | 0,2501 | 10,043 | 8,479 | 0,05 | 0,313 |
| 60 | 0,2502 | 10,043 | 8,543 | 0,05 | 0,300 |
| 90 | 0,2501 | 10,043 | 8,530 | 0,05 | 0,302 |
| 120 | 0,2502 | 10,043 | 8,551 | 0,05 | 0,298 |

Lampiran 11. Data Pengaruh pH terhadap adsorpsi Ion Logam Cr(VI) (t = 45 menit)

Rumus Perhitungan jumlah ion logam Cr(VI) yang teradsorpsi:

$$q_t = \frac{(C_0 - C_e)}{m} \times V$$

Tabel 11. Data penentuan pH optimum Ion Logam Cr(VI) oleh Aerogel Selulosa

| pH | m (g) | C _o (mg.L ⁻¹) | C _e (mg.L ⁻¹) | V (L) | q _t (mg.g ⁻¹) |
|----|--------|--------------------------------------|--------------------------------------|-------|--------------------------------------|
| 2 | 0,2501 | 9,915 | 7,607 | 0,05 | 0,4614 |
| 3 | 0,2501 | 10,043 | 8,333 | 0,05 | 0,3417 |
| 4 | 0,2501 | 7,350 | 5,940 | 0,05 | 0,2819 |
| 5 | 0,2501 | 9,231 | 8,547 | 0,05 | 0,1367 |
| 6 | 0,2501 | 6,752 | 6,453 | 0,05 | 0,0598 |
| 8 | 0,2501 | 5,940 | 5,769 | 0,05 | 0,0342 |
| 10 | 0,2501 | 6,175 | 6,047 | 0,05 | 0,0256 |

Lampiran 12. Data Pengaruh suhu terhadap adsorpsi Ion Logam Cr(VI) (t = 45 menit, pH = 2)

Rumus Perhitungan jumlah ion logam Cr(VI) yang teradsorpsi:

$$q_t = \frac{(C_0 - C_e)}{m} \times V$$

Tabel 12. Data penentuan Suhu optimum Ion Logam Cr(VI) oleh Aerogel Selulosa

| Suhu (°C) | m (g) | C _o (mg.L ⁻¹) | C _e (mg.L ⁻¹) | V (L) | q _t (mg.g ⁻¹) |
|-----------|--------|--------------------------------------|--------------------------------------|-------|--------------------------------------|
| 25 | 0,2501 | 10,171 | 8,974 | 0,05 | 0,239 |
| 35 | 0,2501 | 9,915 | 8,162 | 0,05 | 0,350 |
| 45 | 0,2501 | 10,556 | 8,162 | 0,05 | 0,478 |
| 55 | 0,2501 | 10,769 | 8,462 | 0,05 | 0,461 |
| 65 | 0,2501 | 10,513 | 8,590 | 0,05 | 0,384 |

Lampiran 13. Data Pengaruh Konsentrasi terhadap adsorpsi Ion Logam Cr(VI) (t = 45 menit, pH = 2, T = 45 °C)

Rumus Perhitungan jumlah ion logam Cr(VI) yang teradsorpsi:

$$q_t = \frac{(C_0 - C_e)}{m} \times V$$

Tabel 13. Data penentuan Konsentrasi optimum Ion Cr(VI) oleh Aerogel Selulosa

| Konsentrasi (mg.L ⁻¹) | m (g) | C _o (mg.L ⁻¹) | C _e (mg.L ⁻¹) | V (L) | q _t (mg.g ⁻¹) |
|-----------------------------------|--------|--------------------------------------|--------------------------------------|-------|--------------------------------------|
| 10 | 0,2501 | 9,957 | 7,564 | 0,05 | 0,478 |
| 20 | 0,2501 | 19,231 | 14,701 | 0,05 | 0,906 |
| 30 | 0,2501 | 23,248 | 17,863 | 0,05 | 1,077 |
| 50 | 0,2501 | 50,427 | 39,744 | 0,05 | 2,137 |
| 100 | 0,2501 | 89,103 | 72,650 | 0,05 | 3,291 |
| 150 | 0,2501 | 148,718 | 125,427 | 0,05 | 4,658 |

Lampiran 14. Studi Model Kinetika Adsorpsi Ion Logam Cr(VI)

Kinetika orde satu semu dapat dihitung menggunakan persamaan berikut:

$$\ln (q_e - q_t) = -k_1 t + \ln q_e$$

Tabel 14. Data Studi Kinetika Adsorpsi Ion Logam Cr(VI) oleh Aerogel Selulosa

| t (m) | q _e (mg.g ⁻¹) | q _t (mg.g ⁻¹) | q _e -q _t | ln (q _e -q _t) | t/q _t |
|-------|--------------------------------------|--------------------------------------|--------------------------------|--------------------------------------|------------------|
| 5 | 0,3127 | 0,1581 | 0,155 | -1,867 | 31,634 |
| 15 | 0,3127 | 0,2392 | 0,073 | -2,611 | 62,703 |
| 30 | 0,3127 | 0,2734 | 0,039 | -3,237 | 109,731 |
| 45 | 0,3127 | 0,3127 | 0,000 | 0,000 | 143,910 |
| 60 | 0,3127 | 0,2998 | 0,013 | -4,348 | 200,159 |
| 90 | 0,3127 | 0,3024 | 0,010 | -4,580 | 297,576 |
| 120 | 0,3127 | 0,2981 | 0,015 | -4,224 | 402,613 |

Jika di Plot $\ln (q_e - q_t)$ terhadap t, maka *slope* adalah -k dan Intersep adalah $\ln q_e$, sehingga diperoleh persamaan garis lurus:

$$y = -0,0232x - 1,7716$$

Dari persamaan garis diatas, maka diperoleh nilai slope (a) = -0,0232 dan nilai intersep (b) = 1,7716, sehingga nilai k_1 dapat dihitung sebagai berikut:

$$\text{Slope} = -k$$

$$\begin{aligned} k_1 &= -\text{slope} \\ &= -(-0,0232) \\ &= 0,0232 \text{ menit}^{-1} \end{aligned}$$

Nilai adsorpsi dapat dihitung sebagai berikut :

$$\text{Intersep} = \ln q_e$$

$$\begin{aligned} q_e &= e^{\text{intersep}} \\ &= e^{3,0888} \\ &= 0,1701 \text{ mg.g}^{-1} \end{aligned}$$

$$k_1 = 0,0232 \text{ menit}^{-1}$$

$$R^2 = 0,3379$$

Rumus kinetika orde dua semu dapat dihitung menggunakan persamaan berikut:

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} t$$

Jika di Plot t/q_t terhadap t (waktu), maka slope adalah $1/q_e$ dan Intersep adalah $1/k_2 q_e^2$, sehingga diperoleh persamaan garis lurus:

Dari grafik kinetika orde dua semu diperoleh persamaan garis

$$y = 3,2101x + 10,05$$

dari persamaan garis diperoleh nilai slope (a) = 3,2101 dan intercept (b) = 10,05 nilai k_2 diperoleh sebagai berikut:

$$\text{slope} = \frac{1}{q_e}$$

$$\begin{aligned} q_e &= \frac{1}{\text{slope}} \\ &= \frac{1}{3,2101} \\ &= 0,3115 \text{ mg.g}^{-1} \end{aligned}$$

$$\text{Intercept} = \frac{1}{k_2 q_e^2}$$

$$\begin{aligned}
 k_2 &= \frac{1}{q_e^2 \cdot \text{intercept}} \\
 &= \frac{1}{(0,3115)^2 \times 10,05} \\
 &= 0,2932 \text{ g.mg}^{-1}\text{menit}^{-1}
 \end{aligned}$$

$$k_2 = 0,2932 \text{ g.mg}^{-1}\text{menit}^{-1}$$

$$R^2 = 0,9978$$

Lampiran 15. Penentuan Kapasitas dan Isothermal Adsorpsi Ion Logam Cr(VI)

- Persamaan adsorpsi Isothermal Langmuir:

$$\frac{C_e}{q_e} = \frac{1}{Q_0 b} + \frac{C_e}{Q_0}$$

Tabel 15. Data Isothermal Langmuir terhadap adsorpsi ion logam Cr(VI) oleh aerogel selulosa

| Co (mg.L ⁻¹) | Ce (mg.L ⁻¹) | q _e (mg.g ⁻¹) | Ce/q _e |
|--------------------------|--------------------------|--------------------------------------|-------------------|
| 10 | 9,957 | 0,478 | 15,810 |
| 20 | 19,231 | 0,906 | 16,226 |
| 30 | 23,248 | 1,077 | 16,587 |
| 50 | 50,427 | 2,137 | 18,600 |
| 100 | 89,103 | 3,291 | 22,078 |
| 150 | 148,718 | 4,658 | 26,927 |

Jika di plot Ce/q_e terhadap Ce, maka slope adalah 1/Q₀ dan Intersep adalah 1/Q₀b, sehingga diperoleh persamaan garis lurus:

Berdasarkan model Isothermal Langmuir diperoleh persamaan garis

$$y = 0,0961x + 14,918$$

dari persamaan garis diperoleh nilai slope (a) = 0,0961 dan intercept (b) = 14,918

$$\frac{1}{Q_0} = \text{slope}$$

$$Q_0 = \frac{1}{\text{slope}}$$

$$= \frac{1}{0,0961}$$

$$= 10,4058 \text{ mg.g}^{-1}$$

Intensitas adsorpsi dapat dihitung sebagai berikut :

$$\frac{1}{Q_{0,b}} = \text{intercept}$$

$$b = \frac{1}{Q_0 \cdot \text{intercept}}$$

$$= \frac{1}{10,4058 \times 14,918}$$

$$= 0,0064 \text{ L} \cdot \text{mg}^{-1}$$

Tabel 16. Data Isotermal Freundlich terhadap adsorpsi ion logam Cr(VI) oleh aerogel selulosa

| Co (mg.L ⁻¹) | Ce (mg.L ⁻¹) | q _e (mg.g ⁻¹) | Log Ce | Log q _e |
|--------------------------|--------------------------|--------------------------------------|--------|--------------------|
| 10 | 9,957 | 0,478 | 0,879 | -0,320 |
| 20 | 19,231 | 0,906 | 1,167 | -0,043 |
| 30 | 23,248 | 1,077 | 1,252 | 0,032 |
| 50 | 50,427 | 2,137 | 1,599 | 0,330 |
| 100 | 89,103 | 3,291 | 1,861 | 0,517 |
| 150 | 148,718 | 4,658 | 2,098 | 0,668 |

Contoh perhitungan nilai parameter isotermal Freundlich sebagai berikut:

Persamaan adsorpsi isothermal Freundlich yaitu:

$$\text{Log } q_e = \text{Log } k + \frac{1}{n} \text{Log } C_e$$

Jika di Plot log q_e terhadap Log C_e, maka slope adalah 1/n dan Intersep adalah Log k, sehingga diperoleh persamaan garis lurus:

$$y = 0,8098x - 0,9981$$

dari persamaan garis tersebut diperoleh nilai slope (a) = 0,8098 dan nilai intersep (b) = 0,9981

Nilai kapasitas adsorpsi dapat dihitung sebagai berikut:

$$\log k_f = \text{intercept}$$

$$k_f = \text{invers log intercept}$$

$$= \text{invers log } 0,9981$$

$$k_f = 9,956 \text{ mg/g}$$

Intensitas adsorpsi dapat dihitung sebagai berikut

$$\frac{1}{n} = \text{slope}$$

$$n = \frac{1}{\text{slope}}$$

$$= \frac{1}{0,8098 \text{ L/g}}$$

$$= 1,2349 \text{ g/L}$$

Lampiran 16. Penentuan Termodinamika Adsorpsi Ion Logam Cr(VI)

Parameter termodinamika adsorpsi terdiri dari perubahan entalpi (ΔH°), perubahan entropi (ΔS°), dan perubahan energi bebas Gibbs (ΔG°) yang masing-masing dapat dihitung menggunakan persamaan di bawah ini:

$$\ln K_c = -\frac{\Delta S^\circ}{R} - \frac{\Delta H^\circ}{RT}$$

$$K_c = \frac{q_e}{C_e}$$

$$\Delta G^\circ = \Delta H^\circ - T\Delta S^\circ$$

Tabel 17. Data Parameter Termodinamika (ΔG° , ΔH° , dan ΔS°)

| T (K) | 1/T | qe/ce | ln K _c | ΔG° | ΔH° | ΔS° |
|-------|---------|--------|-------------------|------------------|------------------|------------------|
| 298 | 0,00336 | 0,0267 | -3,62474 | -2699,74 | | |
| 308 | 0,00325 | 0,0508 | -2,98005 | -2790,71 | | |
| 318 | 0,00314 | 0,0699 | -2,66044 | -2881,68 | +11,133 | +9,097 |
| 328 | 0,00305 | 0,0584 | -2,83979 | -2972,65 | | |
| 338 | 0,00296 | 0,0485 | -3,0269 | -3063,62 | | |

Dari grafik plot antara 1/T terhadap ln K_c, diperoleh persamaan garis y = -1339x + 1,0941. Maka slope (a) = -1339 dan nilai intersep (b) = 1,0941

Sehingga, nilai ΔH dapat dihitung:

$$\frac{\Delta H^\circ}{R} = \text{slope}$$

$$\frac{\Delta H^\circ}{8,3145} = -(-1339)$$

$$\Delta H^\circ = 11,133$$

Nilai ΔS diperoleh dari:

$$\frac{\Delta S^{\circ}}{R} = \text{intercept}$$

$$\frac{\Delta S^{\circ}}{8,3145} = 1,0941$$

$$\Delta S^{\circ} = 9,097$$

Penentuan jumlah energi Gibbs (ΔG°) menggunakan persamaan:

$$\Delta G^{\circ} = \Delta H^{\circ} - T\Delta S^{\circ}$$

Untuk $T = 298 \text{ K}$

$$\begin{aligned}\Delta G^{\circ} &= \Delta H^{\circ} - T\Delta S^{\circ} \\ &= 11,133 - (298 \text{ K} \times 9,097) \\ &= -2699,77 \text{ J} \\ &= -2,6997 \text{ kJ}\end{aligned}$$

Untuk $T = 328 \text{ K}$

$$\begin{aligned}\Delta G^{\circ} &= \Delta H^{\circ} - T\Delta S^{\circ} \\ &= 11,133 - (328 \text{ K} \times 9,097) \\ &= -2972,6 \text{ J} \\ &= -2,9726 \text{ kJ}\end{aligned}$$

Untuk $T = 308 \text{ K}$

$$\begin{aligned}\Delta G^{\circ} &= \Delta H^{\circ} - T\Delta S^{\circ} \\ &= 11,133 - (308 \text{ K} \times 9,097) \\ &= -2790,7 \text{ J} \\ &= -2,7907 \text{ kJ}\end{aligned}$$

Untuk $T = 338 \text{ K}$

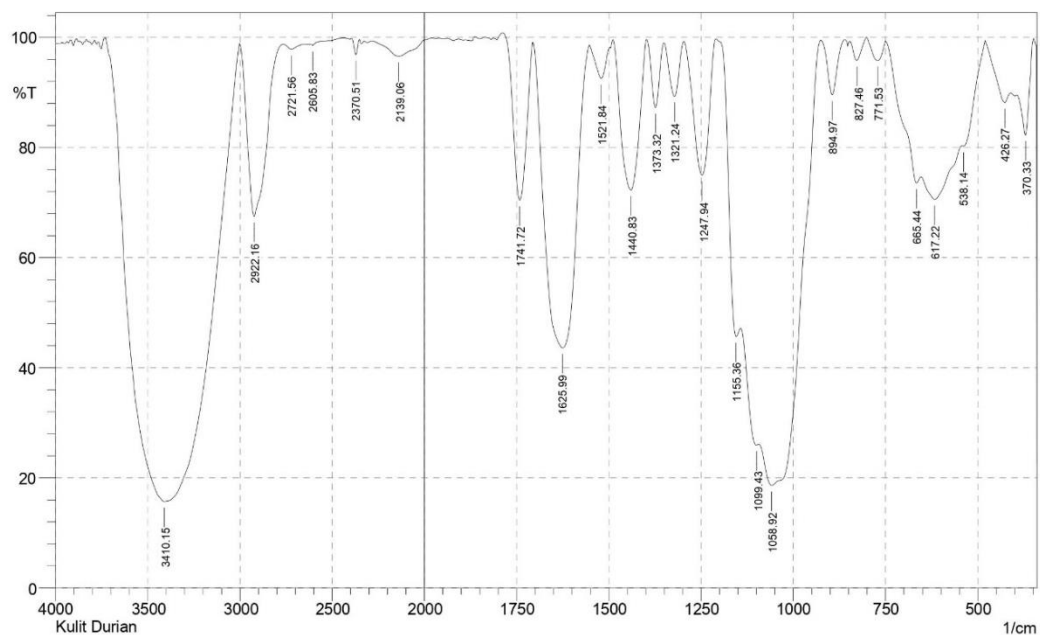
$$\begin{aligned}\Delta G^{\circ} &= \Delta H^{\circ} - T\Delta S^{\circ} \\ &= 11,133 - (338 \text{ K} \times 9,097) \\ &= -3063,6 \text{ J} \\ &= -3,0636 \text{ kJ}\end{aligned}$$

Untuk $T = 318 \text{ K}$

$$\begin{aligned}\Delta G^{\circ} &= \Delta H^{\circ} - T\Delta S^{\circ} \\ &= 11,133 - (318 \text{ K} \times 9,097) \\ &= -2,8816 \text{ J} \\ &= -2,8816 \text{ kJ}\end{aligned}$$

Lampiran 17. Hasil Analisis FTIR

SHIMADZU



| | Peak | Intensity | Corr. Intensity | Base (H) | Base (L) | Area | Corr. Area |
|----|---------|-----------|-----------------|----------|----------|---------|------------|
| 1 | 370.33 | 82.281 | 12.599 | 393.48 | 349.12 | 2.324 | 1.283 |
| 2 | 426.27 | 88.167 | 3.833 | 478.35 | 410.84 | 2.411 | 0.677 |
| 3 | 538.14 | 80.266 | 1.237 | 542 | 480.28 | 3.203 | 0.309 |
| 4 | 617.22 | 70.573 | 5.86 | 651.94 | 543.93 | 14.097 | 2.108 |
| 5 | 665.44 | 73.564 | 4.103 | 748.38 | 653.87 | 7.098 | 0.853 |
| 6 | 771.53 | 95.801 | 3.841 | 800.46 | 750.31 | 0.586 | 0.519 |
| 7 | 827.46 | 95.832 | 3.766 | 846.75 | 800.46 | 0.457 | 0.388 |
| 8 | 894.97 | 89.568 | 9.942 | 923.9 | 862.18 | 1.351 | 1.221 |
| 9 | 1058.92 | 18.655 | 22.64 | 1093.64 | 925.83 | 75.6 | 27.321 |
| 10 | 1099.43 | 25.972 | 1.868 | 1141.86 | 1095.57 | 22.241 | 1.089 |
| 11 | 1155.36 | 45.696 | 10.761 | 1209.37 | 1143.79 | 10.425 | 1.376 |
| 12 | 1247.94 | 75.002 | 24.498 | 1296.16 | 1211.3 | 5.604 | 5.411 |
| 13 | 1321.24 | 89.296 | 9.802 | 1350.17 | 1298.09 | 1.458 | 1.251 |
| 14 | 1373.32 | 87.246 | 12.024 | 1398.39 | 1352.1 | 1.396 | 1.251 |
| 15 | 1440.83 | 72.288 | 27.109 | 1487.12 | 1400.32 | 7.358 | 7.13 |
| 16 | 1521.84 | 92.565 | 5.682 | 1550.77 | 1498.69 | 1.116 | 0.719 |
| 17 | 1625.99 | 43.624 | 55.209 | 1705.07 | 1552.7 | 30.939 | 30.166 |
| 18 | 1741.72 | 70.448 | 29.392 | 1786.08 | 1707 | 5.689 | 5.663 |
| 19 | 2139.06 | 96.578 | 3.001 | 2279.86 | 1980.89 | 2.595 | 2.069 |
| 20 | 2370.51 | 96.904 | 2.784 | 2395.59 | 2353.16 | 0.296 | 0.242 |
| 21 | 2605.83 | 98.553 | 0.348 | 2625.12 | 2524.82 | 0.397 | 0 |
| 22 | 2721.56 | 97.828 | 0.923 | 2763.99 | 2654.05 | 0.806 | 0.204 |
| 23 | 2922.16 | 67.52 | 31.231 | 3001.24 | 2765.92 | 18.775 | 17.491 |
| 24 | 3410.15 | 15.715 | 83.759 | 3730.33 | 3003.17 | 314.645 | 312.752 |

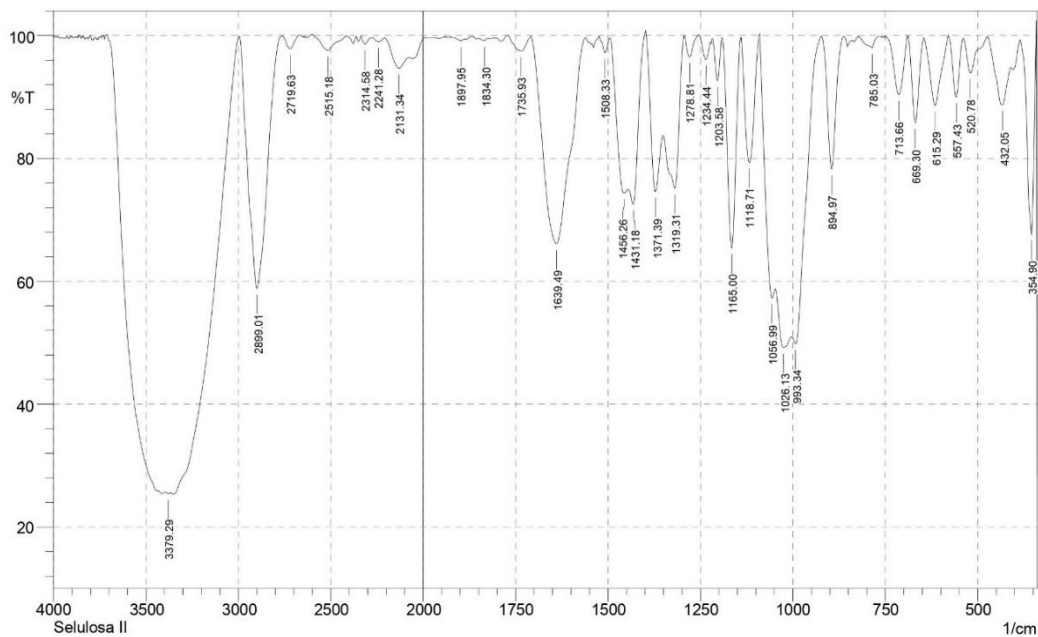
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Resolution;

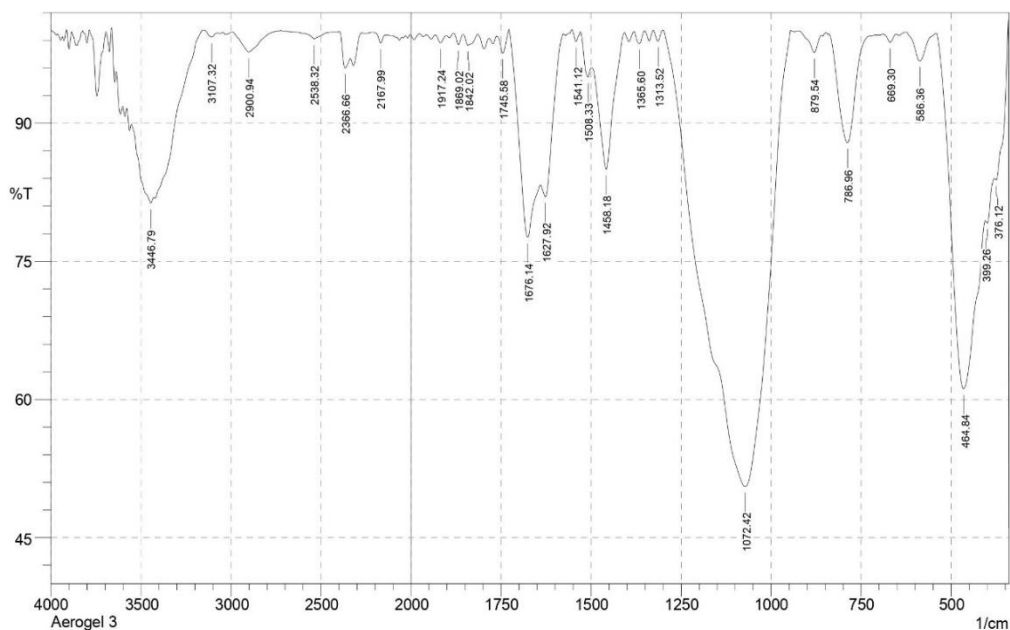
Apodization;



| No. | Peak | Intensity | Corr. Intensity | Base (H) | Base (L) | Area | Corr. Area |
|-----|---------|-----------|-----------------|----------|----------|--------|------------|
| 1 | 354.9 | 67.686 | 30.074 | 383.83 | 343.33 | 3.254 | 2.913 |
| 2 | 432.05 | 88.727 | 7.796 | 472.56 | 410.84 | 1.961 | 1.198 |
| 3 | 520.78 | 93.931 | 5.683 | 540.07 | 474.49 | 0.805 | 0.711 |
| 4 | 557.43 | 90.009 | 9.742 | 580.57 | 540.07 | 0.884 | 0.846 |
| 5 | 615.29 | 88.625 | 11.051 | 644.22 | 580.57 | 1.726 | 1.648 |
| 6 | 669.3 | 85.82 | 13.963 | 688.59 | 646.15 | 1.366 | 1.322 |
| 7 | 713.66 | 90.389 | 9.483 | 750.31 | 690.52 | 1.243 | 1.207 |
| 8 | 785.03 | 97.941 | 1.9 | 823.6 | 767.67 | 0.257 | 0.217 |
| 9 | 894.97 | 78.256 | 21.618 | 921.97 | 864.11 | 2.54 | 2.508 |
| 10 | 993.34 | 49.813 | 7.079 | 1002.98 | 923.9 | 10.915 | 0.959 |
| 11 | 1026.13 | 49.219 | 5.635 | 1047.35 | 1004.91 | 12.228 | 1.056 |
| 12 | 1056.99 | 57.274 | 9.275 | 1089.78 | 1049.28 | 6.428 | 1.529 |
| 13 | 1118.71 | 79.329 | 20.428 | 1139.93 | 1091.71 | 2.705 | 2.659 |
| 14 | 1165 | 65.446 | 34.153 | 1190.08 | 1141.86 | 4.39 | 4.305 |
| 15 | 1203.58 | 92.641 | 6.934 | 1217.08 | 1192.01 | 0.459 | 0.412 |
| 16 | 1234.44 | 96.097 | 3.25 | 1255.66 | 1222.87 | 0.312 | 0.245 |
| 17 | 1278.81 | 96.521 | 3.539 | 1294.24 | 1255.66 | 0.269 | 0.282 |
| 18 | 1319.31 | 75.152 | 17.547 | 1350.17 | 1294.24 | 4.694 | 2.61 |
| 19 | 1371.39 | 74.589 | 16.24 | 1398.39 | 1352.1 | 3.793 | 2.008 |
| 20 | 1431.18 | 72.556 | 10.139 | 1444.68 | 1400.32 | 3.552 | 0.986 |
| 21 | 1456.26 | 74.399 | 5.515 | 1494.83 | 1446.61 | 4.036 | 0.898 |
| 22 | 1508.33 | 97.207 | 2.51 | 1523.76 | 1494.83 | 0.195 | 0.16 |
| 23 | 1639.49 | 66.063 | 33.691 | 1707 | 1562.34 | 13.455 | 13.293 |
| 24 | 1735.93 | 97.496 | 0.139 | 1772.58 | 1734.01 | 0.252 | 0.042 |
| 25 | 1834.3 | 99.145 | 0.384 | 1851.66 | 1826.59 | 0.07 | 0.019 |
| 26 | 1897.95 | 99.112 | 0.416 | 1926.89 | 1886.38 | 0.096 | 0.026 |
| 27 | 2131.34 | 94.675 | 3.075 | 2208.49 | 2079.26 | 2.04 | 0.922 |
| 28 | 2241.28 | 99.014 | 0.678 | 2279.86 | 2208.49 | 0.217 | 0.122 |
| 29 | 2314.58 | 98.63 | 1.208 | 2337.72 | 2279.86 | 0.205 | 0.158 |
| 30 | 2515.18 | 97.556 | 2.515 | 2600.04 | 2416.81 | 0.919 | 0.969 |
| 31 | 2719.63 | 97.876 | 2.123 | 2762.06 | 2669.48 | 0.428 | 0.431 |
| 32 | 2899.01 | 58.825 | 41.047 | 2993.52 | 2763.99 | 23.94 | 23.818 |
| 33 | 3379.29 | 25.416 | 0.206 | 3394.72 | 3367.71 | 16.015 | 0.048 |

Date/Time; 12/29/2021 2:24:54 PM

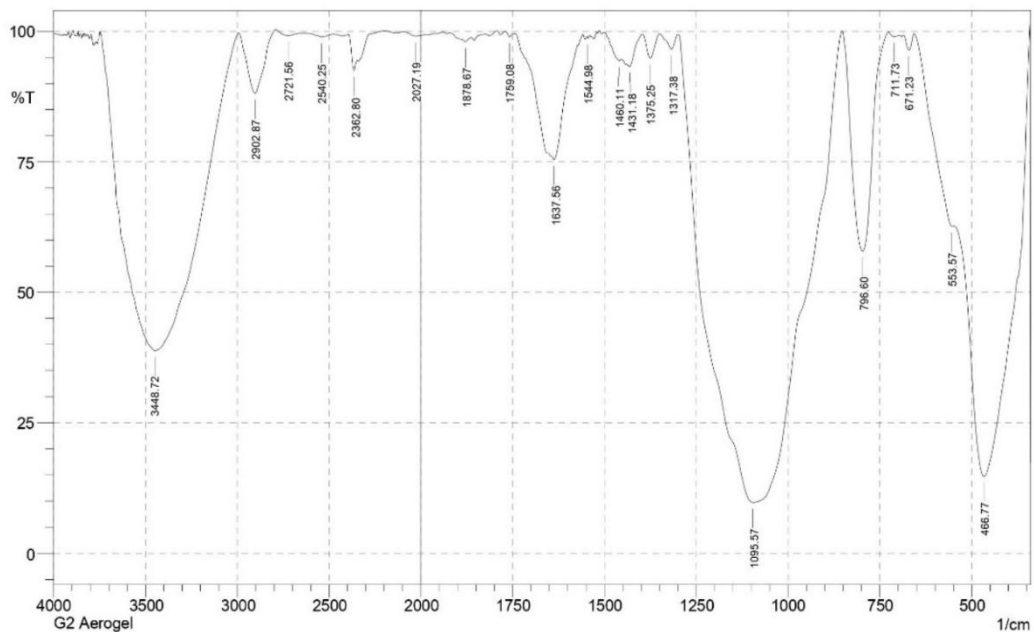
No. of Scans;



| No. | Peak | Intensity | Corr. Intensity | Base (H) | Base (L) | Area | Corr. Area |
|-----|---------|-----------|-----------------|----------|----------|--------|------------|
| 1 | 376.12 | 83.82 | 0.979 | 378.05 | 343.33 | 1.815 | 0.5 |
| 2 | 399.26 | 79.162 | 0.97 | 403.12 | 379.98 | 2.029 | 0.042 |
| 3 | 464.84 | 61.163 | 27.266 | 540.07 | 405.05 | 17.403 | 10.482 |
| 4 | 586.36 | 96.766 | 3.078 | 624.94 | 540.07 | 0.538 | 0.478 |
| 5 | 669.3 | 98.774 | 0.901 | 688.59 | 651.94 | 0.115 | 0.064 |
| 6 | 786.96 | 87.899 | 11.688 | 839.03 | 725.23 | 2.902 | 2.693 |
| 7 | 879.54 | 97.667 | 2.017 | 923.9 | 860.25 | 0.292 | 0.232 |
| 8 | 1072.42 | 50.558 | 49.479 | 1300.02 | 947.05 | 53.336 | 53.422 |
| 9 | 1313.52 | 98.904 | 1.209 | 1327.03 | 1300.02 | 0.055 | 0.069 |
| 10 | 1365.6 | 98.644 | 1.36 | 1381.03 | 1352.1 | 0.096 | 0.096 |
| 11 | 1458.18 | 84.994 | 12.698 | 1498.69 | 1408.04 | 3.245 | 2.417 |
| 12 | 1508.33 | 95.003 | 2.214 | 1529.55 | 1498.69 | 0.459 | 0.179 |
| 13 | 1541.12 | 98.844 | 1.2 | 1552.7 | 1529.55 | 0.056 | 0.061 |
| 14 | 1627.92 | 82.017 | 4.323 | 1639.49 | 1577.77 | 2.904 | 0.555 |
| 15 | 1676.14 | 77.622 | 12.472 | 1726.29 | 1641.42 | 6.008 | 2.548 |
| 16 | 1745.58 | 97.618 | 2.191 | 1762.94 | 1728.22 | 0.192 | 0.163 |
| 17 | 1842.02 | 98.46 | 1.197 | 1855.52 | 1815.02 | 0.185 | 0.125 |
| 18 | 1869.02 | 98.52 | 1.188 | 1882.52 | 1855.52 | 0.095 | 0.061 |
| 19 | 1917.24 | 98.735 | 0.812 | 1932.67 | 1901.81 | 0.112 | 0.052 |
| 20 | 2167.99 | 98.694 | 0.99 | 2214.28 | 2140.99 | 0.191 | 0.103 |
| 21 | 2366.66 | 95.985 | 2.468 | 2397.52 | 2337.72 | 0.718 | 0.323 |
| 22 | 2538.32 | 99.133 | 0.837 | 2723.49 | 2418.74 | 0.35 | 0.333 |
| 23 | 2900.94 | 97.718 | 2.239 | 2993.52 | 2725.42 | 1.119 | 1.098 |
| 24 | 3107.32 | 99.331 | 0.594 | 3151.69 | 3074.53 | 0.107 | 0.09 |
| 25 | 3446.79 | 81.327 | 1.711 | 3552.88 | 3429.43 | 9.165 | 0.923 |

Comment;
Aerogel 3

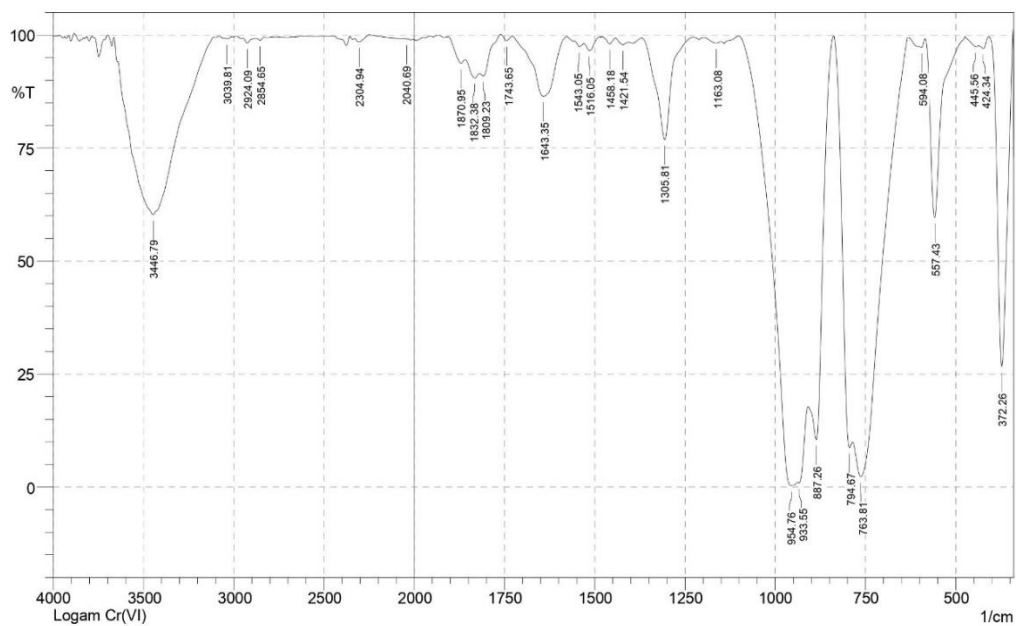
Date/Time; 2/14/2022 3:46:53 PM
No. of Scans;
Resolution;
Apodization;



| No. | Peak | Intensity | Corr. Intensity | Base (H) | Base (L) | Area | Corr. Area |
|-----|---------|-----------|-----------------|----------|----------|---------|------------|
| 1 | 466.77 | 14.692 | 62.048 | 545.85 | 343.33 | 90.515 | 69.581 |
| 2 | 553.57 | 62.612 | 2.055 | 655.8 | 547.78 | 11.635 | 0.637 |
| 3 | 671.23 | 96.4 | 2.999 | 686.66 | 655.8 | 0.282 | 0.201 |
| 4 | 711.73 | 98.96 | 0.603 | 727.16 | 696.3 | 0.105 | 0.047 |
| 5 | 796.6 | 57.883 | 42.139 | 852.54 | 727.16 | 13.397 | 13.404 |
| 6 | 1095.57 | 9.726 | 89.955 | 1298.09 | 854.47 | 212.931 | 212.371 |
| 7 | 1317.38 | 96.597 | 2.854 | 1350.17 | 1300.02 | 0.411 | 0.294 |
| 8 | 1375.25 | 94.816 | 4.666 | 1396.46 | 1350.17 | 0.58 | 0.476 |
| 9 | 1431.18 | 93.228 | 1.554 | 1438.9 | 1396.46 | 0.719 | 0.073 |
| 10 | 1460.11 | 94.316 | 1.021 | 1498.69 | 1454.33 | 0.679 | 0.131 |
| 11 | 1544.98 | 98.654 | 0.376 | 1546.91 | 1539.2 | 0.036 | 0.005 |
| 12 | 1637.56 | 75.428 | 2.387 | 1643.35 | 1573.91 | 4.53 | 0.293 |
| 13 | 1759.08 | 98.898 | 0.897 | 1772.58 | 1749.44 | 0.055 | 0.037 |
| 14 | 1878.67 | 97.958 | 1.044 | 1923.03 | 1863.24 | 0.325 | 0.124 |
| 15 | 2027.19 | 99.031 | 0.304 | 2090.84 | 2007.9 | 0.218 | 0.048 |
| 16 | 2362.8 | 92.47 | 3.778 | 2393.66 | 2345.44 | 1.063 | 0.389 |
| 17 | 2540.25 | 98.877 | 0.685 | 2621.26 | 2474.67 | 0.461 | 0.188 |
| 18 | 2721.56 | 99.121 | 0.863 | 2789.07 | 2665.62 | 0.271 | 0.282 |
| 19 | 2902.87 | 88.106 | 11.891 | 2993.52 | 2791 | 5.296 | 5.325 |
| 20 | 3448.72 | 38.759 | 60.744 | 3739.97 | 2995.45 | 169.128 | 167.639 |

Comment;
G2 Aerogel

Date/Time; 7/1/2022 10:18:13 AM
No. of Scans;
Resolution;
Apodization;



| No. | Peak | Intensity | Corr. Intensity | Base (H) | Base (L) | Area | Corr. Area |
|-----|---------|-----------|-----------------|----------|----------|---------|------------|
| 1 | 372.26 | 26.661 | 71.883 | 406.98 | 343.33 | 14.221 | 13.83 |
| 2 | 424.34 | 97.034 | 1.538 | 437.84 | 408.91 | 0.272 | 0.1 |
| 3 | 445.56 | 97.452 | 0.616 | 474.49 | 437.84 | 0.272 | 0.055 |
| 4 | 557.43 | 59.663 | 39.671 | 584.43 | 474.49 | 7.108 | 6.843 |
| 5 | 594.08 | 97.296 | 1.983 | 632.65 | 584.43 | 0.387 | 0.252 |
| 6 | 763.81 | 2.264 | 20.303 | 785.03 | 634.58 | 86.685 | 22.132 |
| 7 | 794.67 | 8.729 | 15.002 | 837.11 | 786.96 | 24.322 | 2.459 |
| 8 | 887.26 | 10.472 | 32.35 | 908.47 | 839.03 | 31.723 | 8.662 |
| 9 | 933.55 | 0.942 | 2.491 | 937.4 | 910.4 | 35.53 | 1.716 |
| 10 | 954.76 | 0.316 | 10.114 | 1101.35 | 939.33 | 101.329 | 11.883 |
| 11 | 1163.08 | 98.245 | 0.53 | 1197.79 | 1149.57 | 0.274 | 0.06 |
| 12 | 1305.81 | 76.86 | 22.574 | 1369.46 | 1230.58 | 5.296 | 4.958 |
| 13 | 1421.54 | 97.853 | 0.993 | 1442.75 | 1406.11 | 0.259 | 0.086 |
| 14 | 1458.18 | 97.999 | 1.494 | 1479.4 | 1442.75 | 0.187 | 0.11 |
| 15 | 1516.05 | 96.58 | 2.038 | 1529.55 | 1487.12 | 0.401 | 0.192 |
| 16 | 1543.05 | 97.432 | 0.988 | 1556.55 | 1529.55 | 0.242 | 0.055 |
| 17 | 1643.35 | 86.492 | 13.234 | 1728.22 | 1579.7 | 4.316 | 4.147 |
| 18 | 1743.65 | 98.777 | 1.187 | 1761.01 | 1728.22 | 0.088 | 0.084 |
| 19 | 1809.23 | 90.98 | 1.972 | 1818.87 | 1762.94 | 1.139 | 0.167 |
| 20 | 1832.38 | 90.506 | 1.905 | 1857.45 | 1820.8 | 1.369 | 0.194 |
| 21 | 1870.95 | 93.755 | 2.087 | 1905.67 | 1859.38 | 0.822 | 0.226 |
| 22 | 2040.69 | 99.13 | 0.062 | 2056.12 | 2034.9 | 0.074 | 0.003 |
| 23 | 2304.94 | 98.477 | 1.082 | 2331.94 | 2250.93 | 0.315 | 0.208 |
| 24 | 2854.65 | 98.842 | 0.554 | 2873.94 | 2831.5 | 0.157 | 0.047 |
| 25 | 2924.09 | 98.264 | 1.059 | 2949.16 | 2873.94 | 0.355 | 0.129 |
| 26 | 3039.81 | 99.168 | 0.235 | 3049.46 | 3008.95 | 0.113 | 0.021 |
| 27 | 3446.79 | 60.279 | 35.824 | 3641.6 | 3113.11 | 60.324 | 52.836 |

Comment;
Logam Cr(VI)

Date/Time; 10/26/2022 3:44:13 PM
No. of Scans;
Resolution;
Apodization;

Lampiran 18. Hasil Analisis XRD

a. Kulit durian

Match! Phase Analysis Report

Sample: KULIT-DURIAN (2-80)

Sample Data
 File name KULIT-DURIAN.RAW
 File path D:\xrd\KULIT-DURIAN
 Data collected Feb 8, 2023 18:12:28
 Data range 2.000° - 80.000°
 Original data range 2.000° - 80.000°
 Number of points 3901
 Step size 0.020
 Rietveld refinement converged No
 Alpha2 subtracted No
 Background subtr. No
 Data smoothed Yes
 Radiation X-rays
 Wavelength 1.540600 Å

Candidates

| Name | Formula | Entry No. | FoM |
|---|---|-------------|--------|
| Iron | Fe | 96-901-3476 | 0.6773 |
| Chromium | Cr | 96-500-0221 | 0.6746 |
| Chromium | Cr | 96-900-8532 | 0.6746 |
| (Fe _{0.95} W _{0.05}) | Fe _{0.95} W _{0.05} | 96-152-2088 | 0.6734 |
| (Fe _{0.75} V _{0.25}) | Fe _{0.75} V _{0.25} | 96-152-3401 | 0.6688 |
| Iron | Fe | 96-901-3481 | 0.6688 |
| (Au _{0.05} Fe _{0.95}) | Au _{0.05} Fe _{0.95} | 96-151-0056 | 0.6682 |
| | Fe _{0.915} Re _{0.085} | 96-152-3168 | 0.6678 |
| Iron | Fe | 96-901-3479 | 0.6676 |
| Iron | Fe | 96-901-3480 | 0.6676 |
| (Fe _{0.97} Pd _{0.03}) | Fe _{0.97} Pd _{0.03} | 96-152-3167 | 0.6657 |
| Iron | Fe | 96-901-3482 | 0.6643 |
| Iron | Fe | 96-901-3478 | 0.6617 |
| (Fe _{0.9} Ru _{0.1}) | Fe _{0.9} Ru _{0.1} | 96-152-3150 | 0.6611 |
| Periclase | Mg O | 96-901-3219 | 0.6544 |
| | Fe | 96-720-4905 | 0.6507 |
| Iron | Fe | 96-901-3477 | 0.6502 |
| (Cu (N H ₃) ₄) ₃ (Sc F ₆) ₂ | Cu ₃ F ₁₂ H ₃₆ N ₁₂ Sc ₂ | 96-152-5697 | 0.6499 |
| (Fe _{0.94} Rh _{0.06}) | Fe _{0.94} Rh _{0.06} | 96-152-3169 | 0.6491 |
| | Mo ₂ O ₁₅ P ₄ | 96-430-3257 | 0.6458 |
| Niobium oxo phosphate | Nb ₂ O ₁₅ P ₄ | 96-434-5204 | 0.6457 |
| Periclase | Mg O | 96-901-3252 | 0.6436 |
| (Fe _{0.95} Ru _{0.05}) | Fe _{0.95} Ru _{0.05} | 96-152-2769 | 0.6372 |
| Periclase | Mg O | 96-901-3199 | 0.6343 |
| Periclase | Mg O | 96-901-3225 | 0.6268 |
| Bis(oxoniobium) Tetrphosphate(V) | Nb ₂ O ₁₅ P ₄ | 96-151-7730 | 0.6267 |
| | Mo ₂₄ O ₁₈₀ P ₄₈ | 96-430-3258 | 0.6257 |
| Li ₁₉ V O ₂ | Li _{0.19} O ₂ V | 96-153-0868 | 0.6111 |
| | Co Ga | 96-152-5478 | 0.6092 |
| Mn ₃ (Fe (C N) ₆) ₂ (H ₂ O) ₂ | C ₁₂ H ₄ Fe ₂ Mn ₃ N ₁₂ O ₂ | 96-152-6337 | 0.6016 |

Search-Match

Settings
 Reference database used COD-Inorg 2021.12.14
 Automatic zeropoint adaptation Yes
 Downgrade entries with low scaling factors Yes
 Minimum figure-of-merit (FoM) 0.60
 2theta window for peak corr. 0.30 deg.
 Minimum rel. int. for peak corr. 0
 Parameter/influence 2theta 0.50
 Parameter/influence intensities 0.50
 Parameter multiple/single phase(s) 0.50

Peak List

| No. | 2theta [°] | d [Å] | I/I ₀ (peak height) | Counts (peak area) | FWHM |
|-----|------------|--------|--------------------------------|--------------------|--------|
| 1 | 17.34 | 5.1100 | 406.01 | 611.87 | 5.9200 |
| 2 | 21.78 | 4.0773 | 1000.00 | 946.98 | 3.7200 |
| 3 | 44.26 | 2.0448 | 272.53 | 58.28 | 0.8400 |
| 4 | 64.62 | 1.4412 | 298.42 | 60.77 | 0.8000 |
| 5 | 77.72 | 1.2277 | 387.80 | 82.92 | 0.8400 |

Integrated Profile Areas

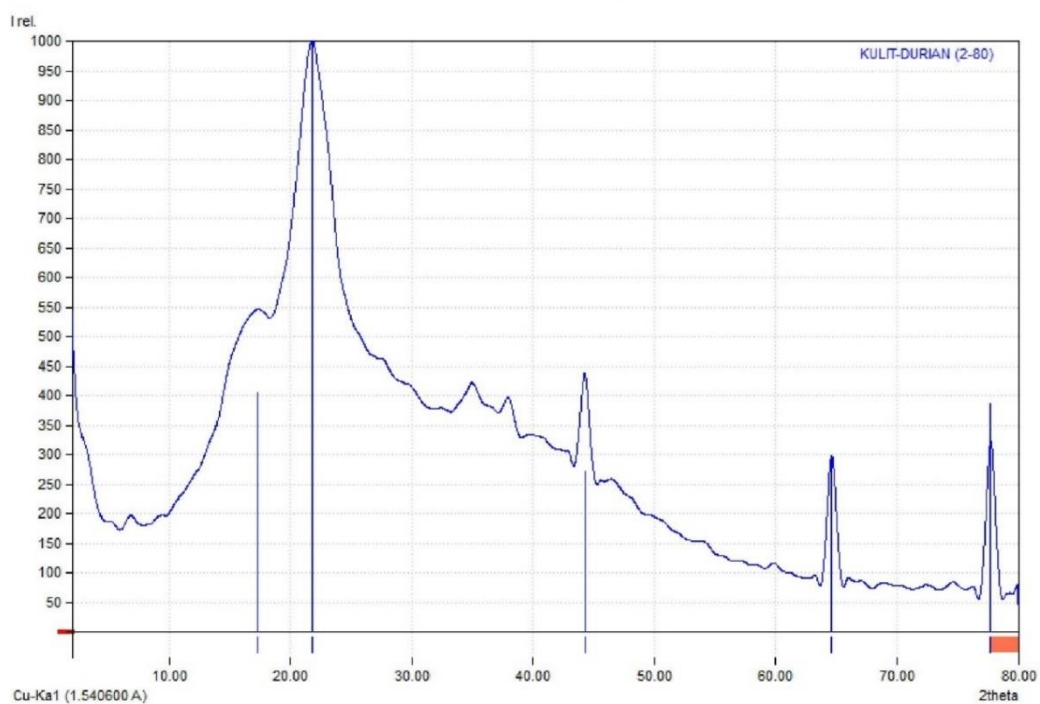
Based on calculated profile

| Profile area | Counts | Amount |
|--|---------------|---------------|
| Overall diffraction profile | 370339 | 100.00% |
| Background radiation | 276727 | 74.72% |
| Diffraction peaks | 93611 | 25.28% |
| Peak area belonging to selected phases | 0 | 0.00% |
| Unidentified peak area | 93611 | 25.28% |

Peak Residuals

| Peak data | Counts | Amount |
|---|---------------|---------------|
| Overall peak intensity | 1761 | 100.00% |
| Peak intensity belonging to selected phases | 0 | 0.00% |
| Unidentified peak intensity | 1761 | 100.00% |

Diffraction Pattern Graphics



b. Selulosa Kulit Durian

```

////////////////////////////////////
/// Profile Data Ascii Dump (XRD)          ///
////////////////////////////////////

Group   : KENSA
Data    : SELUSOSA_ES
File Name : SELUSOSA_ES.RAW

# Profile Datafile
  comment      = 2-80
  date & time  = 01-08-22 12:35:28

# Measurement Condition
X-ray tube
  target       = Cu
  voltage      = 40.0 (kV)
  current      = 30.0 (mA)
Slits
  divergence slit = 1.00000 (deg)
  scatter slit   = 1.00000 (deg)
  receiving slit = 0.15000 (mm)
Scanning
  drive axis    = Theta-2Theta
  scan range    = 2.000 - 80.000
  scan mode     = Continuous Scan
  scan speed    = 2.0000 (deg/min)
  sampling pitch = 0.0100 (deg)
  preset time   = 0.30 (sec)

```

c. Aerogel Selulosa

```

////////////////////////////////////
/// Profile Data Ascii Dump (XRD)          ///
////////////////////////////////////

Group   : KENSA
Data    : Aerogel
File Name : Aerogel.RAW

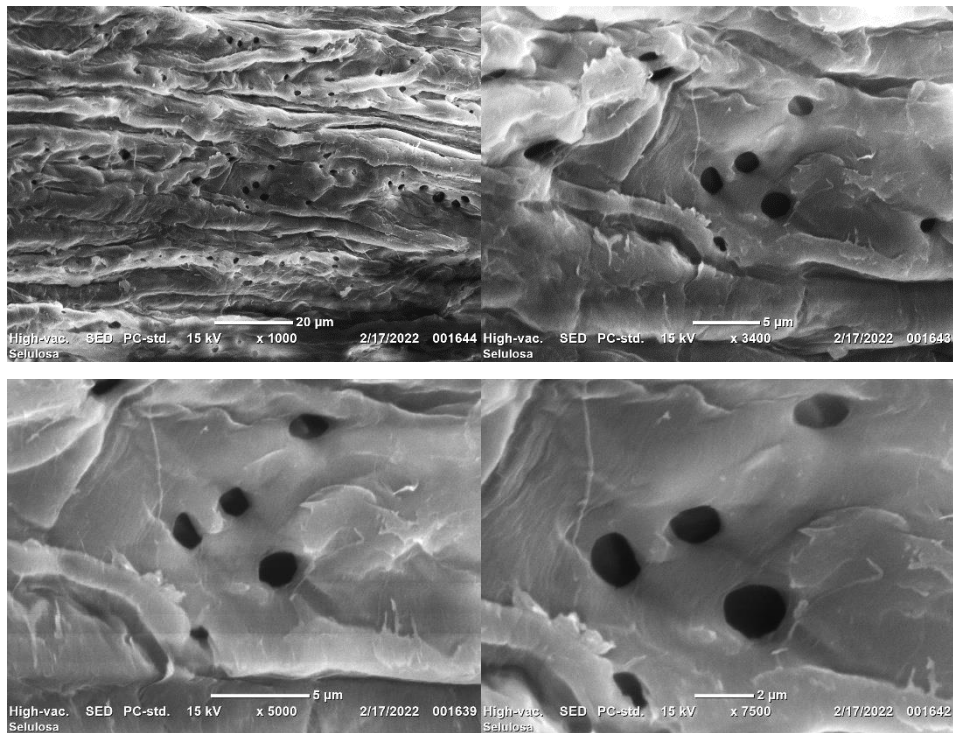
# Profile Datafile
  comment      = 2-80
  date & time  = 02-21-22 10:21:43

# Measurement Condition
X-ray tube
  target       = Cu
  voltage      = 40.0 (kV)
  current      = 30.0 (mA)
Slits
  divergence slit = 1.00000 (deg)
  scatter slit   = 1.00000 (deg)
  receiving slit = 0.15000 (mm)
Scanning
  drive axis    = Theta-2Theta
  scan range    = 2.000 - 80.000
  scan mode     = Continuous Scan
  scan speed    = 2.0000 (deg/min)
  sampling pitch = 0.0200 (deg)
  preset time   = 0.60 (sec)

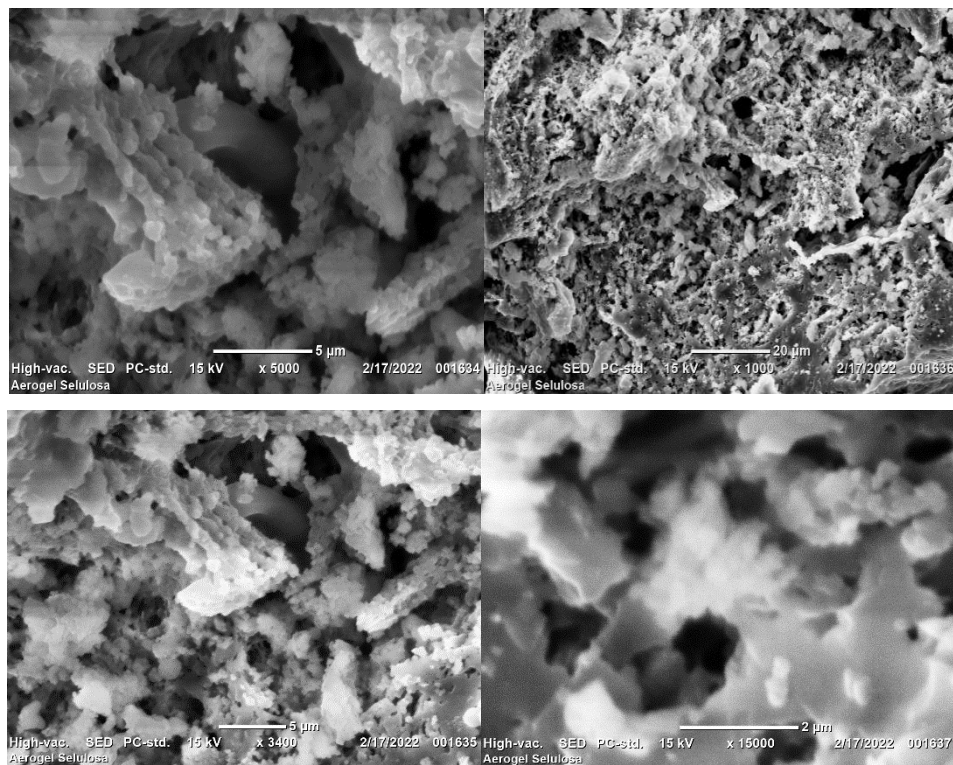
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Lampiran 19. Hasil Analisis SEM

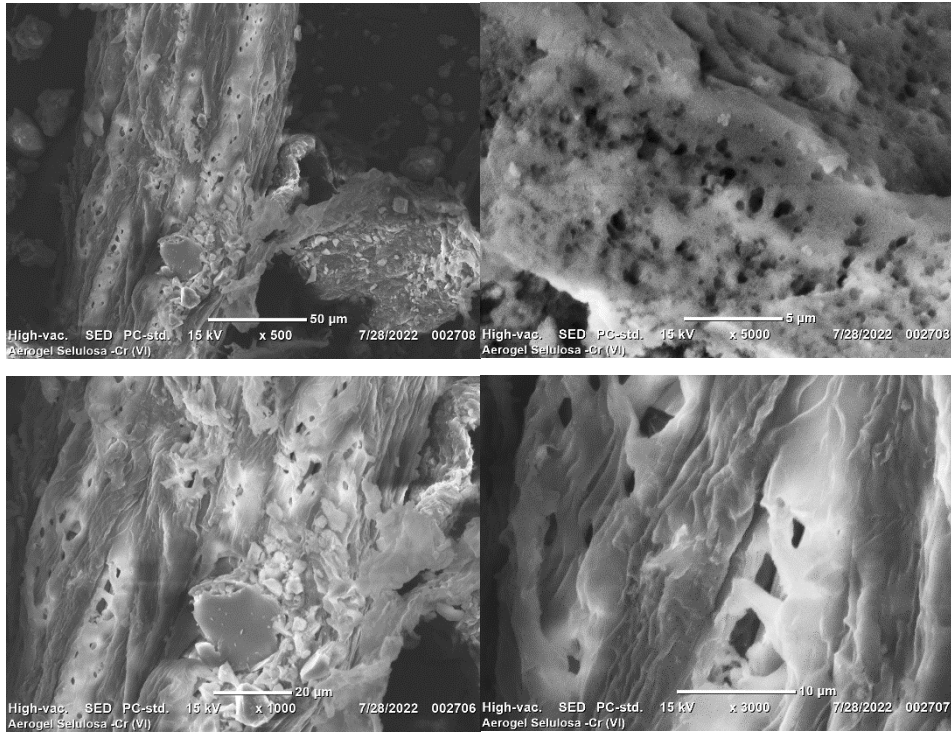
a) Selulosa Kulit Durian



b) Aerogel Selulosa



c) Aerogel selulosa setelah mengadsorpsi Cr(VI)



Lampiran 20. Hasil Analisis BET-BJH



TriStar II 3020 2.00

TriStar II 3020 Version 2.00 Unit
1 Port 1

Serial #: 1108

Page 1

Sample: Aerogel Selulosa
 Operator: Sarah
 Submitter: 37537
 File: C:\TriStar II 3020\data\SAMPEL\2022\...\Aerogel Selulosa.SMP

| | |
|--|---|
| Started: 4/21/2022 12:50:00 PM | Analysis Adsorptive: N2 |
| Completed: 4/21/2022 2:11:07 PM | Analysis Bath Temp.: -195.850 °C |
| Report Time: 4/22/2022 8:16:19 AM | Thermal Correction: No |
| Sample Mass: 0.6741 g | Warm Free Space: 10.9608 cm ³ Measured |
| Cold Free Space: 31.2064 cm ³ | Equilibration Interval: 5 s |
| Low Pressure Dose: None | Sample Density: 1.000 g/cm ³ |
| Automatic Degas: No | |

Summary Report

Surface Area

Single point surface area at P/Po = 0.303369944: 2.0610 m²/g

BET Surface Area: 2.1249 m²/g

t-Plot External Surface Area: 2.3914 m²/g

BJH Adsorption cumulative surface area of pores
 between 1.7000 nm and 300.0000 nm diameter: 2.141 m²/g

BJH Desorption cumulative surface area of pores
 between 1.7000 nm and 300.0000 nm diameter: 2.2928 m²/g

D-H Adsorption cumulative surface area of pores
 between 1.7000 nm and 300.0000 nm diameter: 1.884 m²/g

D-H Desorption cumulative surface area of pores
 between 1.7000 nm and 300.0000 nm diameter: 2.3032 m²/g

Pore Volume

Single point adsorption total pore volume of pores
 less than 171.9564 nm diameter at P/Po = 0.988729858: 0.010222 cm³/g

t-Plot micropore volume: -0.000141 cm³/g

BJH Adsorption cumulative volume of pores
 between 1.7000 nm and 300.0000 nm diameter: 0.010049 cm³/g

BJH Desorption cumulative volume of pores
 between 1.7000 nm and 300.0000 nm diameter: 0.009939 cm³/g

Pore Size

Adsorption average pore width (4V/A by BET): 19.24200 nm

BJH Adsorption average pore diameter (4V/A): 18.7742 nm

BJH Desorption average pore diameter (4V/A): 17.3402 nm

D-H Adsorption average pore diameter (4V/A): 21.0934 nm

D-H Desorption average pore diameter (4V/A): 17.4359 nm



TriStar II 3020 2.00

TriStar II 3020 Version 2.00 Unit
1 Port 1

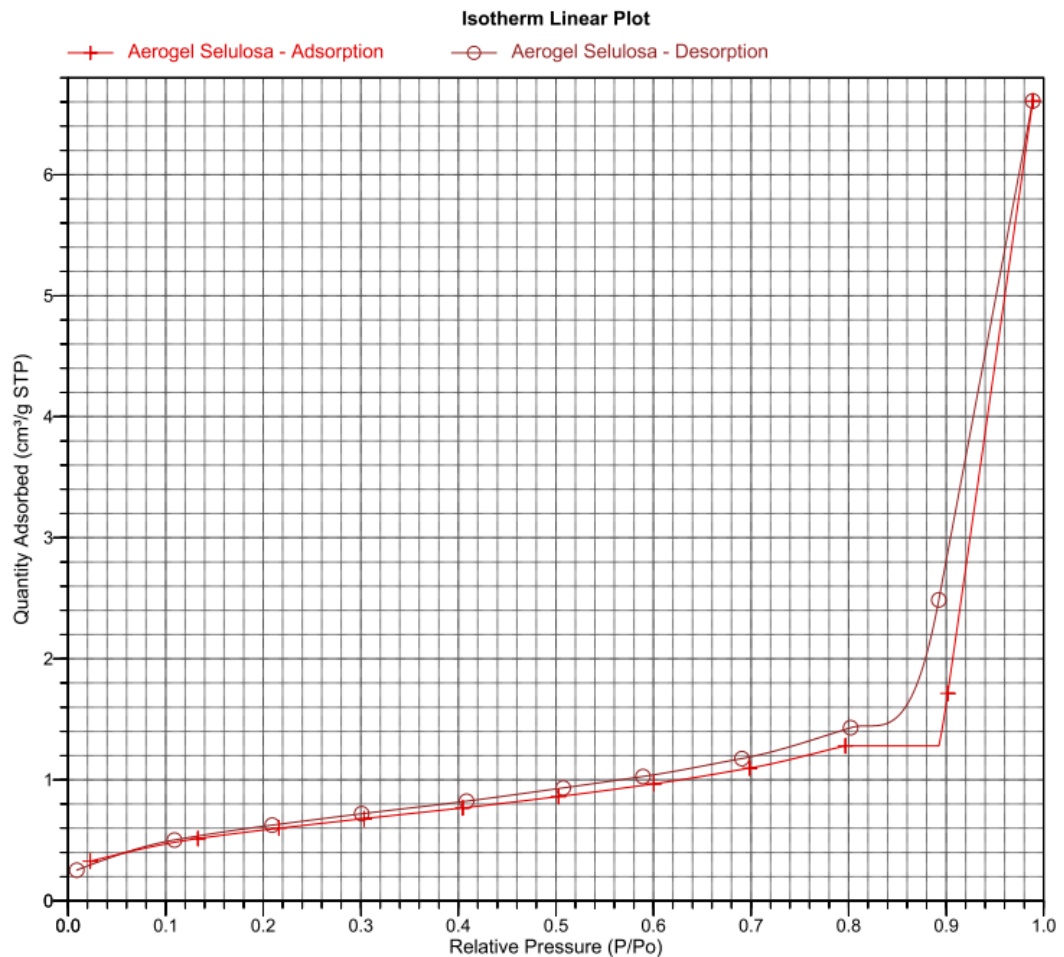
Serial #: 1108

Page 4

Sample: Aerogel Selulosa
 Operator: Sarah
 Submitter: 37537
 File: C:\TriStar II 3020\data\SAMPEL\2022\...\Aerogel Selulosa.SMP

Started: 4/21/2022 12:50:00 PM
 Completed: 4/21/2022 2:11:07 PM
 Report Time: 4/22/2022 8:16:19 AM
 Sample Mass: 0.6741 g
 Cold Free Space: 31.2064 cm³
 Low Pressure Dose: None
 Automatic Degas: No

Analysis Adsorptive: N₂
 Analysis Bath Temp.: -195.850 °C
 Thermal Correction: No
 Warm Free Space: 10.9608 cm³ Measured
 Equilibration Interval: 5 s
 Sample Density: 1.000 g/cm³





TriStar II 3020 2.00

TriStar II 3020 Version 2.00 Unit
1 Port 1

Serial #: 1108

Page 12

Sample: Aerogel Selulosa
 Operator: Sarah
 Submitter: 37537
 File: C:\TriStar II 3020\data\SAMPEL\2022\...\Aerogel Selulosa.SMP

Started: 4/21/2022 12:50:00 PM Analysis Adsorptive: N2
 Completed: 4/21/2022 2:11:07 PM Analysis Bath Temp.: -195.850 °C
 Report Time: 4/22/2022 8:16:19 AM Thermal Correction: No
 Sample Mass: 0.6741 g Warm Free Space: 10.9608 cm³ Measured
 Cold Free Space: 31.2064 cm³ Equilibration Interval: 5 s
 Low Pressure Dose: None Sample Density: 1.000 g/cm³
 Automatic Degas: No

BJH Adsorption Pore Distribution Report

Faas Correction

Harkins and Jura

$$t = [13.99 / (0.034 - \log(P/P_0))] ^{0.5}$$

Diameter Range: 1.7000 nm to 300.0000 nm

Adsorbate Property Factor: 0.95300 nm

Density Conversion Factor: 0.0015468

Fraction of Pores Open at Both Ends: 0.00

| Pore Diameter Range (nm) | Average Diameter (nm) | Incremental Pore Volume (cm ³ /g) | Cumulative Pore Volume (cm ³ /g) | Incremental Pore Area (m ² /g) | Cumulative Pore Area (m ² /g) |
|--------------------------|-----------------------|--|---|---|--|
| 171.8 - 20.9 | 22.8 | 0.009536 | 0.009536 | 1.676 | 1.676 |
| 20.9 - 10.3 | 12.1 | 0.000293 | 0.009829 | 0.097 | 1.773 |
| 10.3 - 6.9 | 7.8 | 0.000016 | 0.009845 | 0.008 | 1.781 |
| 6.9 - 5.0 | 5.6 | 0.000006 | 0.009852 | 0.005 | 1.786 |
| 5.0 - 3.9 | 4.3 | 0.000016 | 0.009867 | 0.015 | 1.800 |
| 3.9 - 3.1 | 3.4 | 0.000029 | 0.009896 | 0.034 | 1.834 |
| 3.1 - 2.4 | 2.7 | 0.000034 | 0.009930 | 0.051 | 1.885 |
| 2.4 - 2.0 | 2.1 | 0.000050 | 0.009980 | 0.094 | 1.979 |
| 2.0 - 1.5 | 1.7 | 0.000069 | 0.010049 | 0.162 | 2.141 |



TriStar II 3020 2.00

TriStar II 3020 Version 2.00 Unit
1 Port 1

Serial #: 1108

Page 13

Sample: Aerogel Selulosa
 Operator: Sarah
 Submitter: 37537
 File: C:\TriStar II 3020\data\SAMPEL\2022\...\Aerogel Selulosa.SMP

Started: 4/21/2022 12:50:00 PM Analysis Adsorptive: N2
 Completed: 4/21/2022 2:11:07 PM Analysis Bath Temp.: -195.850 °C
 Report Time: 4/22/2022 8:16:19 AM Thermal Correction: No
 Sample Mass: 0.6741 g Warm Free Space: 10.9608 cm³ Measured
 Cold Free Space: 31.2064 cm³ Equilibration Interval: 5 s
 Low Pressure Dose: None Sample Density: 1.000 g/cm³
 Automatic Degas: No

BJH Desorption Pore Distribution Report

Faas Correction

Harkins and Jura

$$t = [13.99 / (0.034 - \log(P/P_0))] ^{0.5}$$

Diameter Range: 1.7000 nm to 300.0000 nm

Adsorbate Property Factor: 0.95300 nm

Density Conversion Factor: 0.0015468

Fraction of Pores Open at Both Ends: 0.00

| Pore Diameter Range (nm) | Average Diameter (nm) | Incremental Pore Volume (cm ³ /g) | Cumulative Pore Volume (cm ³ /g) | Incremental Pore Area (m ² /g) | Cumulative Pore Area (m ² /g) |
|--------------------------|-----------------------|--|---|---|--|
| 171.7 - 19.1 | 20.6 | 0.008079 | 0.008079 | 1.567 | 1.567 |
| 19.1 - 10.4 | 12.3 | 0.001741 | 0.009820 | 0.568 | 2.135 |
| 10.4 - 6.6 | 7.6 | 0.000037 | 0.009857 | 0.020 | 2.154 |
| 6.6 - 3.0 | 3.3 | 0.000022 | 0.009879 | 0.027 | 2.181 |
| 3.0 - 2.3 | 2.6 | 0.000017 | 0.009896 | 0.027 | 2.208 |
| 2.3 - 1.8 | 2.0 | 0.000043 | 0.009939 | 0.085 | 2.293 |